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# Direction of arrival estimation of Multiple acoustic sources using a maximum likelihood method in the spherical harmonic domain

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13 Abstract: Direction of arrival estimation (DOA) of multiple acoustic sources has been used for a 14 wide range of applications, including room geometry inference, source separation and speech enhancement. The beamformer-based and subspace-based methods are most commonly used for 15 spherical microphone arrays; however, the former suffers from spatial resolution limitations, while 16 17 the later suffers from performance degradation in noisy environment. This letter proposes a 18 multiple source localization approach based on the maximum likelihood method in the spherical 19 harmonic domain and implements an efficient sequential iterative search of maxima on the cost 20 function in the spherical harmonic domain. The proposed method avoids the division of the spherical Bessel function, which makes it suitable for both rigid-sphere and open-sphere 21 22 configurations. Simulation results show that the proposed method has a significant superiority 23 over the commonly used frequency smoothing multiple signal classification method. Experiments 24 in a normal listening room and a reverberation room validate the effectiveness of the proposed 25 method.

Keywords: multiple source localization; maximum likelihood; spherical harmonic domain;
 alternating projection

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# 29 1. Introduction

The rotationally symmetric spatial directivity makes the spherical microphone array an appealing structure in many audio applications, among which the acoustic source localization, or the direction of arrival (DOA) estimation, plays an important role in speech enhancement [1], room impulse response analysis [2], and room geometry inference [3].

34 Various DOA estimation methods have been proposed, which can be generally classified as 35 beamformer-based [2-5] and subspace-based [6-7]. The beamformer-based methods, such as those 36 based on plane-wave decomposition (PWD) [4] and the minimum variance distortionless response 37 (MVDR) beamformer [3], have the benefit of straightforward implementation, but suffer from low 38 spatial resolution. The subspace-based methods, such as the multiple signal classification (MUSIC) 39 [6], provide a high spatial resolution; however, they suffer from severe performance degradation 40 when the signal-to-noise ratio (SNR) is low [8]. In order to improve the robustness of the DOA 41 estimation of coherent sources, wideband expansion based on focusing matrices or frequency 42 smoothing (FS) techniques has to be employed [7].

43 We proposed a maximum likelihood DOA estimation method in the spherical harmonic 44 domain (SHMLE) recently, which is an attractive alternative DOA estimation method with advantages of high spatial resolution, strong robustness and straightforward wideband
implementation [9]. The proposed SHMLE method only considered one source situation, while two
or more sources often need to be localized in many practical applications. In this letter, the SHMLE
method is extended to estimate the DOA of multiple sources. Generally speaking, the DOAs can be
determined by searching maxima on the maximum likelihood (ML) cost function. However, the
commonly used grid search method is only effective in finding the global maximum, which restricts

51 its applicability in one source situation. To achieve effective DOA estimation of multiple sources, an

- efficient sequential iterative search method is introduced in the spherical harmonic (SH) domain.
   Experiments using a 32-element spherical microphone array validate the feasibility and superiority
- 54 of the proposed method.

# 55 2. Methods

## 56 2.1. Signal model in the spherical harmonic domain

57 The standard spherical coordinate system is utilized with *r*,  $\theta$  and  $\varphi$  representing the radius, the 58 elevation angle and the azimuth, respectively. The sound field is assumed to be composed of plane 59 waves from *L* sources with  $\Psi_l = (\theta_l, \varphi_l)$  (l = 1, 2, ..., L) being the DOA of the *l*-th plane wave and  $s_l(k)$ 60 being its amplitude, where *k* denotes the wave number. The *Q* element spherical microphone array 61 is distributed uniformly on a sphere with a radius of *a* centred at the origin of the coordinate system, 62 and  $\Omega_q = (\theta_q, \varphi_q)$  is the angle position of the *q*-th microphone [10].

63 The sound pressure of the *q*-th microphone for the incident waves can be expressed as [11]

$$p(k,\Omega_q) = \sum_{l=1}^{L} s_l(k) e^{i \mathbf{k}_l^T \mathbf{r}_q} \approx \sum_{l=1}^{L} s_l(k) \sum_{n=0}^{N} \sum_{m=-n}^{n} b_n(k) Y_{n,m}^*(\Psi_l) Y_{n,m}(\Omega_q),$$
 (1)

65 where  $\mathbf{k}_l = -k(\cos\varphi_l\sin\theta_l, \sin\varphi_l\sin\theta_l, \cos\theta_l)^T$  and  $\mathbf{r}_q = a(\cos\varphi_q\sin\theta_q, \sin\varphi_q\sin\theta_q, \cos\theta_q)^T$  denote the wave 66 vector of the *l*th plane wave and the position of the *q*-th microphone in the Cartesian coordinate.  $Y_{n,m}$ 67 is the spherical harmonic of order *n* and degree *m*, *N* is the highest order number for the plane wave 68 decomposition and satisfies  $(N+1)^2 < Q$ . The superscript (\*) denotes complex conjugation, and  $b_n(k)$  is 69 a function of array configuration [11]. Equation (1) can be expressed in matrix form as

70 
$$p(k, \Omega_q) \approx \mathbf{y}^{\mathrm{T}}(\Omega_q) \mathbf{B}(k) \mathbf{Y}^{\mathrm{H}}(\mathbf{\Psi}) \mathbf{s}(k),$$
 (2)

71 with

$$\mathbf{y}\left(\Omega_{q}\right) = \left[Y_{0,0}\left(\Omega_{q}\right), Y_{1,-1}\left(\Omega_{q}\right), Y_{1,0}\left(\Omega_{q}\right), Y_{1,1}\left(\Omega_{q}\right), \dots, Y_{N,N}\left(\Omega_{q}\right)\right]^{\mathrm{T}}, \quad (3)$$

73 
$$\mathbf{y}(\Psi_{l}) = \left[Y_{0,0}(\Psi_{l}), Y_{1,-1}(\Psi_{l}), Y_{1,0}(\Psi_{l}), Y_{1,1}(\Psi_{l}), ..., Y_{N,N}(\Psi_{l})\right]^{\mathrm{T}},$$
(4)

74 
$$\mathbf{Y}(\mathbf{\Psi}) = \left[\mathbf{y}(\Psi_1), \mathbf{y}(\Psi_2), \dots, \mathbf{y}(\Psi_L)\right]^{\mathrm{T}},$$
 (5)

75 
$$\mathbf{B}(k) = diag\{b_0(k), b_1(k), b_1(k), b_1(k), \dots, b_N(k)\},$$
(6)

$$\mathbf{s}(k) = \left[s_1(k), s_2(k), \dots, s_L(k)\right]^{\mathrm{T}},$$
(7)

$$\boldsymbol{\Psi} = \begin{bmatrix} \Psi_1, \Psi_2, \dots, \Psi_L \end{bmatrix}, \tag{8}$$

78 where the superscript  $(^{T})$  denotes the transpose.

79 In the presence of additive noise, the sound pressure at all *Q* microphones can be expressed as

80 
$$\mathbf{p}(k, \Omega) \approx \mathbf{Y}(\Omega) \mathbf{B}(k) \mathbf{Y}^{\mathrm{H}}(\Psi) \mathbf{s}(k) + \mathbf{v}(k),$$
 (9)

81 where

$$\mathbf{Y}(\mathbf{\Omega}) = \left[\mathbf{y}(\Omega_1), \mathbf{y}(\Omega_2), \dots, \mathbf{y}(\Omega_Q)\right]^{\mathrm{T}},$$
(10)

83  $\mathbf{p}(k,\Omega) = [p(k,\Omega_1), p(k,\Omega_2), ..., p(k,\Omega_Q)]^{\mathsf{T}}$  is the vector of the sound pressure of Q microphones, and  $\mathbf{v}(k)$ 84  $= [\nu_1(k), \nu_2(k), ..., \nu_Q(k)]^{\mathsf{T}}$  is the vector of the additive sensor noise added to the system. The 85 uncorrelated noise is assumed to be zero mean complex Gaussian and, for simplicity, be spatially 86 white with a covariance matrix  $\mathbf{R}_{\mathbf{v}}(k) = \sigma_{\mathbf{v}}^2 \mathbf{I}_Q$ , where  $\sigma_{\mathbf{v}}^2$  is the unknown noise variance and  $\mathbf{I}_Q$  is 87 the identity matrix of order  $Q \times Q$ .

For the uniformly spatial sampling configuration used in this letter, the following orthogonal relation holds (note that  $(N+1)^2 \le Q$ ) [10]

90 
$$\frac{4\pi}{Q} \mathbf{Y}^{\mathrm{H}}(\mathbf{\Omega}) \mathbf{Y}(\mathbf{\Omega}) = \mathbf{I}_{(N+1)^{2}}.$$
 (11)

91 The SH transform can be carried out by multiplying both sides of Eq. (9) from the left with 92  $\frac{4\pi}{O} \mathbf{Y}^{\mathrm{H}}(\mathbf{\Omega})$ , which yields

93 
$$\mathbf{p}_{nm}(k) \approx \mathbf{B}(k) \mathbf{Y}^{H}(\mathbf{\Psi}) \mathbf{s}(k) + \mathbf{v}_{nm}(k), \qquad (12)$$

94 where  $p_{nm}(k)$  is a vector containing  $(N+1)^2$  SH domain coefficients, i.e.,

95 
$$\mathbf{p}_{\mathbf{nm}}(k) = \left[ p_{0,0}(k), p_{1,-1}(k), p_{1,0}(k), p_{1,1}(k), \dots, p_{N,N}(k) \right]^{\mathrm{T}}.$$
 (13)

96 The second term on the right side of Eq. (12) is the noise expressed in the SH domain, i.e. 97  $\mathbf{v}_{nm}(k) = \frac{4\pi}{\Omega} \mathbf{Y}^{\mathrm{H}}(\Omega) \mathbf{v}(k)$ , with the mean

98 
$$E\left[\mathbf{v}_{nm}\left(k\right)\right] = \frac{4\pi}{Q}\mathbf{Y}^{\mathrm{H}}\left(\mathbf{\Omega}\right)E\left[\mathbf{v}\left(k\right)\right] = \mathbf{0}, \qquad (14)$$

99 and the covariance matrix

100 
$$\mathbf{R}_{\mathbf{nm}}(k) = E\left[\frac{4\pi}{Q}\mathbf{Y}^{\mathrm{H}}(\mathbf{\Omega})\mathbf{\nu}(k)\mathbf{\nu}^{\mathrm{H}}(k)\mathbf{Y}(\mathbf{\Omega})\frac{4\pi}{Q}\right] = \frac{4\pi}{Q} \cdot \sigma_{\nu}^{2}\mathbf{I}_{(N+1)^{2}}, \qquad (15)$$

where  $E(\cdot)$  denotes the statistical expectation. Apparently, the noise model in the SH domain is also zero-mean complex Gaussian.

# 103 2.2. Sound source localization in the spherical harmonic domain

104 Define  $\boldsymbol{\Theta} = \begin{bmatrix} \boldsymbol{\Psi}^T, \boldsymbol{S}^T, \sigma_n^2 \end{bmatrix}^T$  as the vector of all unknown parameters, where 105  $\mathbf{S} = \begin{bmatrix} \mathbf{s} (k_{\min})^T, \dots, \mathbf{s} (k_{\max})^T \end{bmatrix}^T$  contains the amplitudes of the source signals with  $k_{\min}$  and  $k_{\max}$ 106 representing the minimum and maximum wave numbers and satisfying  $ka \leq N$ . Throughout this 107 letter,  $\boldsymbol{\Psi}$ , s and  $\sigma_v^2$  are assumed to be deterministic and unknown, while the observed data  $\mathbf{p}_{nm}$  is 108 considered to be random [12]. The likelihood function of  $\mathbf{p}_{nm}$  given  $\boldsymbol{\Theta}$  in the SH domain can be 109 expressed as [9,12]

110 
$$f(\mathbf{p}_{nm}; \mathbf{\Theta}) = \frac{\exp\left\{-\sum_{k=k_{min}}^{k_{max}} \left[\mathbf{p}_{nm}(k) - \mathbf{V}_{nm}\left(k, \Psi\right)\mathbf{s}(k)\right]^{H} \mathbf{R}_{nm}^{-1} \left[\mathbf{p}_{nm}(k) - \mathbf{V}_{nm}\left(k, \Psi\right)\mathbf{s}(k)\right]\right\}}{\left(\pi^{(N+1)^{2}} \left|\mathbf{R}_{nm}\right|\right)^{k_{max}-k_{min}}}, \quad (16)$$

111 where  $V_{nm}(k, \Psi) = \mathbf{B}(k)\mathbf{Y}^{H}(\Psi)$ , and  $|\cdot|$  denotes the matrix determinant. The solution to Eq. (16) is 112 given by [9]

4 of 9

(19)

113 
$$\hat{\boldsymbol{\Psi}} = \arg\min_{\boldsymbol{\Psi}} \sum_{k=k_{min}}^{k_{max}} \left\| \boldsymbol{p}_{nm}\left(k\right) - \boldsymbol{V}_{nm}\left(k,\boldsymbol{\Psi}\right) \boldsymbol{V}_{nm}\left(k,\boldsymbol{\Psi}\right)^{\dagger} \boldsymbol{p}_{nm}\left(k\right) \right\|^{2}, \quad (17)$$

114 where  $(\cdot)^{\dagger}$  denotes pseudo-inverse operation.

115 Define the cost function as

116 
$$J(\boldsymbol{\Psi}) = -10\log_{10}\left(\sum_{k=k_{\min}}^{k_{\max}} \left\| \mathbf{p}_{nm}\left(k\right) - \mathbf{V}_{nm}\left(k,\boldsymbol{\Psi}\right) \mathbf{V}_{nm}\left(k,\boldsymbol{\Psi}\right)^{\dagger} \mathbf{p}_{nm}\left(k\right) \right\|^{2}\right), \quad (18)$$

117 then the wideband estimator can be described as

119 The SHMLE has the remarkable benefit of easy wideband implementation as described in Eqs. 120 (17)-(19). This is superior over the other methods in the spherical harmonic domain, which usually 121 require a quite cumbersome frequency smoothing (FS) technique to realize wideband DOA [7]. 122 Compared with the maximum likelihood method in Ref. 13, the division of  $b_n(k)$  is avoided, which 123 makes the method proposed in this letter suitable for both rigid-sphere and open-sphere arrays.

 $\hat{\boldsymbol{\Psi}} = \arg\max_{\boldsymbol{\Psi}} J(\boldsymbol{\Psi}) \,.$ 

#### **124** *2.3. DOA estimation of multiple sources*

125 For one source situation, Eq. (19) can be solved using the grid search method. For P grid points 126 and L sources situation, the computational load of Eq. (19) is  $O(P^L)$ , which is computationally 127 prohibitive. Moreover, effective discrimination of the multiple maxima in the cost function is very 128 difficult even if repetitive traversal is feasible. To alleviate these problems, a nonlinear optimization 129 algorithm is applied in the SH domain with implementation of the alternating projection method 130 [14]. The alternating projection method avoids the multidimensional search by estimating the 131 location of one source sequentially while fixing the estimates of other source locations from the 132 previous iteration.

For nonlinear optimization methods, the initial locations of the sound sources is critical to reach the global maximum. In this letter, the simplified gird search method is adopted to find initial locations, and the procedure of the method is described as follows.

136 (1) Estimate the location of the first source *s*<sup>1</sup> on a single source grid with

137 
$$\Psi_1^{(0)} = \arg \max_{\Psi_1} J(\Psi_1).$$
 (20)

138(2) For l = 2, ..., L, estimate the location of the *l*th source  $s_l$ , assuming locations of the first l-1139sources are fixed by using

140 
$$\Psi_l^{(0)} = \arg \max_{\Psi_2} J\left(\left[\Psi_{l-1}^{(0)}, \Psi_l\right]\right), \tag{21}$$

141 where  $\Psi_{l-1}^{(0)}$  denotes the initial locations of first l-1 sources, i.e.

142 
$$\Psi_{l-1}^{(0)} = \left[\Psi_{1}^{(0)}, \Psi_{2}^{(0)}, \cdots, \Psi_{l-1}^{(0)}\right].$$
 (22)

143 In steps (1) and (2), Eq. (19) only needs to be calculated  $P \times L$  times and the effective initial 144 location information can be obtained. In some cases, this initialization process is not necessary since 145 a good initial location estimate is available, for example, from the estimate of the previous data for 146 slowly moving sources.

147 After initialization, the accurate locations can be estimated using a nonlinear optimization 148 algorithm with implementation of the alternating projection method [14]. The location of  $\Psi_i$  at the (*i* 149 + 1)th iteration can be estimated by solving the one-dimensional maximization problem

150 
$$\Psi_l^{(i+1)} = \arg \max_{\Psi_l} J\left(\left[ \Psi_l, \Psi_s^{(i)}, \right]\right), \tag{23}$$

151 where  $\Psi_s^{(i)}$  denotes the estimated locations of other L - 1 sources, i.e.

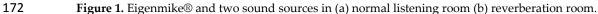
152 
$$\Psi_{s}^{(i)} = \left[\Psi_{1}^{(i+1)}, \cdots, \Psi_{l-1}^{(i+1)}, \Psi_{l+1}^{(i)}, \cdots, \Psi_{L}^{(i)}\right].$$
 (24)

In Eq. (23), the Quasi-Newton (QN) method with Broyden-Fletcher-Goldfarb-Shanno algorithm [15] is used, and the QN method is available in MATLAB as in the *fminunc* function. For the beamformer-based and subspace-based methods, the localization results are acoustic maps [7]. An extra algorithm is needed to identify the location of the sound sources from the acoustic maps. On the contrary, the method proposed in this letter can automatically provide the localization results, as described in Eq. (23). Furthermore, the localization precision of the proposed method can be extremely high, as will be demonstrated in the following simulations and experiments.

## 160 3. Simulations and experiments

161 In this section, the performance of the proposed method, i.e., the multiple source SHMLE 162 (MS-SHMLE), is investigated and compared to the FSMUSIC method [7], which has the benefits of 163 high spatial resolution and easy implementation. The Eigenmike® [16] microphone array model, with Q = 32 microphones arranged uniformly on a sphere with radius a = 4.2 cm (depicted in Fig. 1), 164 165 was used in both simulations and experiments. Only two source cases were considered in 166 simulations and experiments, and the proposed method can be easily utilized to other scenarios with more sources as described in Sec. 2.3. The source signals are independent white Gaussian noise 167 sampled at a sampling rate of  $f_s$  = 16 kHz, and a frame of 1024 samples is extracted from the 168 169 recordings. The localization frequency range is  $ka \in [2.5 \ 3.5]$ . The grid resolution of FSMUSIC is 1°.





173 Root mean squared error (RMSE) is used to assess the performance of the localization results,174 which is defined as

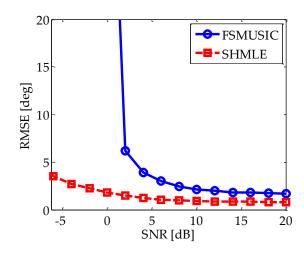
$$RMSE = \sqrt{E\left\{ \left( \Psi - \hat{\Psi} \right) \left( \Psi - \hat{\Psi} \right)^{T} \right\}}.$$
(25)

#### **176** *3.1. Simulations with different SNR*

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Figure 2 depicts the RMSE of the FSMUSIC and the MS-SHMLE as a function of SNR in a room with reverberation time of 0.3 s. In this simulation, the room dimensions are 6×7×5 m<sup>3</sup>, the microphone array is located at [3, 2.5, 1.5] m and the speakers are placed 1.0 m away from the array center. Sound sources incident from directions of (90°, 180°) and (90°, 120°). The RMSE is averaged over 100 different trials. The room impulse responses between the sound sources and the microphones positioned on the rigid sphere are simulated using the method proposed in Ref. 17. It 183 can be seen that the RMSE of the MS-SHMLE is better than that of FSMUSIC especially for the low 184 SNR situations, and FSMUSIC fails to present meaningful DOAs when the SNR is lower than 2 dB.



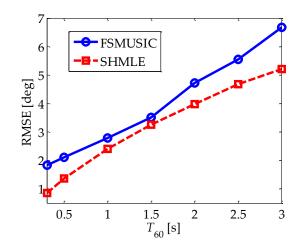
185



#### 188 3.2. Simulations under different reverberation time

189 When the reverberation time is higher than 1.5 s, the method proposed in Ref. 17 is not suitable 190 to simulate the room impulse responses because of its high computational burden and memory 191 requirement. Therefore, an open-sphere array configuration is used in this simulation and the room 192 impulse responses are simulated using the method proposed in Ref. 18. When then open-sphere 193 configuration is used, the FSMUSIC method suffers from ill-conditioning around the zeros of the 194 spherical Bessel function, and a mitigation method proposed in Ref. 19 is utilized.

195 Figure 3 depicts the localization RMSE of the FSMUSIC and the MS-SHMLE as a function of the 196 reverberation time  $T_{60}$ . In this simulation, the SNR is fixed at 15 dB. It can be seen that the RMSE of 197 the MS-SHMLE is better than that of FSMUSIC under different reverberation time.



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- 199

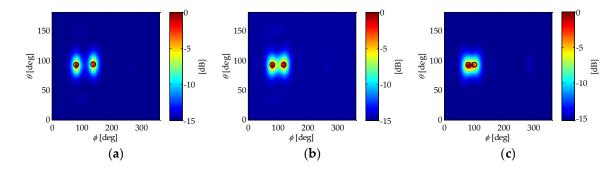
Figure 3. Localization RMSE of the FSMUSIC and the MS-SHMLE versus reverberation time with an 200 SNR of 15 dB.

#### 201 3.3. Two-source experiments in a listening room

202 The experiments for DOA estimation of two sources were carried out in a listening room with 203 background noise less than 30 dBA as depicted in Fig. 1(a). The room dimensions are 5×8×4 m<sup>3</sup> and 204 the reverberation time is around 0.3 s. The microphone array was located at [2.5, 3, 1.5] m. Two

sound sources were placed 1.5 m away from the array with 7 different angle differences  $\Delta \varphi$ . The sound pressure level (SPL) difference of the two sources at the array center is around 2 dB.

207 Figure 4 depicts the localization results for two sources case using the FSMUSIC methods. The 208 DOA of the sound source is denoted by a solid black circle in all these figures. It can be found that 209 FSMUSIC can distinguish both sources when the angle difference between the two sources is larger 210 than  $20^{\circ}$ , as depicted in Fig 4(a) and (b). When the separation angle between sources is close to  $20^{\circ}$ , 211 FSMUSIC fails to identify two sources, as depicted in Fig 4(c), because the local maxima of the 212 weaker source is totally merged into the main lobe of the stronger one. It should be noted that 213  $V_{nm}(k,\Psi)$  in Eq. (17) contains the steering vector of all sources. Therefore, the acoustic maps depicted 214 in Fig. 4 are not suitable for the MS-SHMLE method.



**Figure 4.** Localization results for two sources case using the FSMUSIC method in a listening room with (a)  $\Delta \varphi = 60^{\circ}$ , (b)  $\Delta \varphi = 40^{\circ}$  and (c)  $\Delta \varphi = 20^{\circ}$ .

Table 1 shows the RMSE of the FSMUSIC and the MS-SHMLE for a 10 s recorded data. Although the RMSE of these two methods are close, the FSMUSIC can only locate the stronger one when the separation angle between the two sources is close to 20°, while the MS-SHMLE can distinguish both sources. The average RMSE of the MS-SHMLE is comparatively lower than FSMUSIC, which is in consistence with the simulations results.

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Table 1. RMSE of the FSMUSIC and the MS-SHMLE for two sources case in a listening room

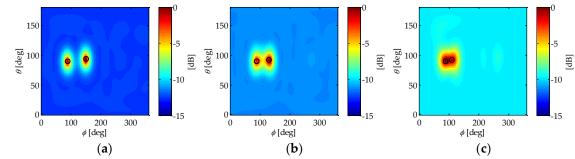
Angle difference	RMSE of FSMUSIC			<b>RMSE of MS-SHMLE</b>		
	Strong	weak	total	strong	weak	total
180 °	0.73 °	1.19°	0.99°	0.32 °	1.66 °	1.20 °
120 °	0.59 °	0.85 °	0.73 °	0.32 °	0.91 °	$0.68~^{\circ}$
90 °	0.76 °	0.89 °	0.83 °	0.42 °	0.90 °	$0.70^{\circ}$
60 °	0.77 °	0.71 °	0.74 °	0.32 °	0.79 °	$0.60^{\circ}$
40 °	0.83 °	$0.78~^\circ$	0.81 °	0.34 °	1.05 °	$0.78^{\circ}$
30 °	1.08 °	1.65 °	1.39 °	0.44 °	1.76 °	1.28 °
20 °	1.66 °	-	-	0.63 °	1.54 °	1.18°

225 3.4. Two-source experiments in a reverberation room

To further validate the robustness of the proposed algorithm in high reverberant environments, the experiments for DOA estimation of two sources were also carried out in a reverberation room as depicted in Fig. 1(b). The room dimensions are  $5.9 \times 7.35 \times 5.22$  m<sup>3</sup>. The reverberation time is around 3 s at frequency range  $ka \in [2.5 \ 3.5]$ . In the experiments, the microphone array was located at [3 2.5 1.5] m, and the sound sources were placed 1.5 m away from the array.

Figure 5 depicts the localization results for the two sources case using the FSMUSIC method. Similar to the results in the listening room, when the angle difference between the two sources is larger than 20°, FSMUSIC can distinguish both sources as depicted in Fig 5(a) and (b). When the separation angle between sources is close to 20°, FSMUSIC can only locate the stronger source while fail to identify the weaker one, as depicted in Fig 5(c).







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237

**Figure 5.** Localization results for two sources case using the FSMUSIC method in a listening room with (a)  $\Delta \varphi = 60^{\circ}$ , (b)  $\Delta \varphi = 40^{\circ}$  and (c)  $\Delta \varphi = 20^{\circ}$ .

Table 2 shows the RMSE of the FSMUSIC and the MS-SHMLE for a10 s recorded data. It can be seen that the localization RMSE in the reverberation room is higher than that in the listening room. The RMSE of these two methods increase significantly when the angle difference between the two sources is close to or lower than 30°. When the separation angle between the two sources is close to 20°, the FSMUSIC can only locate the stronger one, while the MS-SHMLE can distinguish both sources. The superiority of the MS-SHMLE in high reverberant environment coincides well with the simulations presented in Sec. 3.2.

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Table 2. RMSE of the FSMUSIC and the MS-SHMLE for the two sources case in a reverberation room

Angle	<b>RMSE of FSMUSIC</b>			<b>RMSE of MS-SHMLE</b>		
difference	strong	weak	Total	Strong	weak	total
180°	1.38°	1.38°	1.38°	1.42°	1.22°	1.32°
120°	1.25°	1.17°	1.21°	1.30°	1.19°	1.25°
90°	1.49°	1.17°	1.34°	1.40°	1.07°	1.24°
60°	1.54°	1.20°	1.38°	1.29°	0.98°	1.15°
40°	1.53°	1.34°	1.44°	1.73°	1.42°	1.59°
30°	4.22°	3.46°	3.86°	1.99°	2.02°	2.00°
20°	4.57°	-	-	3.56°	4.02°	3.80°

# 248 4. Conclusion

249 This letter proposes a multiple source localization method in the spherical harmonic domain 250 using the maximum likelihood strategy. To avoid high-dimensional grid search with extremely high 251 computational burden, a nonlinear optimization algorithm with implementation of the alternating 252 projection method is introduced, leading to an efficient MS-SHMLE method. The proposed method 253 avoids the division of the spherical Bessel function, which makes it suitable for both rigid-sphere 254 and open-sphere configurations. Simulations and experiments on a 32-microphone model 255 demonstrate that the proposed MS-SHMLE method has very good spatial resolution and can 256 distinguish two sources with 20° angle difference in both normal listening room and reverberation 257 room. Furthermore, the performance is stable in low SNR environment, circumventing the problem 258 faced by the subspace-based method.

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# 260 References

- Kumatani, K.; McDonough, J.; Raj, B. Microphone array processing for distant speech recognition: From
   close-talking microphones to far-field sensors. *IEEE Signal Process. Mag.* 2012, 29, 127-140,
   DOI: 10.1109/MSP.2012.2205285.
- Khaykin, D.; Rafaely, B. Acoustic analysis by spherical microphone array processing of room impulse responses. *J. Acoust. Soc. Am.* 2012, *132*, 261-270, DOI: http://dx.doi.org/10.1121/1.4726012.
- 3. Mabande, E.; Kowalczyk, K.; Sun, H.; Kellermann, W. Room geometry inference based on spherical microphone array eigenbeam processing. *J. Acoust. Soc. Am.* 2013, 134, 2773-2789, DOI: http://dx.doi.org/10.1121/1.4820895.
- 269 4. Park, M.; Rafaely, B. Sound-field analysis by plane-wave decomposition using spherical microphone array. *J. Acoust. Soc. Am.* 2005, *118*, 3094-3103, DOI: http://dx.doi.org/10.1121/1.2063108.
- Zhang, L.; Ding, D.; Yang, D.; Wang, J.; Shi, J. Sound Source Localization Using Non-Conformal Surface
  Sound Field Transformation Based on Spherical Harmonic Wave Decomposition. *Sensors* 2017, 17, 1-12,
  DOI: 10.3390/s17051087.
- Adiri, O.; Rafaely, B. Localization of multiple speakers under high reverberation using a spherical microphone array and the direct-path dominance test. *IEEE/ACM Trans. Audio Speech Lang. Process.*276 2014, 22, 1494-1505, DOI: 10.1109/TASLP.2014.2337846.
- 277 7. Sun, H.; Mabande, E.; Kowalczyk, K.; Kellermann, W. Localization of distinct reflections in rooms using
  278 spherical microphone array eigenbeam processing. *J. Acoust. Soc. Am.* 2012, *131*, 2828-2840,
  279 DOI: http://dx.doi.org/10.1121/1.3688476.
- Mestre, X.; Lagunas, M. Á. Modified subspace algorithms for DoA estimation with large arrays. *IEEE Trans. Signal Process.* 2008, *56*, 598-614, DOI: 10.1109/TSP.2007.907884.
- 9. Hu, Y.; Lu, J.; Qiu, X. A maximum likelihood direction of arrival estimation method for open-sphere microphone arrays in the spherical harmonic domain. *J. Acoust. Soc. Am.* 2015, *138*, 791-794, DOI: http://dx.doi.org/10.1121/1.4926907.
- Rafaely, B. Analysis and design of spherical microphone arrays. *IEEE Trans. Speech Audio Process.* 2005, 13, 135-143, DOI: 10.1109/TSA.2004.839244.
- 287 11. Rafaely, B. Fundamentals of spherical array processing. Springer: Berlin, 2015; pp. 57-99, ISBN 978-3-662-45663-7.
- 289 12. Chen, C. E.; Lorenzelli, F.; Hudson, R. E.; Yao, K. Maximum likelihood DOA estimation of multiple
  290 wideband sources in the presence of nonuniform sensor noise. *EURASIP J. Adv. Signal Process.* 2007, 2008,
  291 1-12, DOI: https://doi.org/10.1155/2008/835079.
- 292 13. Tervo, S.; Politis, A. Direction of arrival estimation of reflections from room impulse responses using a
  293 spherical microphone array. *IEEE/ACM Trans. Audio Speech Lang. Process.* 2015, 23, 1539-1551,
  294 DOI: 10.1109/TASLP.2015.2439573.
- 295 14. Chen, J. C.; Hudson, R. E.; Yao, K. Maximum-likelihood source localization and unknown sensor location
  296 estimation for wideband signals in the near-field. *IEEE Trans. Signal Process.* 2002, *50*, 1843-1854,
  297 DOI: 10.1109/TSP.2002.800420.
- 298 15. Dennis, Jr, J. E.; Moré, J. J. Quasi-Newton methods, motivation and theory. *SIAM review* 1977, 19, 46-89, DOI: https://doi.org/10.1137/1019005.
- 300 16. Meyer, J.; Elko, G. A highly scalable spherical microphone array based on an orthonormal decomposition
  301 of the soundfield. In Proceedings of the IEEE International Conference on Acoustics, Speech, and Signal
  302 Processing (ICASSP), Orlando, FL, USA, May 2002; pp. 1781-1781, DOI: 10.1109/ICASSP.2002.5744968.
- 303 17. Jarrett, D. P.; Habets, E. A. P.; Thomas, M. R. P.; Naylor, P. A. Rigid sphere room impulse response
  304 simulation: Algorithm and applications. *J. Acoust. Soc. Am.* 2012, *132*, 1462-1472,
  305 DOI: http://dx.doi.org/10.1121/1.4740497.
- 306 18. Allen, J. B.; Berkley, D. A. Image method for efficiently simulating small-room acoustics. *J. Acoust. Soc. Am.* 307 1979, 65, 943–950, DOI: http://dx.doi.org/10.1121/1.382599.
- Rafaely, B. Bessel nulls recovery in spherical microphone arrays for time-limited signals. *IEEE Trans. Audio Speech Lang. Process.* 2011, *19*, 2430-2438, DOI: 10.1109/TASL.2011.2136338.