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Quadrature Broadband Phase Shift Generation Using Passive RC Polyphase Filter for RF Front-end

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Abstract - This paper reviews the state of art of a polyphase complex filter for RF front-end low-IF transceivers applications. We then propose a multi-stage polyphase filter design to generate a quadrature I/Q signal to achieve a wideband precision quadrature phase shift with a constant 90° phase difference for self-interference cancellation circuit for full duplex radio. The number of the stages determines the bandwidth requirement of the channel. An increase of 87% in bandwidth is attained when our design is implemented in multi-stage from 2 to an extended 6 stages. A 4-stage polyphase filter achieves 2.3 GHz bandwidth.

Keywords: Phase shift, Polyphase filter, Quadrature, RF Front-end, 90° phase

I. INTRODUCTION

Wireless communications traffic demand is expected to increase by more than 1000-fold in the next decade. To serve this ever-increasing demand, it is of great interest for RF designers to design integrated circuits that are more power/energy efficient with smaller footprint and lower implementation cost [1]-[3]. Since it contains both analogue and digital circuitry, the integration of RF, analogue and baseband in a single chip has always been a critical challenge [4]. Emerging mobile communications (e.g., LTE-Advanced, 5G) demands for extremely high data rate (peaks at 10Gbps) and ultra-low latency (e.g., in order of ms or less) [5][6]. For many years, there have been several efforts in developing single wireless transceivers that integrates both transmitter and receiver on chip. Some of the pioneers who made their contributions in theory and practical implementation of transceivers on chip are Abidi [7], Lee [8] and Steyaert [9]. This led important improvements in design implementation and development of new circuit architecture [5].

The high volume of data traffic in the network will be a big challenge. Full Duplex (FD) technology is considered to be a key technique to potentially double the speed of wireless communication on between a transmitter and a receiver, allowing the transmission and reception of data on the same frequency band [10]. In achieving full duplex transmission, a radio has to completely cancel out the self-interference that is present in the system. If self-interference is not completely cancelled, a residual interference reduces the signal to noise ratio (SNR), reducing the overall throughput of the Full Duplex radio and thus degrading the efficiency of the system [11].

Radio transceivers require a complex filter to eliminate unwanted signals. These are important building blocks in many analog front-end receivers [12]-[17]. Resistor-

Capacitor (RC) Polyphase filter (PPF) is one of the complex filters that can be implemented. Its RC network is suitable for high frequency design [22]. In radio frequency (RF) applications, the performance of passive polyphase filter in terms of image rejection and quadrature signal generation depends on the component mismatch [18][19].

There are various methods to generate the quadrature I/Q signal. For Low-IF architecture, resistor Capacitor polyphase filters are often more favourable thanks to their simple implementation and convenience for high frequency application where high level of integration is required [18]. The capability of RC polyphase filters to provide a required performance in a wide frequency range is critical for the application of double-quadrature low-IF architectures in a multi-standard receiver [24] and transceivers. Furthermore, polyphase filter can be used as a phase shifter by varying the output amplitude, while using a variable gain amplifier (VGA) and combining them to change the phase of the output signal.

This article presents the design consideration and performance of a multi-stage polyphase filter to generate a wide bandwidth quadrature I/Q phase shifter for self-interference cancellation circuit for full duplex radio. The precise quadrature phase shifting is suitable for broadband low-IF RF front-end transceivers with interference cancellation mechanism. This design is simulated using BiCMOS 0.13µm process [28]. The rest of the paper is organized as follows. The concept of complex mixing and quadrature phase shift are in Section II. A polyphase filter design is adopted to generate the precise quadrature in Section III. The simulation results and comparison in Section IV and conclusions are drawn in Section V.

II. COMPLEX MIXING

One important issue in receiver design is to suppress any unwanted signal prior to mixing operation. This unwanted input signal band which will be superimposed on the desired signal after mixing is referred as the image signal band. An image rejection filter implements this process. To avoid image problem that is due to the positive and negative frequencies is to mix the signal with the complex exponential that can be express as

$$e^{-j2\pi f_{LO}t} = \cos(2\pi f_{LO}t) - j\sin(2\pi f_{LO}t). \quad (1)$$

The output of mixing the real signal to the complex exponential gives a shifted version of the real signal spectrum, due to this shifting mechanism it help to eliminate the image problem. Mixing of the two signals as shown in Fig. 1, gives us the following equations;

$$y_r(t) = x_r(t) \cdot z_r(t) - x_i(t) \cdot z_i(t) \quad (2)$$

$$y_i(t) = x_r(t) \cdot z_i(t) - x_i(t) \cdot z_r(t). \quad (3)$$

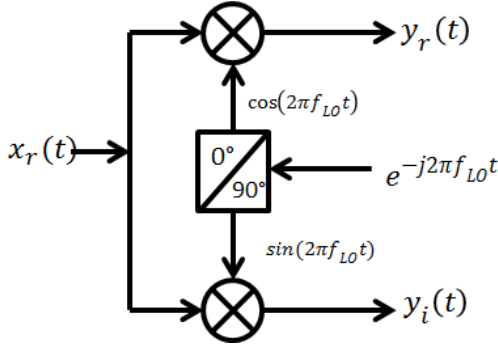


Fig. 1 Mixing real signal with complex exponential

The frequency transfer function of the polyphase filter is not symmetrical to the zero frequency. As such this characteristic of PPF is used in transceiver circuits to implement frequency mixing to reduce the non-idealities in the image signal. It is also used to produce balance quadrature signal at the output.

The 90° hybrid is implemented using a lumped element passive RC polyphase filter. Polyphase filters are also known as complex filters. Their magnitude response is a function of both the input frequency and phase. The input of the complex filter represents the real and imaginary part of the signal. In RF receiver/transceiver the signal is created by separating the I (In-phase) and Q (Quadrature) components through the process of down conversion. Image rejection can be implemented using a polyphase filter [25].

Quadrature generation is widely used in many RF transceiver designs. It is important to consider the accuracy to generate 90° phase shift signal since it is the key attribute to determine the image rejection ratio (IRR) which is equally important to define the transceiver sensitivity [9]. There are different techniques to generate a quadrature shift signal, e.g., frequency division, Haven's technique, RC-CR network and RC-PPF networks. In this design, the RC-Polyphase network is adopted to perform quadrature phase shift.

III. POLYPHASE FILTER

In theory, polyphase filter can cancel the image signal. An image signal is any frequency other than the selected radio frequency carrier that, if allowed to enter the transceiver it will mix with the oscillator and produce a crossed product frequency that is equal to the IF signal. The simple series connection of RC sub-networks that is composed of a ring of resistors and capacitors is arranged alternately to help eliminate the image signal. A simple PPF has 4 inputs and 4 outputs. The phase difference between each port is 90°. The main purpose of this architecture is to generate four (4) quadrature signals that are required in image reject receiver or SSB modulators [20]. These receivers have the ability to pre-select and reject the image frequencies. The maximum image rejection depends on the performance of the PPF circuit, thus it is

crucial to test its functionality and perform optimization prior to the system level design [18]. The accuracy of RC network will determine the filtering performance. One drawback of PPF when implemented on chip is its large chip size [21].

A single-Stage RC Polyphase filter is depicted in Fig. 2 contributing to one pole frequency called notch, where the image is attenuated around the area. It can be express as:

$$f_{pole} = \frac{1}{2\pi RC}. \quad (4)$$

The transfer function $H(\omega)$ can be expressed as:

$$H(\omega) = H_1(\omega) + j H_2(\omega) \quad (5)$$

The positive sequence voltage transfer function can be written as:

$$H(\omega) = A \frac{1 - \omega RC}{1 + j\omega RC} \quad (6)$$

and the negative sequence voltage transfer function is written as:

$$H(-\omega) = A \frac{1 + \omega RC}{1 + j\omega RC}. \quad (7)$$

The characteristic gain of RC PPF depends on the combination of RC values and the magnitude of the zeros. Thus for PPF design, the value of R and C, the order of the location of the zero and the magnitude of each zero must be taken into consideration [22].

The input and output I/Q equation is defined as

$$I_{in} = I_{in+} - I_{in-} \quad (8)$$

$$Q_{in} = Q_{in+} - Q_{in-} \quad (9)$$

$$I_{out} = I_{out+} - I_{out-} \quad (10)$$

$$Q_{out} = Q_{out+} - Q_{out-}. \quad (11)$$

The output of the polyphase filter is a differential quadrature, I_{out+} , I_{out-} , Q_{out+} and Q_{out-} respectively. PPF output is usually followed by a differential amplifier to improve the dynamic range.

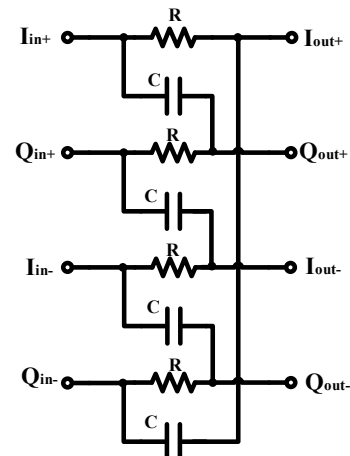


Fig. 2 Single-stage RC polyphase filter network

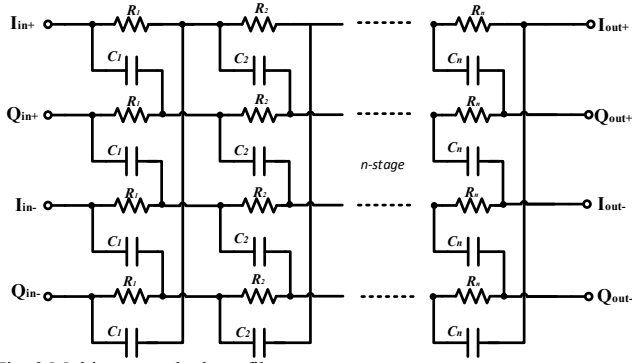


Fig. 3 Multi-stage polyphase filter

Fig. 3 shows the multiple stage polyphase filters, the cascading n -stage RC network can produce 0° , 90° , 180° and 270° respectively. By increasing the number of RC stages, we can improve the image rejection ratio (IRR). The required number of stages determines the bandwidth requirement of the channel. The PPF can provide good constant gain matching and quadrature precision. However, one drawback of the multi-stage design is the large layout area or chip footprint for wideband application [25].

A single PPF contributes one-pole frequency at which the image signal is attenuated; however it provides a narrowband rejection. A wider bandwidth can be accomplished by cascading a multi-stage PPF. The notches that the multi-stage PPF have are placed at the equal frequency ratio, given the following equation:

$$\alpha = \frac{f_{p2}}{f_{p1}} = \frac{f_{p3}}{f_{p2}} = \frac{f_{pn}}{f_{p3}} \quad (12)$$

Wherein the pole frequency ratios α are equal. For a better image rejection, a smaller α ratio is desired.

A. PPF Excitation

To make use of the four-phase I/Q signal, the input terminals must be connected in a proper way. There are two input feeding topologies or PPF excitations. Type I generates constant amplitude, the input asymmetric polyphase sequence consists a pair of phasors which have the same magnitude but phase difference of 180° . Type II has constant phase. The input asymmetric polyphase sequence is composed of two identical pairs of phasors where each pair has the same magnitude but they are separated by 180° . Type II excitation has a loss of about 3dB less than type I [18][20][24].

The differential voltage can be express as

$$V_I = V_{i_{out+}} - V_{i_{out-}} \quad (13)$$

$$V_Q = V_{Q_{out+}} - V_{Q_{out-}} \quad (14)$$

In type I the magnitude (A) and the phase (ϕ) is defined as;

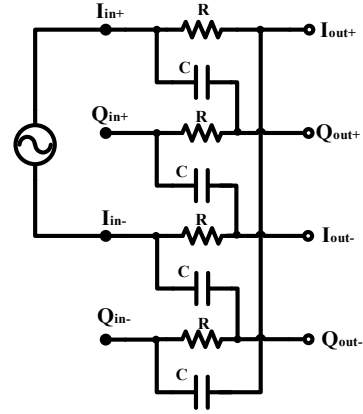
$$A = \frac{1}{|\omega RC|} \quad (15)$$

$$\phi = -\frac{\pi}{2} \quad (16)$$

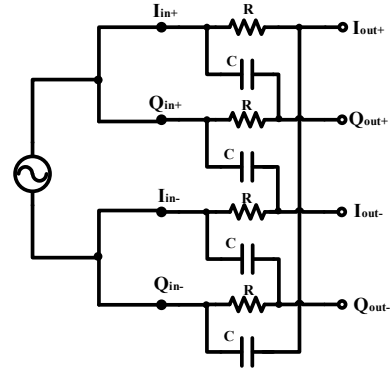
In type II the magnitude (A) and the phase (ϕ) is defined as;

$$A = 1 \quad (17)$$

$$\phi = \arctan \left(\frac{-2\omega RC}{1-(\omega RC)^2} \right) \quad (18)$$



(a) Type I
(b)



(b) Type II

Fig. 4 Polyphase filter input feeding excitation

B. PPF Termination

There are two ways to terminate a polyphase filter as discussed in [23]. The first method in Fig.5(a) shorted pairwise output, where I_{out+} is shorted to Q_{out+} and Q_{out-} is shorted to I_{out-} , respectively. In the second method Fig.5(b) one output pair termination in dummies, where the differential output signal from $I_{Q_{out+}}$ and $I_{Q_{out-}}$ is terminated using a dummy capacitance.

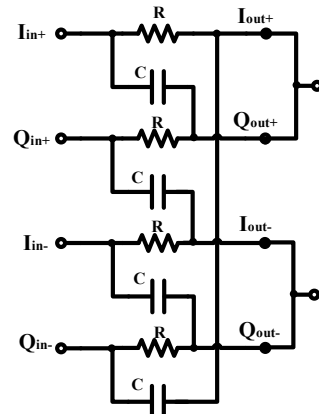


Fig.5(a) Shorted pairwise output termination

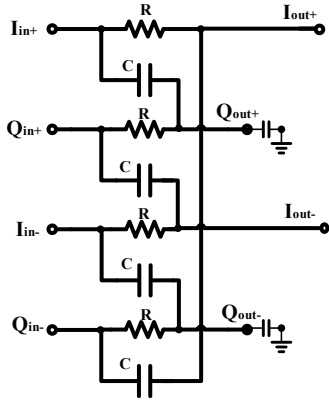


Fig. 5(b) One output pair termination

IV. SIMULATIONS

As shown in Fig. 6, the output of each of the I/Q port of the PPF shifter is in quadrature with respect to other branch. The amplitude of the output sinusoidal signals are equal. Fig. 7 shows the simulation of the one stage polyphase filter generating 90° and -90° phase difference from each I/Q branch. Fig. 8 shows the 3 stage PPF I/Q output phase I_{out+} , Q_{out+} , I_{out-} , Q_{out-} , and generate 0° , 90° , 180° and 270° phase difference from each I/Q output branch respectively.

A multi-stage PPF is depicted in Fig.3. By cascading several stages with different notch frequency, a wide bandwidth can be achieved. Simulation of the phase of the I/Q signal is shown in Fig. 7, for 1, 2 and 3 stages respectively and Fig. 8 for 4, 5 and 6 stages respectively. As can be seen, the higher number of the cascading stages, the higher the bandwidth generated by the PPF increases. The bandwidth and the percent increase of each stage are summarizing in Table 1. At 2 stage cascaded PPF, the bandwidth is 0.4 GHz, at 3 stages PPF the bandwidth is 1.517 GHz which is 73.6 % increase in bandwidth as compare to 2 stages PPF. Thus, the required number of the stages determines the bandwidth requirement of the channel. One trade-off of multi-stage PPF is the gain losses generated at previous stage.

A comparison with other polyphase filter designs is given in table 2. Note that the PPF listed are implemented in 4-stages, in these paper the proposed design PPF achieved 2.3 GHz bandwidth.

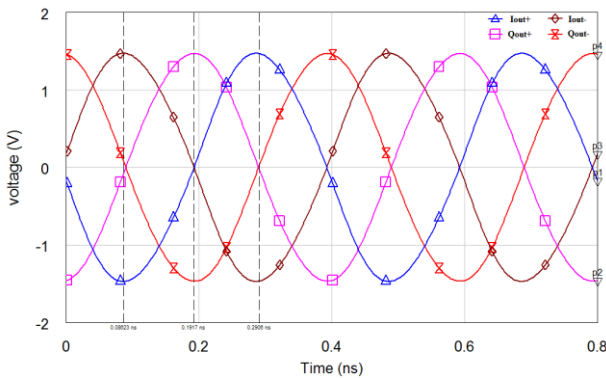


Fig. 6 Output voltage of 3-stage polyphase shifter with ideal differential source with respect to time

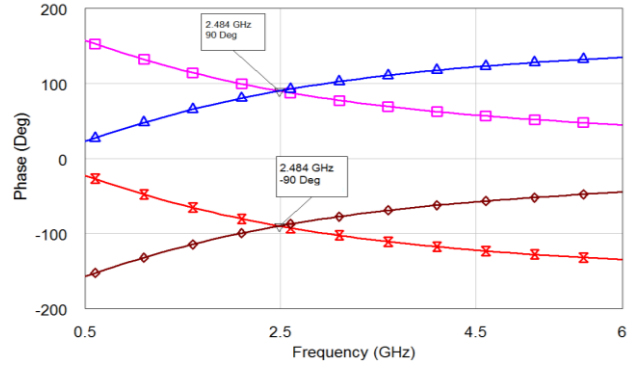


Fig.7 One stage 90° phase difference between I/Q output branch

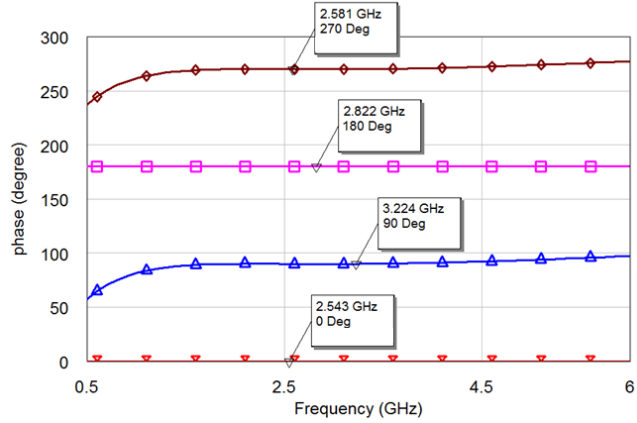


Fig.8 3-stage PPF I/Q output

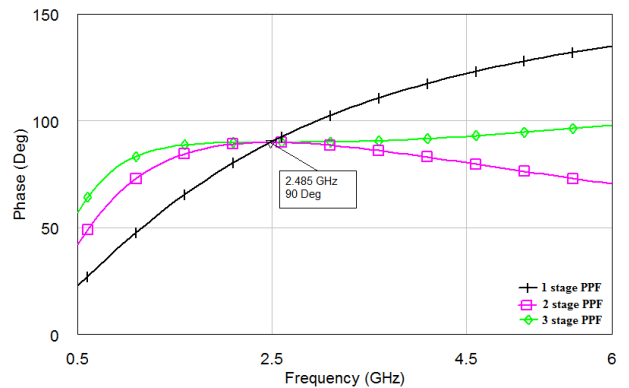


Fig. 9 Simulated phase of the I/Q signal of multi-stage PPF (1,2,3-stages respectively)

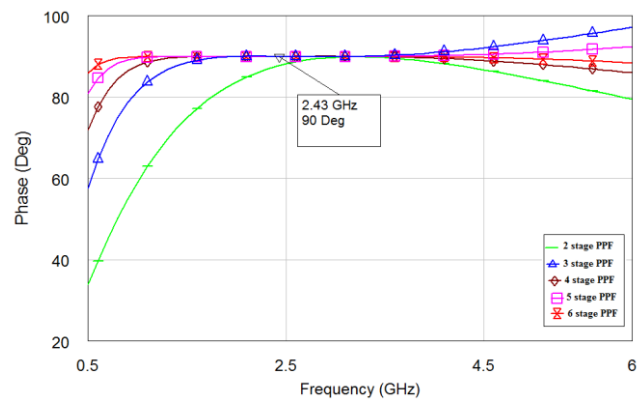


Fig. 10 Simulated phase of the I/Q signal of multi-stage PPF (2,3,4,5 and 6 – stages respectively)

Table1. Summary of the multi-stage bandwidth

Stage	Frequency range (90°)	Bandwidth	% increase
2	2.8 GHz - 3.2 GHz	0.4 GHz	
3	2.033 GHz – 3.55 GHz	1.517 GHz	73.6 %
4	1.405 GHz – 3.709 GHz	2.304 GHz	34.15 %
5	1.129 GHz – 3.96 GHz	2.831 GHz	18.6 %
6	0.95 GHz – 4.1 GHz	3.15 GHz	10.13 %

Table 2 Comparison with previous work

Ref.	[5]	[21]	[26]	[27]	This work
Process (µm)	CMOS 0.13	CMOS 0.35	CMOS 0.13	CMOS 0.25	BiCMOS 0.13
Topology	Passive RC	Active RC	Tunable	Active RC	Passive RC
Stages	4	4	4	4	4
Bandwidth	1.8 GHz	72 MHz	0.5 GHz	24MHz	2.3 GHz

CONCLUSIONS

This paper presents a multi-stage polyphase complex filter design to generate a wide bandwidth quadrature I/Q signal with constant 90° phase shift for self-interference cancellation circuit for full duplex radio. By cascading n-stages passive RC PPF an increase of 87% in bandwidth was attained by implementing 2 to extended 6 stages. A 4-stage PPF achieved 2.3 GHz bandwidth. The broadband PPF was used to eliminate unwanted signal in RF front-end low-IF transceivers with interference cancellation mechanism. However, a multi-stage design has a trade-off with increase complexity, large chip footprints and gain loss.

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