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### On-chip stimulated Brillouin scattering and its applications

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#### **ABSTRACT**

We review recent demonstration of stimulated Brillouin scattering in a chalcogenide photonic chip and its application to optical and microwave signal processing tasks. The interaction between light and sound via stimulated Brillouin scattering (SBS) was exploited in chalcogenide photonic circuits to achieve on-chip SBS slow and fast light, microwave photonic filters, and dynamic gratings using travelling-wave geometry. Using a ring-resonator geometry, photonic-chip based Brillouin laser was demonstrated.

**Keywords:** stimulated Brillouin scattering, on-chip, chalcogenide, slow-light, dynamic grating, microwave signal processing, dynamic grating, Brillouin laser

#### 1. INTRODUCTION

Stimulated Brillouin scattering is a nonlinear scattering process where a pump wave  $(\omega_p)$ , when encounter acoustic vibrations  $(\Omega_B)$  in the medium, gets backscattered, resulting in a light beam which is down-shifted in frequency  $(\omega_s = \omega_p - \Omega_B)$  with respect to the pump by the acoustic frequency [1]. This backscattered signal is known as the Stokes wave. A probe, centered at the Stokes frequency, experiences gain when counter-propagated to the pump wave whereas a probe that is up-shifted with respect to the pump  $(\omega_{as} = \omega_P + \Omega_B)$ , known as the anti-Stokes wave, experiences absorption. The gain and absorption associated with the Stokes and anti-Stokes frequency exhibit a resonant behavior, where the resonance has a Lorentzian shape whose linewidth  $(\Delta v_B)$  is determined by the acoustic phonon lifetime in the medium. The long phonon lifetime, which is typically of-the-order of several nanoseconds in most of the commonly used optical materials, results in a narrow SBS linewidth ~ 10 MHz. The narrow gain and absorption response of the SBS process has recently been exploited in long (~km) silica optical fibers for applications in optical and microwave signal processing. The small Brillouin scattering cross-section  $(g_B)$  and large effective mode area  $(A_{eff})$  of silica fiber necessitated the use of long lengths  $(L \sim km)$  in order to obtain large gain  $G = g_B P_p L A_{eff}$  using reasonable pump power  $P_p \sim 100$  mW. Exploiting SBS in a chip-scale device is critical to realize photonic integration of optical and microwave signal processing tasks and Brillouin lasers. However, this requires generating large gain (G) in short length using moderate power level, which is challenging due to the constraints on the optical and acoustic properties of material and device.

Here we review our recent work on exciting SBS in a chalcogenide photonic-chip [2-4] and its application to a number of signal processing tasks such as slow- and fast-light induced tunable delay [5], Brillouin dynamic gratings [6], microwave photonic filters [7-9] and Brillouin laser [10]. The key to these demonstrations was the large Brillouin scattering cross-section ( $g_B \sim 0.74 \times 10^9 \text{ m/W}$ ) and small mode area ( $A_{eff} \sim 2.3 \text{ } \mu\text{m}^2$ ) of the photonic chip [4], which resulted in large gain at low powers. Slow- and fast-light will be discussed in Section 2 followed by on-chip dynamic gratings in Section 3. In Section 4, we discuss the application of narrow SBS gain/loss profile to

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microwave photonic filter followed by review of photonic-chip Brillouin laser in Section 5. In Section 6, we present a summary of our results followed by conclusion.

#### 2. ON-CHIP SBS SLOW AND FAST LIGHT

SBS based slow and fast light exploit the gain and absorption resonances, where the large index slope, resulting as a consequence of the Kramers-Kronig relation, leads to significant reduction (advancement) in the speed of light pulses centered at the Stokes (anti-Stokes) frequencies [11-14]. In order to realize SBS slow-light in short lengths (~cm), careful consideration must be given to optical and acoustic properties of the material and device because the slowing down factor ( $\Delta n_g = g_B P_p c / \Gamma_B A_{eff}$ ) depends on their parameters, where the Brillouin linewidth  $\Gamma_B$  is determined by the phonon lifetime in the material and  $P_p$  is the pump power. Large  $\Delta n_g$ required to achieve large delay  $(T_d = L\Delta n_g/c)$  in short length using small powers, therefore, can be achieved using a device with large  $g_B$  and small  $A_{eff}$ . A material with large refractive index (n) and elasto-optic coefficient  $(p_{12})$  when used to design a device that provides strong acousto-optic overlap ( $\eta$ ) results in large  $g_B$ , which is given according to:

$$g_B = \eta \frac{4\pi n^8 p_{12}^2}{c\rho \nu_B \Delta \nu_B \lambda_D^3}, \qquad (1)$$

where material parameters such as density  $(\rho)$ , Brillouin shift  $v_B$  and linewidth  $\Delta v_B = \Gamma_B/2\pi$  typically vary with in a factor of two for commonly used optical materials. Strong dependence of  $g_B$  on material parameters such as n and  $p_{12}$  however plays a crucial role in material choice. For example, silica (n=1.445) and chalcogenide (n=2.45) have nearly the same  $p_{12}$  however; the large n of chalcogenide glass results in a  $\frac{n_{As_2S_3}^8}{n_{Silica}^8} \sim 70$ , which is a significant

increase in  $g_B$  just based on the choice of material.

In a recent demonstration, SBS slow- and fast-light was reported in a 7 cm long chalcogenide photonic-chip where the large refractive index (n) and elasto-optic coefficient  $(p_{12})$  when combined with the strong acousto-optic overlap  $(\eta)$  in the chip (see Fig. 1) resulted in large  $g_B$ . The large  $g_B$  and small  $A_{eff}$  of the photonic-chip generated large  $\Delta n_g$ , required for chip-based SBS slow-light. The Brillouin shift and gain bandwidth for the photonic chip were 7.7 GHz and 34 MHz respectively. The chip was used to measure  $\Delta n_g$  (see Fig. 2(a, b)) and pulse delay (see Fig. 2(c, d)), which can be tuned by varying the pump power. The  $\Delta n_g$  for the slow (fast) light regime, obtained from the delay (advancement) of a low frequency sinusoidal signal, was found to be 68 (-44) using a gain (absorption) of 11 dB (-7dB). Tunable delays ranging from -7ns to 23 ns were measured for 25 ns and 100 ns long nearly

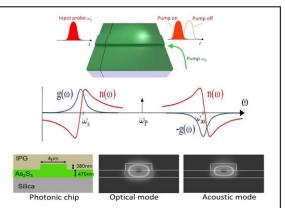


Fig.1 Schematic of on-chip SBS slow-light showing the large index-slope associated with the Stokes and anti-Stokes resonances, which results in large group-index for the slow-and fast-light regimes. The large acousto-optic confinement in the photonic chip in combination with small mode area and large refractive index and elasto-optic coefficient results in large on-chip gain.

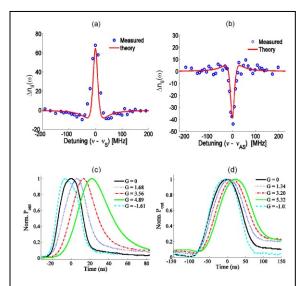


Fig.2 Group-index (a,b) and pulse delay (c,d) measurement for the SBS slow- and fast-light in a photonic chip showing large group-index 68 (-44) for the slow (fast) light regime and pulse delay of nearly pulse width for a 25 ns long Gaussian pulse (c).

Gaussian pulses. A large group-index change  $\Delta n_g \sim 130$  was obtained from the delay of 100 ns pulse when a gain of 23 dB

was generated at a pump power of  $\sim 300$  mW. This  $\Delta n_g$  is nearly 13 times larger than the record  $\Delta n_g \sim 10$  for the fiber-based SBS slow-light, which was obtained when a pump power of  $\sim 650$  mW was injected in a 2m long erbium-doped tellurite fiber to realize a gain of 53dB [15]. SBS in a chalcogenide photonic-chip, therefore, provides a highly efficient, compact device for realizing large tunable delays. This large tunable delay can be used for applications in phased array antenna and for designing microwave photonic filters.

#### 3. PHOTONIC-CHIP BASED MICROWAVE PHOTONIC FILTER

Narrowband, tunable and reconfigurable microwave photonic filters (MPFs) with high Q-factor are critical to microwave signal processing. Reconfigurable, narrowband MPFs with wide tuning range have been demonstrated using SBS in long length ( $\sim 10$ -20 km) optical fibers [16], which are incompatible with photonic integration. On-chip MPFs have been demonstrated using ring resonators; however demonstrated filter 3dB bandwidth ( $f_{3dB} \sim 1 GHz$ ) and small tuning range has resulted in very low Q-factor  $\sim 10$ .

Recently, an on-chip narrowband, reconfigurable, microwave photonic filter with large Q  $\sim$  520 and wide tuning range was demonstrated exploiting the large gain and narrow spectral response of the SBS process in a 6.5 cm long chalcogenide rib waveguide. The MPF maintained a stable 3 dB bandwidth of  $23 \pm 2$ MHz (see Fig. 3(b)) and amplitude of  $20 \pm 2$  dB (see Fig. 3(b)) over a large frequency tuning range of 2-12 GHz (See Fig. 3(a)). By tailoring the pump spectrum, the 3dB bandwidth  $f_{3dB}$  of the MPF was reconfigured from  $\sim$ 20 MHz to  $\sim$ 40 MHz resulting in a tuning of the shape factor S, defined as the ratio of 20dB bandwidth to 3dB bandwidth (S= $f_{20dB}/f_{3dB}$ ), from 3.5 to 2 [7, 8].

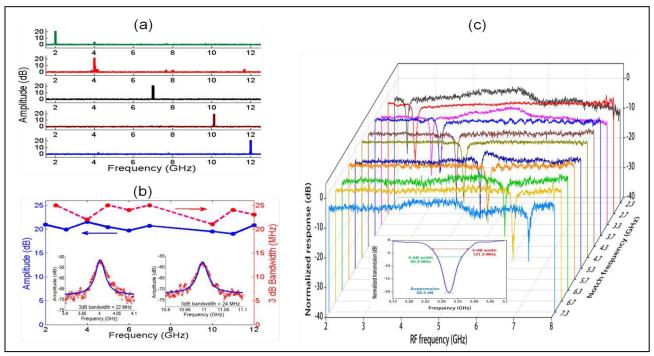


Fig.3. Measured response of the photonic-chip based microwave photonic filter showing (a) a tuning range of 2-12 GHz for a bandpass photonic filter (b) amplitude and  $f_{3dB}$  for the photonic-chip based bandpass photonic filter demonstrating good amplitude (~20  $\pm$  2 dB) and bandwidth (23  $\pm$  2 MHz) stability [7, 8] and (c) tuning response of a SBS based on-chip notch filter demonstrating a wide tuning range 2-8 GHz with a 3 dB bandwidth of ~ 130  $\pm$  10 MHz and a notch depth of ~ 18  $\pm$  2 dB [9]. Inset (b): MPF profiles taken at centre frequencies of 4 and 11 GHz and (c) notch response at 53.GHz.

As mentioned earlier, SBS process generates gain and absorption resonances at the Stokes and anti-Stokes frequency. Using the SBS absorption in a chalcogenide photonic-chip, a widely tunable (2-8 GHz), microwave photonic notch filter (see

Fig. 3(c)) was demonstrated with a 3 dB notch bandwidth of  $\sim 130~\pm 10~\text{MHz}$  and a notch depth of  $\sim 18 \pm 2~\text{dB}$  [9]. This demonstration enables on-chip microwave signal processing using SBS.

#### 4. ON-CHIP BRILLOUIN DYNAMIC GRATING

Dynamic gratings provide a novel platform for applications such as sensing, microwave signal processing and tunable delay [17, 18]. Recently Brillouin dynamic gratings (BDGs) have been demonstrated in tens-of-meter long polarization maintaining fibres (PMFs)[19], in single-mode fibers (SMFs) [20], and in few-mode fibres (FMFs) [21]. Photonic integration of functionalities such as microwave signal processing, tunable delay lines and data storage requires realization of on-chip BDG. Realization of Brillouin grating in a photonic-chip, however, has been a challenge due to the small cross-section of the stimulated Brillouin scattering (SBS) process in silica glass, which is the commonly used material for optical fibers.

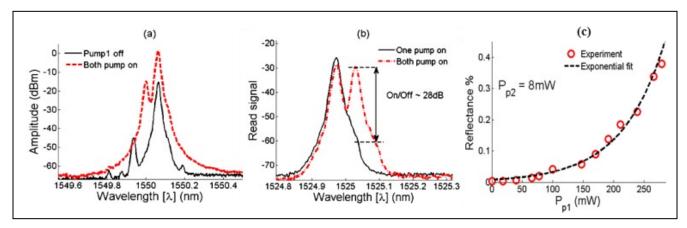


Fig. 4 (a) Pump2 spectrum when pump1 is off (solid) and on (dashed) demonstrating Brillouin gain and generation of BDG; (b) switching characteristics of the BDG when both pumps are turned on resulting in an On/Off ratio ~28 dB and (c) reflectance of the on-chip BDG for powers P<sub>p1</sub> of pump 1 [6].

Recently, dynamic gratings were demonstrated using large gain and high birefringence of the chalcogenide photonic-chip discussed in previous sections. Figure 4 shows the switching characteristic and reflectance of an on-chip Brillouin dynamic grating. When the pump1 is off (on), pump2 experiences no gain (gain: see dashed Fig. 4(a)) demonstrating the generation of a BDG; where both pump1 and pump2 are x-polarized. The BDG is then characterized by launching a probe in y-polarization. When the pump1 in x-polarization is off, no read signal is observed in the backscattered signal (solid Fig. 4(b)) [6]. However, when both the pumps are turned on a large read signal with an On-Off ratio ~28dB was observed (dashed Fig. 4(b)). The reflectance of BDG for different pump1 power ( $P_{p1}$ ) while pump2 power ( $P_{p2} = 8mW$ ) is fixed is shown in Fig. 4(c) demonstrating an exponential growth, as expected because Brillouin gain increases exponentially with  $P_{p1}$ . All the applications of on-chip SBS discussed so far rely on the travelling-wave geometry where both the pump and the probe propagate the device once. It is well-known that in the presence of feedback, the power required to excite SBS reduces significantly, where the threshold reduction depends on the quality factor Q of the resonator, and results in lasing action. In the next section, we discuss application of SBS in chalcogenide photonic-chip to realize a Brillouin laser.

#### 5. PHOTONIC-CHIP BASED BRILLOUIN LASER

Brillouin lasers have been known for their narrow linewidth, low noise and low threshold properties. Recent focus on realizing efficient, low noise sources for coherent optical communications and microwave photonic signal processing has generated an interest in on-chip Brillouin lasers. Low threshold, low-frequency noise Brillouin lasers were recently demonstrated using silica wedge resonators, where both the pump and Stokes were aligned with the cavity resonances [22, 23], and used for realizing a highly stable, on-chip microwave source. Here we discuss a different approach where only the Stokes signal experiences feedback [24] and use it to realize a photonic-chip based Brillouin laser.

Figure 5 shows the principle of the Brillouin laser based on a chalcogenide photonic chip where on-chip tapers were used to improve coupling efficiency [25]. In this configuration (see Fig. 5(a)), pump propagates through the chip only once before it is removed by a circulator whereas the Stokes signal recirculates in a ring comprising a 7cm long photonic chip and 10 m long silica fibre with chip acting as a gain medium. The laser demonstrated a threshold of 360 mW [10], which is nearly five times smaller than that for the single-pass geometry, and a slope efficiency of 30% (see Fig. 5(b)). In this demonstration, the measured linewidth of 100 kHz was 15 times smaller than the linewidth (1.55 MHz) of the Brillouin pump and 340 times smaller than the Brillouin bandwidth (34 MHz) in the photonic-chip [4]

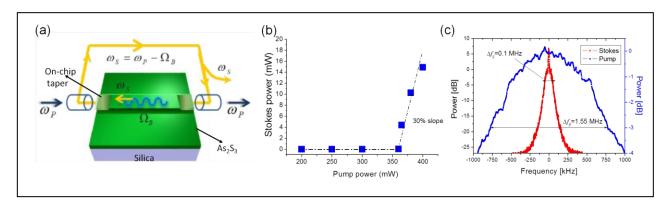


Figure 5 (a) Schematic showing the principle of photonic-chip based Brillouin laser and its threshold characteristics (b) and linewidth measurement (c) [10].

The demonstration of on-chip SBS using travelling-wave and resonator geometry has opened up opportunities for optical and microwave signal processing. New methods of fabricating chalcogenide photonic chips have recently been explored to harness SBS in a chip platform [26]. While chalcogenide photonic chip provides large on-chip SBS gain, realizing SBS in a silicon nanostructure would result in giant SBS enhancement due to combined effect of radiation pressure and electrostriction [27]. Harnessing SBS in a CMOS compatible platform will enable mass production of photonic integrated circuits for signal processing, nanolasers and tailoring the interaction between light and sound [28, 29].

#### 6. CONCLUSION

We discussed our recent demonstration of realizing slow, fast and negative group velocities using on-chip SBS, where  $\Delta n_g$  was continuously varied from -44 to +130 resulting in group velocities of 2307 km/s and -6818 km/s for slow- and fast-light respectively. Such a wide variation allowed continuously tunable, on-chip delays ranging from -6 ns to +23 ns in a 7cm long photonic chip with the maximum delay achieved at the relatively low pump power of  $\sim 300$  mW. On-chip Brillouin dynamic gratings and microwave photonic filters with record performance were presented. A photonic-chip based Brillouin ring laser demonstrated a 15 times reduction in the laser linewidth. In future, application of chirped dynamic grating for efficient pulse storage and retrieval will be explored [30]. Fully integrated Brillouin laser using distributed feedback will provide a stable low noise source for coherent optical communication [31].

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