

UNIVERSITY OF TECHNOLOGY SYDNEY  
School of Mathematical and Physical Sciences

**Stimulated Brillouin scattering in nanophotonic  
waveguides and resonators**

by

**Sayyed Reza Mirnaziry**

A THESIS SUBMITTED  
IN PARTIAL FULFILLMENT OF THE  
REQUIREMENTS FOR THE DEGREE

**Doctor of Philosophy**

Sydney, Australia

February, 2018

## Certificate of Authorship/Originality

I certify that the work in this thesis has not been previously submitted for a degree nor has it been submitted as a part of the requirements for other degree except as fully acknowledged within the text.

I also certify that this thesis has been written by me. Any help that I have received in my research and in the preparation of the thesis itself has been fully acknowledged. In addition, I certify that all information sources and literature used are quoted in the thesis.

© Copyright 2018 Sayyed Reza Mirnaziry

Production Note:

Signature removed prior to publication.

20/02/2018

# ABSTRACT

## **Stimulated Brillouin scattering in nanophotonic waveguides and resonators**

by

Sayyed Reza Mirnaziry

Dissertation directed by Associate Professor Christopher G. Poulton  
School of Mathematical and Physical Sciences

In this work, we theoretically and numerically study Stimulated Brillouin Scattering (SBS) in integrated waveguides and resonators. We review SBS process by using coupled equations and determine a broad range of SBS parameters including SBS gain, opto-acoustic overlap, optical forces and power conversion between pump and Stokes waves. For numeric analysis, in addition to performing simulations we write appropriate codes and employ different iterative techniques as well as root finding methods to analyze SBS in interested configurations.

We study silicon-chalcogenide slot waveguides as a robust candidate to enhance SBS. We explain how constructive contribution of radiation pressure and electrostriction can increase the SBS gain in this structure. We also optimize the waveguide geometry and determine the optimum pump power as well as waveguide length as a function of SBS figure of merit, using our analytic expressions. We also show that putting a silica layer on top of the waveguide lead to a significant increase in the opto-acoustic overlaps and therefore, rise the SBS gain while reducing the impact of nonlinear losses in this structure.

We explore SBS in integrated racetrack ring resonators in both regimes of amplifying and lasing. We use analytic and numeric approaches to demonstrate pump and Stokes evolution in designed rings and through the output. In addition we an-

alyze the impact of nonlinear dispersion as well as thermal effects on SBS in rings. Finally, we determine the pump power to achieve Stokes amplification, the threshold pump power for lasing and the output Stokes power in the presence of linear and nonlinear optical losses.

## Dedication

*To Mudafi'an-i Haram who defended the Ahl al-Bayt (a) and fought against takfiri terrorists.*

## Acknowledgements

My deepest gratitude goes to my primary supervisor Dr. Christopher Poulton for his patience, motivation, enthusiasm and invaluable support throughout my PhD. He persistently tracked my progress and enlightened me with new ideas in our meetings. He was a meticulous supervisor who carefully read my manuscripts, especially this thesis, which greatly helped me improve its content. At many stages, where I had made mistakes in my analysis, he comprehensively assisted me in detecting them. I thank him for all his kind support.

I would like to thank my industrial supervisors, Dr. Benjamin Eggleton of Sydney University and Dr. Michael Steel of Macquarie University, for the patience, guidance, encouragement and advice they provided throughout my PhD. I also want to express my sincere gratitude to my co-supervisor Dr. Christian Wolff. His deep insights throughout this project assisted me through all stages of my research. I really appreciate the time he spent to go through my draft papers. I also thank Dr. Kokou Dossou at UTS for helping me in better understanding numerical techniques.

I am very indebted to these prestigious institutions for their support in this work; CUDOS for giving me this opportunity to collaborate with leading researchers and experimentalists and the University of Technology, Sydney for providing the facilities and supporting me throughout my PhD. I also acknowledge the financial support from the Industrial Doctoral Training Centre (IDTC) during my PhD, especially as they also provided training courses and annual conferences to establish contact between students and industries.

Last but not the least, I would like to thank my family in my language:

پدر و مادر عزیزم! بی تردید لحظه لحظه های زندگیم و ذره ذره موفقیت هایم مرهون فداکاری شما  
و بخشش سخاوتمندانه عمر با برکتتان است. از خداوند بزرگ آرزوی سلامتی و عاقبت به  
خیری برایتان دارم. همسر عزیزم! همراهی تحسین بر انگیزت رادر دوران تحصیل صمیمانه  
قدر دانم. به وجود افتخار، و در کنارت و سید مادی عزیزم احساس خوشبختی می کنم.

Sayyed Reza Mirnaziry  
Sydney, Australia, 2017.

# List of Publications

## Journal Papers

1. Sayyed Reza Mirnaziry, Christian Wolff, MJ Steel, Benjamin J Eggleton, and Christopher G Poulton. Stimulated Brillouin scattering in silicon/chalcogenide slot waveguides. *Optics Express*, 24(5):4786–4800, 2016.
2. Sayyed Reza Mirnaziry, Christian Wolff, MJ Steel, Benjamin J Eggleton, and Christopher G Poulton. Stimulated Brillouin scattering in integrated ring resonators. *JOSA B*, 34(5):937–949, 2017.
3. Sayyed Reza Mirnaziry, Christian Wolff, Blair Morrison, MJ Steel, Benjamin J Eggleton, and Christopher G Poulton. Lasing in ring resonators by Stimulated Brillouin scattering in the presence of nonlinear loss. *Optics Express*, 25(20):23619–23633, 2017.

In addition to presentations in annual CUDOS workshops, a poster is presented from this project in the following conference

1. Sayyed Reza Mirnaziry, Christian Wolff, MJ Steel, Benjamin J Eggleton, and Christopher G Poulton. Stimulated Brillouin scattering in silicon-chalcogenide slot waveguides. *CLEO/Europe EQEC 2015 Conference*, Munich, Germany.

We note that Chapters 4, 5 and 6 are written according to papers 1, 2 and 3, respectively with small modifications.



# Contents

Certificate	ii
Abstract	iii
Dedication	v
Acknowledgments	vi
List of Publications	viii
List of Figures	xiii
Abbreviation	xxiii
<b>1 Introduction</b>	<b>1</b>
1.1 Thesis Organization . . . . .	3
<b>2 Background</b>	<b>5</b>
2.1 Early work on SBS . . . . .	9
2.2 SBS in integrated waveguides . . . . .	10
2.3 Applications . . . . .	14
2.3.1 SBS microwave filters . . . . .	14
2.3.2 SBS lasers . . . . .	14
2.3.3 Optical data storage . . . . .	15
2.3.4 All optical isolator . . . . .	17
2.4 Theory of SBS in optical waveguides and context of this thesis . . . . .	17
<b>3 Theory</b>	<b>21</b>

3.1	Initial assumptions . . . . .	21
3.2	Electromagnetic waves in waveguides . . . . .	21
3.3	Acoustic waves in waveguides . . . . .	23
3.3.1	Voigt notation . . . . .	25
3.4	Acoustic waves: solution . . . . .	26
3.5	Acoustic power and energy . . . . .	28
3.6	Power conversion in SBS: field perturbation and mechanism of energy exchange . . . . .	31
3.6.1	Impact of electrostriction away from waveguide boundaries . . . . .	33
3.6.2	Field perturbation on waveguide boundaries . . . . .	34
3.7	Acoustic wave equation . . . . .	37
3.7.1	Relation between the defined overlap integrals . . . . .	39
3.8	Optical forces in waveguides . . . . .	40
3.8.1	Electrostrictive force . . . . .	40
3.8.2	Radiation pressure . . . . .	43
3.9	SBS gain in a translationally invariant waveguide in the steady state . . . . .	45
3.10	Coupled equations in the presence of linear loss . . . . .	47
3.11	Coupled equations in the presence of nonlinear loss . . . . .	51
3.11.1	Simplified equations for intramode SBS . . . . .	55
3.12	Coupled equations: Solutions in the presence of nonlinear losses . . . . .	55
3.13	Solution in the case of small signal approximation . . . . .	57
3.13.1	Case study: Only linear loss and FCA exist in a waveguide . . . . .	58
3.14	Appendix: Derivation of the coefficient $\sum^{\text{TPA}}$ . . . . .	60
3.15	Appendix: Derivation of the coefficient $\sum^{\text{FCA}}$ . . . . .	61

<b>4</b>	<b>SBS in hybrid slot waveguides</b>	<b>62</b>
4.1	Introduction . . . . .	62
4.2	Formalism . . . . .	63
4.2.1	Definitions and gain . . . . .	63
4.2.2	Optical parameters of SBS gain . . . . .	64
4.3	Slot waveguide on substrate . . . . .	67
4.3.1	Cancellation of radiation pressure . . . . .	71
4.3.2	Geometry optimization . . . . .	71
4.4	Slot waveguides with silica cover . . . . .	73
4.5	Impact of optical losses . . . . .	75
4.5.1	Computation of nonlinear losses in slot waveguides . . . . .	77
4.6	Conclusion . . . . .	79
4.7	Appendix: The derivation of the optimum waveguide length . . . . .	81
<b>5</b>	<b>SBS amplifiers in integrated ring resonators</b>	<b>82</b>
5.1	Introduction . . . . .	82
5.2	Governing equations . . . . .	84
5.3	SBS in ring resonators with linear loss . . . . .	89
5.3.1	SBS with linear loss . . . . .	89
5.3.2	SBS with linear loss and pump depletion . . . . .	90
5.3.3	Maximum Stokes transmission in presence of pump depletion . . . . .	92
5.4	SBS in ring resonators with Linear and nonlinear effects . . . . .	95
5.4.1	Simplifying the nonlinear model . . . . .	99
5.5	Conclusion . . . . .	105

5.6 Appendix: Impact of third- and fifth-order dispersion on SBS in ring resonators . . . . .	106
5.6.1 Dispersion . . . . .	108
5.6.2 Impact of tolerance of the ring length on SBS . . . . .	110
<b>6 SBS lasing in ring resonators</b>	<b>111</b>
6.1 Introduction . . . . .	111
6.2 Geometry and numerical computations . . . . .	113
6.3 Thresholds for rings with linear loss only . . . . .	117
6.4 Thresholds for rings with both linear and nonlinear losses . . . . .	122
6.5 Conclusion . . . . .	129
6.6 Appendix: The derivation of the optical quality factor . . . . .	130
<b>7 Conclusion</b>	<b>131</b>
<b>Bibliography</b>	<b>135</b>

# List of Figures

2.1	(a) Schematic of the (Backward) SBS process. Pump and Stokes enter the waveguide in opposite (for BSBS) directions. (b) An acoustic wave is excited and starts propagation in the direction of pump. (c) In terms of optical properties, a traveling refractive index forms in the waveguide which causes pump scattering and red-shifting to the Stokes. (d) Energy diagram for Brillouin scattering. In SBS, pump photons loose energy by releasing an acoustic phonon, hence are converted to Stokes photons. . . . .	6
2.2	Dispersion diagrams showing (a) intra mode (b) inter mode scenarios between optical modes in SBS. (c) is the acoustic dispersion diagram of the four situations shown in (a) and (b). In (a) an optical mode in forward and backward propagating are shown. In forward coupling (red vector), both pump and Stokes reside in the same mode. The acoustic wave vector resulting from this interaction —shown in (c)— is very small ( $\approx \frac{\omega_1 - \omega_2}{c} n_{\text{eff}}$ ). In contrast, in backward coupling (green vector) the acoustic wave vector is approximately $q = 2\beta$ . In the case of inter mode coupling pump and Stokes carry different optical modes as shown in (b). . . .	7
2.3	The Lorentzian of the SBS gain measured in a chalcogenide rib waveguide. Picture from [12]. . . . .	8
2.4	Waveguide geometries for harnessing SBS in chip-scale. Picture from [2]. . . . .	11

2.5	(a) A silicon nanowire on a tiny pillar with cross section dimensions shown in (b). (c) The Lorentzian SBS gain of the structure. The inset shows the profile of depleted anti-Stokes photons. Picture from [46]. . . . .	13
2.6	(a) Dual side-modulated optical signal as in input of the filter, containing out of phase but unequal sides. (b) SBS gain amplifies the weaker side at the gain resonance to reach the same amplitude as in the strong side. (c) The modified signal is sent to a high speed photodetector for direct detection. (d) At the frequency where amplification has occurred, sideband have equal amplitude but opposite signs. Therefore, they cancel each other and leads to a significant suppression. . . . .	15
2.7	Data storage process in an optical fiber. (a) A short write pulse acting as Stokes seed and interfere with the data pulses. (b) Through the SBS process, data pulse is depleted, write pulse is enhanced and an acoustic wave is generated which travels opposite to the write pulse. (c)A read pulse enters and (d) retrieve the data pulse Credit: Z. Zhu [65]. . . . .	16
3.1	Schematic of translationally invariant waveguide along $z$ . Pump, Stokes and acoustic waves with their parameters and direction — in BSBS — are shown. . . . .	22
3.2	Types of acoustic waves in a waveguide. (a) compressional (b) Shear waves. Picture from [81] . . . . .	26
3.3	Pure longitudinal acoustic modes in a suspended silicon nanowire with cross section dimensions $300[\text{nm}] \times 210[\text{nm}]$ . . . . .	29
3.4	Pure shear acoustic modes in a suspended silicon nanowire with cross section dimensions $300[\text{nm}] \times 210[\text{nm}]$ . . . . .	29

3.5	Acoustic modes in a suspended silicon nanowire with cross section dimensions $300[\text{nm}] \times 210[\text{nm}]$ . . . . .	30
3.6	(a) Schematic of a typical waveguide in two different situations; no strain and under strain. (b-d) Waveguide boundary deformed by electrostriction and radiation pressure; (b) Before deformation (c) deformed by only electrostriction (d) deformed only due to radiation pressure. . . . .	33
3.7	The field components (a) $\text{Re}E_x$ , (b) $\text{Re}E_y$ and (c) $\text{Im}E_z$ of the fundamental optical mode in a suspended silicon waveguide with cross section dimensions $300 [\text{nm}] \times 220 [\text{nm}]$ . Electrostrictive force components (d) $\text{Re}(f_x^{(\text{ES})})$ (e) $\text{Re}(f_y^{(\text{ES})})$ and (f) $\text{Im}(f_z^{(\text{ES})})$ in an intra mode BSBS process. Pump and Stokes optical modes carry fundamental mode as shown in (a-c). . . . .	40
3.8	Electrostrictive boundary forces in intra mode BSBS process in the suspended silicon waveguide with geometry and optical mode profile described in Fig. 3.7. . . . .	41
3.9	Radiation pressure on boundaries of the suspended silicon waveguide with geometry and optical mode profile described in Fig. 3.7(a-c) in an intra mode BSBS process. (a) and (b) show the relative direction and magnitude of forces $F_x^{(\text{RP})}$ and $F_y^{(\text{RP})}$ , respectively. (c) and (d) shows the absolute value of the two forces. . . . .	44
3.10	(a) Backward SBS gain for an intra mode coupling between pump and Stokes in the suspended silicon waveguide. (b) Absolute values of the overlap integrals $Q_1$ , $Q^{(\text{ES})}$ , $Q^{(\text{ESP})}$ and $Q^{(\text{RP})}$ for the BSBS process with the SBS gains shown in (a) . In both figures, the waveguide geometry and mode profiles are as shown in Fig. 3.7. . . . .	47
3.11	(a)Variation of Stokes power in BSBS process in a waveguide with $\alpha = 1[\text{dBcm}^{-1}]$ , $L = 4 \text{ cm}$ for $ gP^{(1)}(0)  = \{15, 40, 60\} [m^{-1}]$ . (b) Stokes amplification $\mathcal{A}$ in [dB] as a function of $\alpha L$ and $\frac{gP^{(1)}(0)}{\alpha}$ . . . . .	50

3.12	Stokes power variation in a waveguide with $L = 4$ cm in FSBS at different values of SBS gains. Small signal approximation is applied. .	59
3.13	contours of Stokes amplification for a waveguide with (a) $\mathcal{F} = 1.5$ and (b) $\mathcal{F} = 2$ for a range of $\alpha L$ and $U$ . . . . .	60
4.1	Schematic of a silicon chalcogenide slot waveguide . . . . .	62
4.2	Hybrid silicon chalcogenide slot waveguide on a silica substrate. Top panel: sketch of the geometry. Bottom panel: The transverse profile of the fundamental optical mode as well as the displacement field components and the acoustic frequency of three lowest order acoustic modes that can propagate in the waveguide. The waveguide dimensions are $a = 250$ nm, $b = 190$ nm and $c = 150$ nm. .	68
4.3	BSBS gain of the acoustic modes described in Fig.4.2. The gain is obtained by assuming the acoustic quality factor of 1000. The profile of acoustic power is shown for the three lowest modes. . . . .	69
4.4	(a) BSBS gain (red graph) in slot waveguide with $a = 250$ nm and $b = 190$ nm in a logarithmic scale . Gain is obtained only for the high gain acoustic mode. The green (blue) curve shows the gain when only radiation pressure (electrostriction) is considered in calculations. (b) Variation of acoustic frequency of the acoustic mode with slot gap width (blue curve) in Rayleigh surface waves. The red curve shows variations of the frequency as the slot gap varies from 240 nm to 85 nm assuming that $a = 250$ nm and $b = 190$ nm. . . . .	70



4.5	Interactions of radiation pressure and acoustic displacement fields in the overlap integral. (a) The transverse boundary forces due to Pressure (i.e $T_{xx}$ and $T_{yy}$ ). (b) The product of $\mathbf{F} \cdot \mathbf{u}^*$ is positive (negative) in vertical (horizontal) gap wall, regardless of the gap width. As the gap width increases, $\int \mathbf{F} \cdot \mathbf{u}^* dy$ decreases on the vertical walls [see Fig. 4.5.b (right and left)]. However, the integral does not change on horizontal walls i.e reduction in the overlap integral is compensated as the gap width is enlarged. . . . .	72
4.6	BSBS gain in [ $\text{W}^{-1}\text{m}^{-1}$ ] for a slot waveguide with (a) $c = 200$ nm and (b) $b = 220$ nm. . . . .	73
4.7	Profiles of optical and acoustic modes corresponding to the largest BSBS gain in a silicon chalcogenide slot waveguide with $a = 220$ nm and $a = 220$ nm at the the gap widths $c = 150$ nm, $200$ nm and $250$ nm. The field components are normalized to $1$ W. . . . .	74
4.8	slot waveguide with top layer . . . . .	75
4.9	(a) Comparison of the BSBS gain for silica cover layers with thicknesses $0$ nm, $50$ nm, $100$ nm and $150$ nm in a slot waveguide with $a = 250$ nm and $b = 190$ nm. The sketch of the geometry is shown on the right side. (b) Variation of BSBS gain in a slot with the gap width of $c = 160$ nm and similar silicon beam dimensions as in (a). . .	76
4.10	Nonlinear loss coefficients $\beta$ and $\gamma$ for two slot waveguides as a function of the gap size. The red curves in (a) and (b) shows the loss coefficients for slot with $a = 220$ nm and $b = 220$ nm, the blue curve shows the same for a waveguide with a silica cover with $150$ nm thickness. . . . .	78

4.11 (a) The Figure of merit for four slot waveguides, including two slots and two slots with silica cover ( $t = 150$  nm). The silicon beams have fixed dimensions for all the structures ( $a = 220$  nm and  $b = 220$  nm). The linear loss of  $\alpha = 2.3$  m<sup>-1</sup> and  $\alpha = 11.5$  m<sup>-1</sup> are considered in finding the figures of merit. (b) The Stokes amplification corresponding to the waveguides described in (a). The waveguides have optimum lengths. . . . . 79

5.1 Schematic of a ring resonator in vicinity of a straight coupler. The length of the coupling region  $L_c$  is assumed to be considerably smaller than  $L$ . . . . . 85

5.2 Illustration of the transmission spectrum of a ring resonator. Pump and Stokes are assumed to be on resonance (red arrows). The smallest length of a ring designed for SBS applications corresponds to the case that the pump and Stokes frequencies lie on consecutive resonances of the ring (see (5.17)). . . . . 87

5.3 (a) Example of the Stokes amplification in a ring resonator for a range of input pump powers varying from 24 mW to 32 mW. The linear loss is assumed to be 1.5 dB/cm;  $\Gamma = 400$  W<sup>-1</sup>m<sup>-1</sup>;  $L$  and  $L_c$  are 1.745 cm and 7.476  $\mu$ m, respectively and  $|\kappa_1|$  is 0.6. The impact of pump depletion is ignored. (b) Contours of the  $(\Gamma/\alpha)P_p^{\min}$  in natural units at the resonance frequency. It is assumed that the ring is designed according to the method demonstrated in section 2. . . . . 89

5.4 (a) The Stokes transmission of four ring resonators with different SBS gains as a function of input pump power at the resonance frequency. The dot-dashed lines shows the Stokes gain in the absence of the pump depletion term. Moreover, the right hand side of the vertical line in each case shows the lasing region.  $|\kappa_1|$  is 0.312;  $f_B = 6.25$  GHz;  $R_p = 10^{-5}$  and  $L$  and  $L_c$  are 7.419 mm and  $10 \mu\text{m}$ , respectively. (b) The contour of the variation of  $T_{s,r}$  in dB for ring resonators with linear losses at a range of coupling coefficients. The solid- circle line shows the critical coupling corresponding to  $|\tau_1| = \exp[-\alpha L/2]$ . . . . . 93

5.5 Stokes amplification of a ring resonator at different frequency shifts from the resonance . It is assumed that  $\alpha = 1.5$  dB/cm;  $\Gamma = 400 \text{ W}^{-1}\text{m}^{-1}$ ,  $f_B = 15$  GHz;  $R_p = 10^{-5}$  and  $|\kappa_1| = 0.3$ . The ring circumference is 7.8 mm with  $L_c = 10 \mu\text{m}$ . . . . . 95

5.6 (a) Example of the Stokes transmission for a ring resonator with  $\alpha$  varying from 0.5 dB/cm to 0.9 dB/cm. The FCA is assumed to be  $\gamma = 1 \times 10^5 \text{ W}^{-2}\text{m}^{-1}$ . The free carrier dispersion is also included in numerical computations. In this case silicon is assumed to be the source of FCD. (b) Stokes transmission plots of a ring resonator at different initial Stokes powers.  $\Gamma = 3000 \text{ W}^{-1}\text{m}^{-1}$  and the input pump power is 6 mW for both figures. . . . . 98

5.7 Typical Stokes gain  $G_{s,r}$  graphs of ring resonator with linear and nonlinear losses. In all three graphs the linear loss is assumed to be 1.5 dB/cm,  $|\kappa_1| = 0.312$  and  $\Gamma = 1300 \text{ W}^{-1}\text{m}^{-1}$ . The FCA coefficient  $\gamma$  for the ring with nonlinear loss is assumed to be  $1.5 \times 10^4 \text{ W}^{-2}\text{m}^{-1}$ . The black line shows the upper limit of the gain that is equal to  $|\tau_2|^{-1}$  according to (6.9). . . . . 99

5.8	Maximum Stokes transmission $T_s$ and the corresponding optimal value of inverse $U$ as a function of $\mathcal{F}$ and $\alpha L$ in a ring resonator with linear and nonlinear (FCA) losses at $\kappa_1 = 0.45$ . It is assumed that for the Stokes gain over 20 dB the simplified nonlinear model is no longer valid. The white line shows the zero dB transmission (see (5.60)). . . . .	102
5.9	Maximum Stokes transmission of a ring resonator with linear and nonlinear (FCA) loss at resonance frequency for (a) $\mathcal{F} = 1.1$ , (b) $\mathcal{F} = 1.25$ , (c) $\mathcal{F} = 1.5$ and (d) $\mathcal{F} = 1.75$ . It is assumed that for the Stokes gain over 20 dB can not be estimated correctly with the simplified nonlinear model. The green solid-circle line shows the critical coupling. . . . .	103
5.10	Typical pump transmission spectrum for a ring resonator. The dashed blue shows the pump transmission in the absence of dispersion. In presence of dispersion the transmission is slightly shifted as shown in the solid pink curve. . . . .	106
5.11	(a) The normalized change of the silicon refractive index of a waveguide as a function of input pump intensity at different values of $H$ defined in inset. We have assumed that the free carrier lifetime, $\tau_{lt} = 10$ ns, $\beta_{\text{TPA}} = 5 \times 10^{-12}$ m/W at the wavelength $\lambda_p = 1550$ nm. (b) The impact of the ring length tolerance on the Stokes amplification of a ring resonator with the linear and FCA losses in the small signal approximation regime. The loss coefficients of $\alpha = 1.5$ dB/cm and $\gamma = 1 \times 10^5$ W <sup>-2</sup> m <sup>-1</sup> . The coupling coefficient $\kappa_2$ is 0.4, $L_R = 5.79$ mm and the Brillouin linewidth is assumed to be 30 MHz. The input pump power in each case is assumed to be its optimal value. . . . .	107
6.1	Schematic of a ring resonator in vicinity of a straight coupler. . . . .	114

- 6.2 Output Stokes power as a function of input pump power at the lasing region and resonant condition in the presence of (a) linear losses and (b) both linear and nonlinear losses. In (a)  $\Gamma = 500 \text{ W}^{-1}\text{m}^{-1}$ ,  $R = 10^{-11}$  and  $\kappa = 0.31$ . In (b)  $\alpha L = 0.2$ ;  $\gamma = 1.8 \times 10^5 \text{ W}^{-2}\text{m}^{-1}$ ,  $\beta = 10 \text{ W}^{-1}\text{m}^{-1}$ ,  $\kappa = 0.16$  and  $\Gamma = 4000 \text{ W}^{-1}\text{m}^{-1}$ . The length  $L = 10.879 \text{ mm}$  corresponds a ring resonator with free spectral range equal to a Brillouin frequency shift of 10 GHz. . . . . 116
- 6.3 (a) Schematic variation of the round-trip gain in a ring resonator with linear loss within the SSA and full model. (b) The corresponding Stokes total amplification of a ring resonator with the parameters described in Fig. 6.2(a). The solid circle lines show  $\mathcal{A}$  for the small signal model. . . . . 119
- 6.4 (a) Contours of the lasing threshold as a function of  $\alpha L$  and the coupling coefficient. The dashed line shows the critical coupling. (b) The threshold difference  $\Delta P_{\text{p}}^{\text{in,th}}$  between the power obtained by Eq. (6.13) with the threshold estimated from 6.15, plotted for a range of the coupling coefficient  $|\kappa|$  and for different values of  $\alpha L$ .  $\Delta P_{\text{p}}^{\text{in,th}}$  is normalized to the exact theoretical value of the threshold (i.e. Eq. (6.13)) and is plotted in percentage. . . . . 121

- 6.5 (a) Schematic variation of the round-trip gain in a ring resonator with nonlinear loss in three different operating regimes shown in pink (with two lasing thresholds), green (with single threshold) and blue (no lasing). Dashed lines show the result of the small signal model and the solid lines are expected in the full model. (b) An example of the Stokes output power for a ring with two lasing thresholds. The black dotted lines shows the SSA. The results of the full model are also shown for different values of the power ratio  $R$ . for a ring with the SBS gain and loss parameters described in Fig. 6.2(b). (c) The Stokes output power for a ring with parameters which leads to a single lasing threshold.  $\Gamma = 5970 \text{ W}^{-1}\text{m}^{-1}$ ;  $|\kappa| = 0.24$ ;  $\alpha = 40.9 \text{ m}^{-1}$  and  $\gamma = 1.8 \times 10^5 \text{ W}^{-2}\text{m}^{-1}$ . (d) The Stokes output power in a ring with parameters that leads to only Stokes amplification.  $\Gamma = 5700 \text{ W}^{-1}\text{m}^{-1}$  and the loss and coupling parameters are as in (c). . . . . 123
- 6.6  $V^{\min}$  and  $V^{\max}$  at the lasing threshold as a function of  $\kappa$  and  $\alpha L$  for (a,b)  $\mathcal{F} = 1.1$  and (c,d)  $\mathcal{F} = 1.5$ . . . . . 125
- 6.7 Minimum/Maximum values of the lasing threshold in mW as a function of  $\kappa$  and  $\alpha L$  for  $\mathcal{F} = 1.1$  (a,b) and  $\mathcal{F} = 1.5$  (c,d) for  $\frac{\alpha}{\gamma} = 2 \times 10^{-4} \text{ W}^2$ . . . . . 126
- 6.8 Lasing thresholds as a function of the coupling coefficient for different values of  $\mathcal{F}$ .  $\alpha L$  is assumed to be 0.3 and  $\alpha/\gamma = 2 \times 10^{-4} \text{ W}^2$ . 128
- 6.9 The normalized input pump power corresponding to the maximum Stokes output in the lasing regime for a range of  $\alpha L$  and SBS figure of merit.  $|\tau|$  is assumed to be 0.9. (b) The maximum Stokes output in mW. The initial Stokes is assumed to be 1 pW. . . . . 128

# Abbreviation

CW - Continuous Wave

SBS - Stimulated Brillouin Scattering

BSBS - Backward Stimulated Brillouin Scattering

SSA - Small Signal Approximation

TPA - Two Photon Absorption

FCA - Free Carrier Absorption

FCD - Free Carrier Dispersion

FSR - Free Spectral Range

SMF - Single Mode Fiber

Mid-IR - Mid- Infrared

WGR - Whispering Gallery Resonator