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### Mechanisms of Heavy Metal Immobilisation using Geopolymerisation Techniques – A review

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#### **Abstract**

Every year, substantial amount of waste materials containing toxic substances is produced throughout the world, which causes serious damage to the environment and poses threat to human health. Among available techniques of immobilisation of toxic elements in harmful by-products, geopolymerisation is considered as an effective approach to deal with many environmental issues. Geopolymer binders have long been recognised to have great potential in immobilisation of hazardous wastes due to its advantages over Portland cement based binders. A profound knowledge of how hazardous elements are immobilised by geopolymer binders is necessary for achieving effective waste management strategies. This paper provides some important aspects of geopolymer materials regarding the immobilisation mechanisms and factors influencing the immobilisation efficiency, which are necessary to carry out further research on addressing the hazardous waste immobilisation.

#### 1. Introduction

The rapid industrialisation of many countries, including Vietnam, gives rise to generation of millions of tons of industrial wastes every year and releases undesirable contaminants to the environment. Toxic heavy metal contaminants may be the most dangerous wastes because of their recalcitrant nature (Tchounwou et al. 2012) and the severe damage they cause to human health (Science Communication Unit of University of the West of England 2013). Just a very small proportion of harmful wastes produced is reused while most of it is often disposed of at hazardous landfills. In some cases, stabilisation/solidification methods are applied to immobilise toxic elements in harmful wastes and then the subsequent product is disposed of at non- hazardous landfills, which is very useful to minimize environmental threat. If not stabilised, it may become an issue because hazardous waste disposal on land may lead to serious groundwater pollution problems (Bishop 1988). Apart from industrial waste, heavy metals can also be released from several other sources in the environment, as shown in Fig. 1.

In the immobilisation of heavy metals, binders obviously have a key role to play and Portland cement is,

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<sup>3</sup>Senior Research Fellow, School of Civil and Environmental Engineering, University of Technology Sydney, Broadway, NSW, Australia. often, widely used as the cementitious material in stabilisation/solidification systems because it has low processing costs and the ability to meet stringent processing and performance requirements (Portland Cement Association 1991; Glasser 1997). However, the production of Portland cement not only consumes a large quantity of natural resources and energy but also releases a significant amount of greenhouse gases into the atmosphere (Davidovits 1991, 1994; Neupane 2016). Producing one ton of cement clinker consumes about 3000 MJ of heat energy (although the theoretical value is considered to be about 1750 MJ per ton of clinker) and is very much dependent on the process used. Production of one ton of cement releases nearly one ton of CO<sub>2</sub>. Thus, stabilisation/solidification methods using Portland cement could probably be viewed as half measures and new types of binder are required, in terms of the protection of the environment.

Geopolymer, an amorphous inorganic polymer composed of [SiO<sub>4</sub>] and [AlO<sub>4</sub>]-tetrahedrons linked alternately by sharing all the oxygen (Davidovits 1991), a solid and stable aluminosilicate material formed by alkali hydroxide or alkali silicate activation of a precursor (Duxson *et al.* 2007a), has been valued as a viable alternative to Portland cement in the concrete industry (Davidovits 2005; Duxson *et al.* 2007b; Lloyd and Rangan 2009; Neupane 2016). Since the production of geopolymer materials could enable the reuse of a considerable amount of by-products such as fly ash and slag, generated by industrial activities and reduce the CO<sub>2</sub> emission generated by the production of cement by about 80-90%, geopolymers are ideal materials for immobilisation of toxic wastes.

It was reported that geopolymers have the properties such as high early strength, low shrinkage and improved resistance to alkali-silica reaction, freeze-thaw, sulfate attack and reinforcement corrosion and thus make them ideal for the construction of many structural components including floor slabs of containment disposal facilities (Davidovits 1994). Portland cement based materials are unsuitable for stabilisation of various toxic wastes (especially those containing sodium salts of arsenate, borate, phosphate, iodate and sulfides, salts of magnesium, tin, zinc, copper, and lead), and are also unsuitable for solidification of end-product residues with high sulfide contents (Davidovits 2002). This view was shared by Palomo and de la Fuente (2003) who suggested that excellent performances of geopolymers could be achieved in the immobilisation of certain chemical species. This is because geopolymers exhibit superior properties such as having a favourable pore structure with the abundance of the very small pores, low permeability, very high alkalinity, good chemical stability, and a three-dimensional microstructure. A considerable amount of recent researches on geopolymers reported on the degree of toxic waste immobilisation of geopolymers but only a few have attempted to explain how heavy metals are immobilised in geopolymer matrices. This review paper focuses on the immobilisation mechanisms and possible effects of some important factors such as characteristics of source materials, type and dosage of alkali activator, characteristics of the heavy metal forms, and the microstructure of geopolymers on the metal immobilisation of geopolymer bind-

### 2. Background

#### 2.1 Geopolymerisation / Activation

Geopolymers can be produced from waste and natural aluminosilicate materials such as fly ash, slag, kaolinite, metakaolinite and red mud, through a process called geopolymerisarion, or activation procedure. The chemistry of geopolymerisarion, or activation procedure of different types of source materials was detailed in RILEM State of the Art Reports (Bernal et al. 2014; Provis and Bernal 2014a; Provis et al. 2014). There are some noticeable models for geopolymerisation processes. Firstly, Glukhovsky (1959) described that the alkali activation of materials containing silica and reactive alumina consists of a series of processes, namely, destruction, coagulation, condensation and crystallisation. Many researchers then further developed the Glukhovsky theory and proposed different models for geopolymerisation processes. Palomo and de la Fuente (2003) claimed that the geopolymerisation of raw materials might be related to a set of destructioncondensation reactions that could be divided into three stages: Firstly, bonds such as Si-O-Si, Al-O-Al and Al-O-Si of the raw materials are broken. This process needs a stimulus, for example, the variation of the ion force of the medium when adding ions with electro-donor properties (alkaline metals). It is needed in order to redistribute the electronic density over the silicon atoms and stimulate the Si-O-Si bond to break. The negative electrical load of these anions is balanced by cations of alka-

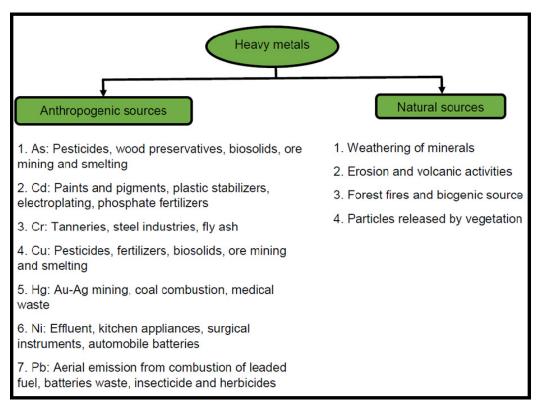


Fig. 1 Sources of heavy metals in the environment (Dixit et al. 2015).

Alkaline activated materials										
Type	I	II	III							
Precursor	High calcium and silican can	Low CaO contents (metakaolin,	A combination of the type I + II (such							
	· ·	type F fly ash)	as a blend of blast furnace slag and							
	tents (blast furnace stag BFS)	type i' iiy asii)	type F fly ash)							
The main reaction product	A calcium silicate hydrate C-S-H	A three- dimensional inorganic								
	gel, similar to the gel obtained	alkaline polymer, a sodium alu-								
	during OPC hydration, with a	minosilicate hydrate N-A-S-H	A mix of C-A-S-H and N-A-S-H gels							
	small percentage of Al in its	gel that is considered as geo-	_							
	structure C-A-S-H gel	polymer gel								

Table 1 The simplification of the source materials and reaction products of alkaline activation processes, based on previous studies (Provis and Bernal 2014b; Palomo et al. 2014; Provis 2014).

line metals, generating alkaline silicates. In addition, these alkaline silicates may react with divalent ions, forming Si-O-Ca-OH type complexes. The Al-O-Si bonds are influenced in the same way, and depending on the pH, complexes of the type Al(OH)<sub>4</sub>-, Al(OH)<sub>5</sub><sup>2-</sup> and Al(OH)<sub>6</sub><sup>3</sup> will be formed. Secondly, de-segregated products accumulate, generating a coagulation structure in which polycondensation processes take place. The final stage of geopolymerisation is the precipitation of products. Duxson et al. (2007) described geopolymeri-

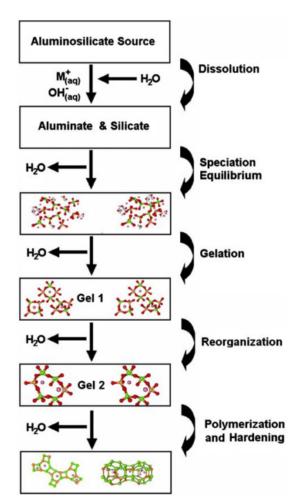


Fig. 2 Conceptual model for geopolymerisation (Duxson et al. 2007). [Reprinted by permission of Springer, Journal of Materials Science, © 2007]

sation process as the multiple gel stages (see Fig. 2).

In Fig. 2, the first stage of the process starts with dissolution of the vitreous component of solid aluminosilicate source by alkaline hydrolysis, and produces aluminate and silicate species. This stage is followed by incorporation of aluminate and silicate species into the aqueous phase. After gelation, a massive precipitation of a rich Al gel (gel 1) occurs. Following that, gel 1 is transformed into a new and more stable gel (gel 2) that is Si-rich. After polymerization and hardening, a synthetic alkali aluminosilicate with three-dimensional network is formed.

According to a recent perspective, geopolymer is deemed as a low calcium subset of the alkaline activated materials (AAMs). AAMs are solid and stable aluminosilicate materials formed by alkali hydroxide or/and alkali silicate activation of a precursor (Provis and Bernal 2014b). There are three types of AAMs, as shown in **Table 1**, primarily depending on the nature of the source materials or precusors, and geopolymer is considered as the type II of AAMs.

Type I and type II have distinct activation procedures and produce different reaction products. The right-hand pathway in Fig. 3 describes the geopolymerisation of low calcium content precursors (type II), while the lefthand pathway shows the activation of high calcium source materials (type I).

The main reaction product of type I activation is a C-A-S-H (calcium-silicate-hydrate) gel (see Fig. 4), while that of type II is a three dimensional inorganic alkaline polymer (zeolite framework) which can be regarded as a zeolite precursor N-A-S-H (sodium aluminosilicate hydrate) (see Fig. 5) or K-A-S-H (potassium aluminosilicate hydrate). Type III is a mix of these two mentioned types, in which C-A-S-H gels co-exist with zeolite precursor N-A-S-H or K-A-S-H under some conditions (Garcia-lodeiro et al. 2011). Due to the zeolite framework within the geopolymeric matrix (see Fig. 5), heavy metals could be locked and the matrix could possess superior mechanical properties and durability.

Red mud is a toxic by-product of the industrial process that refines bauxite, raw aluminum ore, into aluminum oxide, or alumina (Power et al. 2011). Bauxite is a mixture of minerals. In addition to aluminum compounds, it contains iron oxides, sand, clay and small amounts of a form of titanium oxide called anatase; it

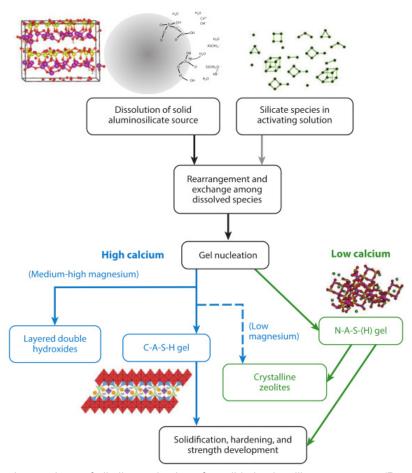


Fig. 3 Process and reaction products of alkaline activation of a solid aluminosilicate precursor (Provis and Bernal 2014b). [Republished with permission of the Annual Reviews,©2014]

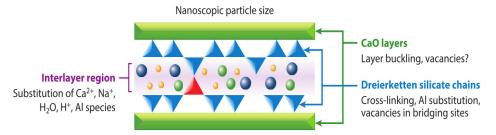


Fig. 4 Tobermorite like C-A-S-H gel structure (Provis and Bernal, 2014b). [Republished with permission of the Annual Reviews,©2014]

can also hold traces of radioactive minerals, such as uranium or thorium compounds (Gu et al. 2017). This raw material is bathed in a solution of a strong base such as sodium hydroxide (lye or caustic soda) at a high temperature and pressure. The aluminum compounds in the bauxite dissolve in the hot caustic solution while the other components remain behind. Everything that does not get dissolved in the process is called red mud, its rusty colour is derived from the iron compounds. The mud also has a high pH because of the sodium hydroxide solution used in the refining process. Apart from some limited use to produce a pigment in the manufacture of bricks (Pera et al. 1997) and cement (Singh et al. 1996; Singh et al. 1997), the red mud is a waste mate-

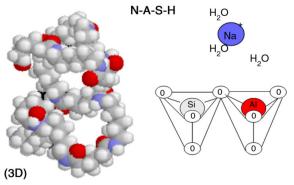


Fig. 5 The three-dimensional structure of a N-A-S-H gel (Palomo *et al.* 2014).

rial. Although it contains useful elements, such as iron, titanium and residual aluminum, there is no economically viable way to extract them from the mud. Most refineries collect the mud in open ponds to allow some of the water to evaporate. Once it is dry, after several years, the red mud is buried or mixed with soil. Some refineries use powerful presses to squeeze the water out of the mud and evaporators to dry most of the rest. Red mud is also used as a source material for geopolymers (He and Zhang 2011). It will be useful to study red mud based geopolymer systems to immobilise toxic wastes.

### 2.2 Method of evaluation of immobilisation efficiency - Leaching test

The efficiency of heavy metal immobilisation is defined basically by strength and the leach resistance (Malviya and Chaudhary 2006). While the strength development is considered as an indicator of solidification, leaching test is probably the most important measure to assess the degree of heavy metal stabilisation. Many leaching methods have been commonly used to acquire useful information for environmental decision-making. Yet, there is no a single leaching test that can assess the leaching behavior of a wide variety of waste materials. Selecting an appropriate leachate test was summarized in the guide of Environmental Protection Agency (Environmental Protection Agency 2011). Palacios and Palomo (2004) studied on three different leaching tests including Modified Static Leaching Test (MCC1-P), Leaching test of the matrices by means of the American National Standard (ANSI/ANS 16.1), and Toxicity Characteristic Leaching Procedure (TCLP) in order to determine the amount of lead fixed by activated fly ash systems. They concluded that the different results obtained from the various leaching tests can be justified according to the nature of each individual test. Each test is found to have advantages and disadvantages regarding evaluating the results, and the major mechanism responsible for lead leaching is diffusion. According to Fernández Pereira et al. (2009), the best results of stabilisation were observed with geopolymers when using the EN 12457 test, whilst the TCLP test showed the best results in OPC samples. Mercury immobilisation efficiencies are consistently higher in TCLP tests than EN 12457 tests (Donatello et al. 2012). This is probably due to the fact that the test material used in TCLP tests are coarser than that in EN 12457, and that the high leachate pH value used in EN 12457 tests possibly increases the solubility of mercury precipitates. Thus, choosing the leaching test method should be taken into account when evaluating the efficiency of heavy metal immobilisation of geopolymer materials. Using more than one leaching test method is strongly recommended.

### 3. Mechanisms for heavy metal immobilisation

In traditional stabilisation and solidification systems,

heavy metals are generally converted to low solubility precipitates such as carbonates, hydroxides, silicates, or sulfides, and then formed as a solid with solidification reagents (Portland Cement Association 1991). According to Shi and Spence (2004), there are three aspects in the stabilisation and solidification by cements. The first two aspects rely on the nature of the hydration products, including chemical fixation of contaminants and physical adsorption of the contaminants on the surface of hydration products of the cements (see Fig. 6). The third aspect is the physical encapsulation of contaminated waste (due to low permeability of the hardened pastes), which is governed by both the nature of the hydration products and the density and physical structure of the pastes.

In stabilisation and solidification systems using geopolymer binders, geopolymer cements might capture hazardous elements within the three dimensional framework of the geopolymeric matrix and convert semi-solid waste into an adhesive solid (Davidovits 1994). It was also stated that heavy metals might be immobilised through three general steps (Zheng *et al.* 2010):

- (1) metal ions are taken into the geopolymer network;
- (2) metal ions are bound into the structure for charge balancing roles and
- (3) a precipitate containing heavy metals is physically encapsulated.

To date, the exact mechanism of heavy metal immobilisation in geopolymer materials has not been fully understood, though in principle most of the heavy metal cations are easily attracted and combined with [AlO<sub>4</sub>] tetrahedrons due to larger mass, smaller radius and higher valence (van Jaarsveld *et al.* 1999). Future studies on the current topic are therefore recommended.

A study on the immobilisation of Cu and Pb in geopolymers derived from fly ash, carried out by van Jaarsveld *et al.* (1998), reported that these metals may be immobilised in geopolymeric matrices by physical encapsulation, chemical bonding and adsorption. van Jaarsveld *et al.* (1998) found that there were some dif-

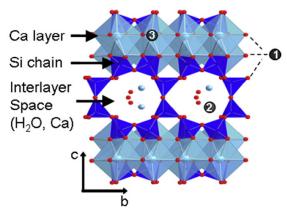


Fig. 6 Possible positions of heavy metals in the tobermorite structure. [Reprinted from (Vespa *et al.* 2014) with permission from Elsevier, ©2014]

ferences in infrared spectra and no apparent major differences in X-ray diffraction between the geopolymer matrix containing Cu and the matrix containing Pb, while these matrices exhibited different compressive strengths and leaching behaviour. These results implied that these metals might be taken into the geopolymer network and possibly bound into the structure for charge balancing roles, and that these metals are bound into the amorphous regions of the product matrices.

One question that needs to be asked, however, is whether physical encapsulation, chemical bonding and adsorption are equally effective. van Jaarsveld *et al.* (1998) concluded that, in geopolymers, physical microencapsulation is deemed to be more important than chemical bonding in influencing the efficiency of immobilisation, and adsorption is not thought to play a major role. Geopolymeric matrices with smaller pore openings as well as higher compressive strength, which is related to solidification, often, exhibited better immobilisation efficiency.

The dominance of physical encapsulation was also observed in several other studies (Palacios and Palomo 2004; Phair and van Deventer 2001). Findings of Phair and van Deventer (2001) showed that increasing the dissolution of Al and Si from the aluminosilicate sources (by raising pH of alkali silicate activation) leads to a greater amount of monomeric and/or oligomeric species of both aluminate and silicate available, which is essential for insolubilising polycondensation reactions. This resulted in better reactive conditions for the immobilisation of Pb. Therefore, the immobilisation of Pb within geopolymer matrices was believed to be an encapsulation process of precipitates and gels, and the contribution of the adsorption process might be negligible. Palacios and Palomo (2004) also found that the Pb compound formed in the fly ash matrix is a highly insoluble silicate Pb<sub>3</sub>SiO<sub>5</sub>, identified by XRD, implying that the immobilisation of Pb in fly ash based geopolymers is mainly by encapsulation of Pb<sub>3</sub>SiO<sub>5</sub>.

In contrast, the predominance of chemical immobilisation was proven by Fernandez-Jimenez *et al.* (2005), in which As was supposed to be chemically bound rather than physically encapsulated. To be more specific, As was found to be associated with amorphous Fe-rich regions within fly ash based geopolymers through EDX data.

In a recent study about the mechanism of immobilisation of Pb(II), Cu(II), Cd(II) and Cr(III) in geopolymers derived from kaolin/zeolite, conducted by El-Eswed *et al.* (2015), heavy metals were believed to balance the negative charge of tetrahedral Al in unreacted zeolite and geopolymer frameworks, and the emphasis was not placed on physical encapsulation process. They stated that the mechanical strength and XRD results were not influenced by incorporation of heavy metals. Therefore physical encapsulation, formation of metal hydroxides or carbonates and silicates were not probably mechanisms for immobilisation of metals. This is because

there is no evidence for participation of heavy metals in new reactions of geopolymerisation process. It appears that this area requires further investigation.

### 4. Factors influencing immobilisation efficiency

Conner (1990) reported that the immobilisation of heavy metals depends not only on the solubility of the metal precipitate, but also on the permeability of the monolith which is a function of pore structure and the amount of water present in the waste. As a consequence, all factors that can change the solubility of the metal precipitate and the permeability of geopolymeric matrix can probably have a bearing on the final immobilisation efficiency of heavy metals, as shown in **Fig. 7**. These factors and their effects are described in detail below.

#### 4.1 The characteristics of the source materials

Raw materials are generally used as the primary reagents in generating the geopolymeric binders that serve as a medium for the immobilisation of metals. It is a fact that fly ash is commonly used as a source material in generating geopolymer binders, though chemical composition of fly ashes varies a lot with the coal source and burning conditions (Rickard *et al.* 2011; Rickard *et al.* 2012). This results in inconsistent geopolymer products. Regarding hazardous waste management, metakaolin may be a better raw material as it has more consistent chemical compositions than fly ash (Zhang *et al.* 2016). However, metakaolin is a thermally treated product from kaolin, which is energy intensive, therefore using geopolymers obtained from metakaolin would not be a cost effective solution.

In some cases, hazardous wastes which need to be treated also play a role in the choice of the source material for producing geopolymer binders. Red mud generally serves as the filler in geopolymeric matrix because of its poor dissolubility in the alkaline solution (Dimas et al. 2009). After experiencing thermal pre-treatment, the red mud dissolves better in alkaline solution and hence functions as a source of alumina and silica for geopolymerisation process, with a higher solubility of calcined red mud resulting in a higher strength of the binders (Ye et al. 2014). Municipal solid waste incineration residue, a hazardous waste (because of high content of heavy metals), was used as an aluminosilicate source for producing geopolymer binder that could successfully stabilise and solidify heavy metals (Zheng et al. 2010). After being calcined at 800°C for 1 hour and ground to have a suitable particle size, water treatment residue that contains heavy metals was valued as an alternative waste material for the synthesis of geopolymers due to its suitable chemical composition (Waijarean et al. 2014).

The structure and properties of the geopolymer materials obtained strongly depend on the particle size, the vitreous phase content and SiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> ratio of raw ma-

terials (Fernández-Jiménez and Palomo 2003; Jang and Lee 2016), implying that the immobilisation capacity of hazardous elements is strongly dependent on the properties of source materials. The increasing Al, Si species liberated from raw materials would provide better environment to form a new phase that would adequately bind and encapsulate heavy metals into a more insoluble form. In addition, the geopolymeric matrix with the highest immobilisation efficiency seems to have the smaller pore openings as well as the higher compressive strength. van Jaarsveld et al. (1998) stated that the source materials appear to have the greatest impact on the eventual ability of the matrix to immobilising metals, since the source materials had an effect on the structure formation at an intratetrahedral scale. The matrices produced from a six-coordinated aluminum source, for example kaolinite, seem to be more stable under leaching conditions than those synthesised from a fourcoordinated aluminum source, for example metakaolinite, probably because the six coordinated aluminum is easier to complete the process of geopolymerisation than its four coordinated counterpart (van Jaarsveld et al. 1998). Palacios and Palomo (2004) compared the capacity of fixation of Pb in two types of fly ash activated in a highly alkaline medium. They pointed out that the nature of the fly ash has a significant impact on the effectiveness of Pb fixation in these systems. In other words, fly ash with a higher proportion of reactive silica and fine particles (greater specific area) would result in greater containment capacity of geopolymeric matrix.

These factors will make a better Pb immobilisation system, since Pb might be mainly immobilised in geopolymeric matrix by physical encapsulation. This view was shared by Nikolić et al. (2017) and he concluded that fly ash reactivity was a deciding factor for the immobilisation property. An other investigation conducted by Phair et al. (2004) on the effect of the Al sources on the Pb and Cu stabilisation showed that the immobilisation of Pb is linked with the total extractable cation concentration of the Al source. It is difficult to explain this result, but it may be related to the fact that Pb precipitates are more susceptible to subsequent reactions than Cu precipitates, so they tend to be affected by the available amount of cations released from Al source, which can transform Pb precipitates into more stable forms, amorphous aluminosilicate phases. In contrast, the immobilisation of Cu was observed to be mainly associated with the physical characteristics of the source of Al (Phair et al. 2004). This is possibly because precipitates of Cu may be more stable than that of Pb. Thus, compressive strength of the matrix and the suspension viscosity of the Al source have a considerable effect on the Cu immobilisation efficiency.

### 4.2 The pH and type of alkali activator

In general, the pH of alkali activator is strongly affected by the type of activator and its concentration. The pH of alkali activator was deemed to be a major contributing factor for the final immobilisation efficiency, since increasing pH would lead to the reduction of the pore size,

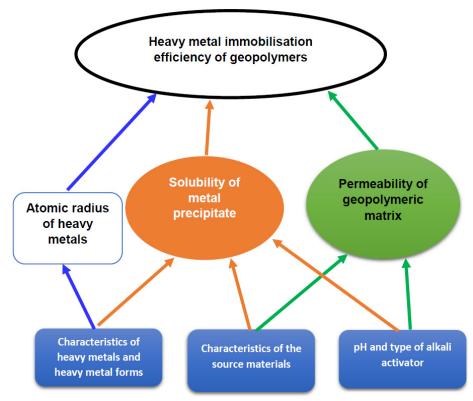


Fig. 7 Possible factors affecting the capacity of geopolymer materials for immobilising heavy metals.

Atomic	Element	Empirical	Calculated	Van der Waals	Covalent (Single bond)	Covalent (Triple bond)	Metallic
Number		(pm)	(pm)	(pm)	(pm)	(pm)	(pm)
24	Cr	140	166	no data	127	103	128
27	Co	135	152	no data	126	96	125
28	Ni	135	149	163	121	101	124
29	Cu	135	145	140	138	120	128
30	Zn	135	142	139	131	no data	134
33	As	115	114	185	119	106	
34	Se	115	103	190	116	107	
48	Cd	155	161	158	148	no data	151
80	Hg	150	171	155	149	no data	151
82	Pb	180	154	202	147	137	
92	U	175	no data	186	no data	118	156

Table 2 Atomic radii of some toxic heavy metals.

and therefore matrix permeability (Davis et al. 1994). Depending on the relative proportions of silicate and hydroxide available in the alkali silicate environment, heavy metal precipitates formed in geopolymeric matrices could be either metal hydroxide and/or metal silicate species. Therefore, the metal immobilisation within geopolymers was thought to be strongly dependent on the pH of the alkali activator used (Phair and van Deventer 2001). For instance, at pH 12 the amount of silicate ions would be large enough to preferentially combine with the cations in considerable amounts, while at pH 14 there would be a tendency for cations to combine with hydroxide than at pH 12. Further, the precipitates formed at pH 12 is more insoluble than the precipitates at pH 14, so the immobilisation efficiency at pH 12 is expected to be higher than at pH 14. Notwithstanding, the matrix produced at pH 12 was found to be more porous and subsequently more permeable, and therefore reduced the efficiency of metal immobilisation (Phair and van Deventer 2001). Thus, it could be concluded that the increase of immobilisation efficiency and the increasing pH are directly linked. In another study of Cheng et al. (2012), the amount of heavy metals adsorbed on the geopolymers increased with increasing pH of the solution. It was explained that when the concentration of H<sup>+</sup> in the solution is higher, geopolymer tends to adsorb H<sup>+</sup>. As a result, the adsorption capability of heavy metals increases in a higher pH environment. A similar result was seen by Nikolić et al. (2013). Increasing pH of alkali solution resulted in better Zn immobilisation from metallurgical waste.

As for the impact of alkali activator type on the stabilisation of heavy metal, Phair and van Deventer (2001) reported that Cu or Pb are stabilised better in sodium silicate solutions than potassium silicate solutions. It may be probably because sodium silicate is less polymerised at high pH than potassium silicate because of the larger hydration sphere of the sodium ion. In addition, the hydration spheres of sodium silicate, Cu and Pb are relatively similar, so Cu and Pb interchange with sodium silicate more easily than with potassium silicate, resulting in the better immobilisation efficiency (Phair and van Deventer 2001). Similarly, using sodium hydroxide in the activating solution led to the higher ca-

pacity of Cr immobilisation compared to using potassium hydroxide (Galiano *et al.* 2011). Moreover, the characteristic pore size of geopolymers was demonstrated to be closely related to the type of the alkali cation Na<sup>+</sup> or K<sup>+</sup> used in activation (Kriven *et al.* 2008; Steins *et al.* 2014), implying that the heavy metal stabilisation is possibly influenced by the choice of alkali.

### 4.3 The characteristics of heavy metals and heavy metal forms

Atomic radius of metal has been an important factor for the heavy metal immobilisation. The atomic radius of an element is the distance from the centre of the nucleus to the outermost shell of the electron. Since the boundary is not a well-defined physical entity, there are various non-equivalent definitions of atomic radius. Depending on the definition, the term may apply only to isolated atoms, or also to atoms in condensed matter, in covalent bond in molecules, or in ionised state. Atomic radii of some toxic heavy metals are shown in **Table 2**.

The immobilisation of Cu in geopolymeric matrices is generally less effective compared to Pb, since the atomic radius of Cu is smaller than that of Pb (see **Table 2**), which makes diffusion, translocation and leaching of Cu much easier although the electrical charges on both Cu and Pb are the same (Phair and van Deventer 2001). Slag based geopolymeric matrix showed a better immobilisation efficiency for Pb than for Cu in the case of large dosages of heavy metals, probably because ionic radius of Pb and Cu are different. Hence, Cu and Pb are immobilised in different ways in the slag based geopolymeric matrix (Yunsheng *et al.* 2007).

The size of the hydrated ions which bears on the attraction force between hydrated ion and metal, free energy of hydration (the higher the level of free energy of hydration, the smaller is the possibility for heavy metal ions to enter the adsorbent structure), and activity of metal ions were thought to be responsible for the adsorption of the heavy metal ions on the geopolymeric matrix (Cheng *et al.* 2012). On the other hand, Xu *et al.* (2006) investigated the leaching behaviour of Cd, Cu, Pb and Cr in fly ash based geopolymer and stated that the leaching behaviour of heavy metals could be influenced by other heavy metals in a complex system as

well. However, this study was unable to explain how this occurred and led to many unanswered questions which need further investigation.

Apart from size, the nature of heavy metals is also important. The stabilisation of metals in geopolymeric matrices could be affected by the chemical properties of the metal compounds. This was proved in the case of Pb (Guo et al. 2017) and Cr (Zhang et al. 2008b; Chen et al. 2016). Three types of the Pb contaminants PbO, PbSO<sub>4</sub> and PbS, common in the environment, were added in the fly ash based geopolymer matrices. Pb was proved to be dispersed throughout the geopolymeric matrix in the case of PbO addition, forming leaded geopolymer via Pb-O-Al or/and Pb-O-Si. By contrast, PbS was observed to be segregated from the bulk of the binder (Guo et al. 2017). It was concluded that when Pb compounds were supplied in the form soluble in sodium hydroxide solution, the Pb ions would participate in the formation of geopolymer network, stimulating both chemical bonding and physical encapsulation. In the case of the Pb compounds that are inert to alkali, the immobilisation may be mainly by the physical encapsulation in the geopolymeric matrices. As a result, the upper limit of the Pb content, which can be immobilised in the geopolymer, varies with the form of Pb (Guo et al. 2017).

In nature, common oxidation states of Cr are 3<sup>+</sup> and 6<sup>+</sup> states. Cr(VI) is particularly toxic, soluble, and relatively mobile in the environment (Kresic 2006). The immobilisation of Cr(VI) was found problematic (Palomo and Palacios 2003; Zhang et al. 2008a). The matrix of alkali-activated fly ash was found to be unable to stabilise 2.6% Cr(VI) in the form of CrO<sub>3</sub>, because Cr(VI) acted on the activation of fly ash due to the formation of a highly soluble compound Na<sub>2</sub>CrO<sub>4</sub>.4H<sub>2</sub>O (observed through XRD and FTIR) (Palomo and Palacios 2003). Even with a smaller dosage of Cr(VI) 0.5% as Na<sub>2</sub>CrO<sub>4</sub> added in fly ash based geopolymers, long-term leaching tests in different media showed that more than 75% Cr extraction was observed (Zhang et al. 2008a). On the contrary, Cr(III) is less toxic, less mobile, and relatively insoluble as Cr(OH)<sub>3</sub> as well as mixed hydroxide phases containing some Ca (Omotoso et al., 1996). Reduction from Cr(VI) to Cr(III) was recommended as pre-treatment before immobilisation of chromium wastes in several previous studies (Eary and Rai 1988; Portland Cement Association 1991; Lan et al. 2007). The most common chemical reductants for converting Cr(V1) to Cr(II1) are ferrous Fe(II)compounds (shown in Eq.1) and sulfur compounds.

$$6FeSO_4 + 2Cr(SO_4)_3 \rightarrow Cr_2(SO_4)_3 + 3Fe_2(SO_4)_3$$
 (1)

In a study carried out by Zhang *et al.* (2008b), sulfur compound (Na<sub>2</sub>S.9H<sub>2</sub>O) was added to fly ash based geopolymer, which reduced Cr(VI) (Na<sub>2</sub>CrO<sub>4</sub>, PbCrO<sub>4</sub>) to Cr(III), enabling precipitation in highly insoluble forms and resulting in the increasing the immobilisation

efficiency. In another case, a mixture of FeCl<sub>2</sub>.4H<sub>2</sub>O and K<sub>2</sub>Cr<sub>2</sub>O<sub>7</sub> was used to convert Cr (VI) to Cr (III) (Chen *et al.*, 2016). Cr<sup>3+</sup> was then attracted by [AlO<sub>4</sub>] due to the electrostatic attraction and stabilised in metakaolin-based geopolymerical matrices, leading to a relatively high immobilisation efficiency of Cr (Chen *et al.* 2016).

### 5. Conclusions

From the literature reviewed above, the following conclusions can be reached:

Heavy metal immobilisation in a geopolymer binder is mainly conditional upon the nature of heavy metal, the characteristics of the raw materials of the geopolymer, the pH and type of activator and the resulting pore structure of the geopolymer.

The mechanisms of immobilisation of different heavy metals in geopolymer matrices could be physical encapsulation or chemical bonding. However, most often it is a combination of the two mechanisms and the combination varies considerably, depending on the nature of heavy metals and metal compounds which needs to be safely disposed. It is essential that the correct combination of the physical and chemical mechanisms is identified and developed for safe disposal of a particular heavy metal waste.

For efficient immobilisation of toxic metals, the synthesis and curing conditions of geopolymers and the long term stability of the products are important considerations. These areas are avenues available for obtaining an effective stabilisation/solidification system of harmful metals.

Different raw materials and their reactivity in the presence of different activators also need to be investigated further for a certain hazardous metal immobilisation.

In addition to this, the role of interfacial transition zone of geopolymers materials with particular reference to physical encapsulation process of heavy metal immobilisation should be further investigated.

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