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Abstract

 Nanoscale zero-valent iron (nZVI), with its high reactivity towards a broad range of contaminants, has been a promising material for groundwater remediation. Membrane- supported nZVI can both avoid nZVI agglomeration for better reactivity and recycle nZVI to lower the risk of secondary pollution. In this study, we successfully fabricated a PVDF-GO membrane via electrospinning technology and employed the functionalized nanofiber membrane to immobilize nZVI particles. The addition of GO into PVDF nanofibers can both increase the hydrophilicity to improve membrane flux and offer –COOH as a binder to immobilize nZVI particles. PVDF-GO-nZVI membranes with different GO loadings (0%, 0.5%, 1%, 3% of PVDF) were tested with two typical nZVI-targeted contaminants (Cd(II) and trichloroethylene (TCE)) via gravity-driven membrane filtration. The results show that membrane with 1% GO had the best nZVI distribution against the aggregation and a better performance in both Cd removal (100%) and TCE removal (82%). The nZVI membrane had an high flux in gravity-driven filtration at 255LMH for Cd(II) and 265LMH for TCE respectively. Generally, the developed PVDF-GO-nZVI electrospun nanofiber membrane had an excellent performance in the gravity-driven membrane filtration system for groundwater remediation.

 Keywords: nano-scale zero valent iron, electrospun nanofiber membrane, graphene oxide, groundwater remediation, gravity-driven membrane filtration

1. Introduction

47 With the rapid urban and economic development and the growing population, contaminants in groundwater has become complex and intractable. Various pollutants like heavy metals, chlorinated organics and dyes seriously influence the quality and safety of groundwater (Vidmar et al., 2018). Nanoscale zero-valent iron particles (nZVI), with their high reactivity towards a broad range of contaminants, are widely used in groundwater remediation (Tosco et al., 2014). However, nZVI particles themselves are prone to agglomeration, sedimentation and oxidization (Dong et al., 2017; Lefevre et al., 2016). Traditional methods to address these issues are to add surfactants (Kim et al., 2010), suspending agents and stabilizers (Hwang et al., 2014) to maintain the uniformity and activity of nZVI particles distributed in the groundwater. Though nZVIs particles are effective in removing the target pollutants, the adsorbed auxiliary additives and contaminants and the nZVI particles themselves may pose a risk of secondary pollution as long as they remained in groundwater without retrieving them (Dong et al., 2012).

60 To solve these issues, immobilizing the nZVI particles on a high-surface area membrane substrate would be recycled and potentially reduce the risk of secondary pollution, thus this approach of nZVI particle-loaded membrane is put forward here (Wan et al., 2017). An ideal substrate for nZVI would be a membrane with high specific surface area, recyclable and easily- functionalized properties, which not only can stably immobilize nZVI to avoid agglomeration and sedimentation, but also can recycle nZVI particles or adsorbed contaminants after use (Ren et al., 2017a). Electrospinning is one of the alternative membrane fabrication technologies but has only found its application for nZVI immobilization in recent years due to its low cost, large specific area, size-controllable and easily-functional properties (Ren et al., 2017b). PVA-PAA membrane have been used to immobilize nZVI particles and the PVA-PAA-nZVI membrane had an excellent removal on trichloroethylene (TCE) (Ma et al., 2012). Liu et al. (Liu et al., 2014) also successfully immobilized nZVI particles onto a polyacrylonitrile (PAN)-based oxidized membrane to reduce water contaminants, which had shown an excellent removal performance. However, these kinds of membranes are lacking mechanical strength (Bichara et 74 al., 2014) or chemical stability (Manavi - Tehrani et al., 2010) and hard to be employed in a long-term filtration process. Although, in our previous studies (Ren et al., 2017b; Ren et al., 2019), we have successfully improved the immobilization of nZVI and mechanical strength of the PVA-PAA-nZVI membrane, it still had some difficulties in nZVI regeneration due to lack of chemical/ acid-base resistance.

 Polyvinylidene fluoride (PVDF) with its strong mechanical strength and excellent chemical stability has already been one of the most commonly-used materials in membrane fabrication (Kang and Cao, 2014). However, PVDF is highly hydrophobic and does not have active functional groups to bind with nZVI particles (Boo et al., 2016). To solve the problem, graphene oxide (GO) with good hydrophilicity and a large number of carboxylic groups (– COOH) could be a good additive to improve membrane hydrophilicity and introduce –COOH onto PVDF membrane for nZVI immobilization (Wang et al., 2014a). Jang et al. (Jang et al., 2015) fabricated PVDF-GO membrane by electrospinning and improved membrane flux due to the introduction of GO in microfiltration process. However, the research on both using PVDF-GO membrane for nZVI immobilization and its application via gravity-driven membrane filtration process has not been reported yet.

 Thus, this study aims to fabricate a PVDF-GO nanofiber membrane by electrospinning and the fabricated membrane was used to immobilize nZVI particles by in-situ synthesis method. The effect of GO on membrane fabrication and hydrophilicity were characterized by scanning electron microscopy (SEM), attenuated total reflectance - fourier transform infrared spectroscope (ATR-FTIR), X-ray diffraction (XRD), contact angle and mechanical strength.

 The immobilization performance of nZVI was examined by SEM, energy dispersive X-ray spectrometry (EDX), Thermo-gravimetric analysis (TGA), XRD and pore size. Two typical nZVI-targeted contaminants (cadmium (Cd) and TCE, as representatives of heavy metal and chloride organics) were separately filtered by the fabricated PVDF-GO-nZVI membranes via gravity-driven filtration process. The effect of nZVI particles and contaminants on membrane flux and removal performance were tested as well.

2. Materials and methods

2.1 Materials

 PVDF (Kynar® 761, Mw = 441,000 g/mol) was purchased from Arkema InC., Australia. Graphene oxide (GO), ferrous sulfate heptahydrate (FeSO4·7H2O), sodium borohydride 105 (NaBH₄), cadmium nitrate $(Cd(NO_3))$, trichloroethylene (TCE), ethanol and n-hexane were all purchased from Sigma-Aldrich. De-ionized (DI) water from a Millipore Milli-Q water system was used; all the oxygen-free water was prepared by purging nitrogen gas for 10 min to remove the dissolved oxygen and avoid the oxidation of nZVI particles. All chemicals were used as received.

2.2 Solution preparation and electrospinning of PVDF-GO nanofiber membranes

 GO particles with different ratios (**Table 1**) were added into a mixed solvent composed of DMF and acetone (3:1 by wt%) at room temperature with sonication for 3 h to make it well- distributed. Then PVDF powders were dissolved into the GO-mixed solvent by stirring for 48 h at room temperature.

115 The electrospinning set-up is similar to our previous study (Ren et al., 2017b). Nanofibers were directly fabricated onto a rotating drum collector covered with baking paper in a sealed chamber. The feed flow rate was controlled at 1 ml/h by a syringe pump. All the fabricated mats were electrospun at an employed voltage of 18 kV and the tip-to-collector distance (TCD) was 15 cm.

 The polymer solution was supplied by a 12 ml syringe attached with a needle (21G, inner diameter = 0.51 mm) connected via a metallic adaptor. The membranes thickness were 122 controlled at 100 \pm 5 µm. The as-spun membranes were dried in oven at 60 °C for 48h to remove the residual solvent.

Table 1. Composition of PVDF-GO solution for electrospinning

Membrane	$PVDF(wt\%)$	$GO/PVDF(wt\%)$	DMF $(wt\%)$	Acetone $(wt\%)$
PVDF	15		68	
PVDF-GO0.5		0.5		
PVDF-GO1				
PVDF-GO3				

2.3 Synthesis of nZVI on the PVDF-GO membrane

 Fig. 1 shows the schematic of the synthesis of nZVI-decorated PVDF-GO membranes. All the PVDF-GO membranes were first filtered with 0.2 mol/L FeSO4 solution for 3 h to allow the complexation of ferrous ions (see **Fig. 1**). After that, all the PVDF-GO-Fe(II) membranes 130 were filtered with 0.5 mol./L NaBH₄ solution in an anaerobic chamber (filled by N₂ gas) to form and immobilize nZVI particles. The reaction is shown below (Wang et al., 2008),

132
$$
Fe^{2+} + 2BH_4^- + 6H_2O \rightarrow Fe^0 \downarrow + 2B(OH)_3 + 7H_2 \uparrow
$$
 (1)

 The successful formation of nZVI on the PVDF-GO membrane is indicated by the change 134 of color of the mat into black, and once the black color was stable (~10 mins generation time), the PVDF-GO-nZVI mats were rinsed by ethanol then stored in a sealed glass bottle, which was filled with nitrogen gas.

Figure 1. Schematic diagram of the nZVI particles growth and re-immobilization

2.4 Gravity-driven membrane filtration

 To test the performance of PVDF-GO-nZVI membranes on a relatively real condition of groundwater remediation, all the membranes were used to filtrate Cd(II) and TCE solutions seperately by a gravity-driven membrane filtration application.

 Schematic diagram of the filtration set-up is shown in **Fig. 2**. The thickness of each mat 144 was controlled at 100 \pm 10 µm and the area for filtration was 14 cm². The initial Cd(II) concentration was 20 mg/L and 100 ml solution was filtered in each filtration cycle (5 cycles 146 for 500 mL in total). 10 mL permeated sample was withdrawn after each filtration cycle for the analysis of Cd(II) concentration via microwave plasma-atomic emission spectrometry (4100 MP-AES, Agilent Technologies, US). Removal efficiency to Cd(II) was determined using the following equation:

150 Removal efficiency (
$$
\%
$$
) = $\frac{C_{\text{int}} - C_{\text{end}}}{C_{\text{int}}} \times 100\%$ (2)

151 where, C_{int} and C_{end} refer to the initial and final Cd(II) concentrations, respectively.

Figure 2. Schematic diagram of nZVI membrane gravity-driven filtration system

 In addition, TCE as a typical chloride organic was also selected to test the dechlorination capacity of PVDF-GO-nZVI membrane. Similarly, the concentration of TCE was also 20 mg/L but the permeated sample was withdrawn and transferred to a new vial for the subsequent liquid-liquid extraction. The chemical n-hexane was used to extract TCE from water. The concentration of the extracted TCE solution was measured by GC-MS-TQ8040 (Shimadzu, Japan). The removal efficiency was calculated using the following equation:

161
$$
\text{TCE removal efficiency } (\%) = \frac{c_{\text{int}} - c_{\text{end}}}{c_{\text{int}}} \times 100\%
$$
 (3)

162 where, C_{int} and C_{end} are the initial and the final TCE concentrations, respectively.

2.5 Membrane Characterizations

 Membrane surface morphology and element component analysis were measured by scanning electron microscopy and energy dispersive X-ray spectrometry (SEM and EDX, Zeiss Supra 55VP, Carl Zeiss AG). All the fiber/particle sizes and distributions were measured by Image J.

 Thermo-gravimetric analysis (TGA) was measured by Discovery TGA thermo-gravimetric 168 analyzer (SDT-Q600, US) from 80°C to 800°C at a heating rate of 10°C/min in N₂ atmosphere [27]. The functional groups of membranes/particles were analyzed by attenuated total reflectance Fourier transform infrared spectroscopy (ATR-FTIR) via Paragon 1000 Spectrometer (PerkinElmer, USA), wavelength from 600 to 4000 cm-1 with a minimum of 40 scans. X-Ray diffraction (XRD) (Siemens D5000) was carried out over Bragg angles ranging 173 from 1° to 80° (Cu K α , λ =1.54059Å) (Woo et al., 2016). The mechanical properties of different membrane samples were measured using a Universal Testing Machine (UTM, Lloyd), equipped with a 1 kN load cell. The test was conducted using a constant elongation velocity of 5 mm/min under room temperature (Woo et al., 2017). Galwick (surface tension of 15.9 mN/m) 177 was used to wet the membranes in pore size. Each sample was first applied with N_2 gas to measure the gas permeability. A sessile drop method utilizing Theta Lite 100 (Attension, Sweden) with built-in software was used to analyses the contact angles of all the membranes (Yao et al., 2019). A water droplet around 5 µl was released from a needle tip onto the membrane surface. A motion camera was mounted to take photos at a rate of 12 frames per second. Each sample was measured for three times and the average value was taken.

3. Results and discussion

3.1 Effect of GO on PVDF membranes

Fig. 3 shows the SEM images and fiber size distributions of as-spun PVDF-GO nanofiber membranes with different GO ratios. All the membranes showed bead-less and defect-free cylindrical nanofiber structure. The average fiber sizes of the as-spun membranes (PVDF, 188 PVDF-GO0.5, PVDF-GO1 and PVDF-GO3) were 167 ± 79 , 259 ± 129 , 311 ± 131 and 355 ± 129 237 nm, respectively. It is clear that the fiber size increased with the increase in the GO added into the PVDF solution. However, the addition of GO broke the continuity of polymer jetting during the electrospinning, which resulted to a wider fiber size distribution. Similar results were also reported in previous studies (Jang et al., 2015).

 Figure 3. Surface SEM images and corresponding fiber size distributions of (a) PVDF; (b) PVDF-GO0.5; (c) PVDF-GO1 and (d) PVDF-GO3 electrospun nanofiber membranes

 Fig. 4 shows the ATR-FTIR spectra of the PVDF-GO membranes. For the pristine PVDF, 197 the characteristic absorption band is mainly in the wavenumber region of $840 - 1402$ cm⁻¹. 198 Specifically, the peak intensities at 1181, 1275 cm⁻¹ represents symmetrical stretching of $-CF$ and −CF₂ stretching, while peaks at 840, 883, 1070 and 1402 cm⁻¹ represents the −CH₂ rocking, −CH2 wagging of vinylidene, bending of −CH bond and the stretching vibration of C-H bonds (Ghaffar et al., 2018; Zeng et al., 2016) respectively. In terms of GO membranes, The peaks at 202 1622, 1720 and 3500 cm⁻¹ indicated the existence of C=C, -COOH and -OH, which proved the deposition of GO onto the PVDF membrane (Ghaffar et al., 2018). With the increase of GO ratio, the peak of –COOH and C-OH increased correspondingly but the characteristic peaks of PVDF reduced due to the ratio of PVDF in the composite reduced as well. The XRD results of 206 all the electrospun membranes are presented in Fig. 5. There are clear peaks at $2\theta = 10.5^{\circ}$ on all the PVDF-GO membranes indicating the existence of GO. The peak intensity increased with the increase of GO/PVDF ratio and PVDF-GO3 had the highest GO peak intensity, which was consistent with FTIR results (**Fig. 4**).

211 **Figure 4.** ATR-FTIR spectra of all the PVDF-GO elelctrospun nanofiber membranes

212

213 **Figure 5.** XRD patterns of all the PVDF-GO elelctrospun nanofiber membranes

214 A contact angle measurement was conducted on the PVDF-GO membranes and the results 215 are shown in **Fig. 6**. The pristine PVDF membrane showed the highest contact angle of $140 \pm$ 216 1.9°, indicating being highly hydrophobic. Expectedly, the addition of GO nanoparticles 217 significantly reduced the contact angle of PVDF membrane, because the –COOH and -OH on 218 GO are hydrophilic. With the increase of GO ratio, the average contact angle reduced from 219 140° to 110° and the PVDF-GO3 had the lowest contact angle at 110 ± 4.2 °.

220

221 **Figure 6.** Contact angles of all the PVDF-GO electrospun nanofiber membranes

	Tensile strength (MPa)	Strain (%)	Young's modulus (MPa)
PVDF	6.4	49.3	13
PVDF-GO0.5	5.2	27	19.3
PVDF-GO1	4.8	12.6	38.1
PVDF-GO3	4.4	9.5	46.3

 Table 2. Mechanical properties of the neat PVDF and PVDF-GO electrospun nanofiber membranes

 The mechanical properties of the neat PVDF membrane and the PVDF-GO membranes are presented in **Table 2**. It is obvious that the addition of GO led to a decrease of the tensile strength as well as the percentage of the strain. With the increase of GO ratio in the membrane, the tensile strength decreased from 6.4 MPa to 4.4 MPa and the strain reduced from 49.3% to 9.5%. However, the Young's modulus increased from 13 MPa to 46.3 MPa, which means the more GO added, the more plastic the nanocomposites will be. Although the PVDF-GO membranes became more plastic, they had a better resistance to deformation of fiber structure (Ren et al., 2019).

3.2 Immobilization of nZVI onto PVDF-GO membrane

235 The surface SEM images of all the nZVI-immobilized PVDF-GO membranes are shown in **Fig.7**. It is clear that nZVI nanoparticles have been successfully generated on each PVDF- GO membrane. However, the neat PVDF membrane without GO did not show a good immobilization of nZVI due to the lack of functional groups and only a few nZVI particles were stuck among fibers via physical interaction other than chemical bonding. With the increase of GO content in PVDF nanofiber, nZVI immobilized on PVDF-GO membranes increased as well. It is noticed that although PVDF-GO3 seemed to have the most nZVI particles immobilized onto nanofibers, the particles were more aggregated and not well- distributed (**Fig. 7c**). Specifically, nZVI particles were more immobilized on the thin fibers 244 than thicker fibers. This is due to the fact that the functional moieties (-COOH) are mainly on the edge of GO and the edges of GO are more likely to pierce the surface of thinner fibers rather than encapsulated inside the thicker fiber (Hu et al., 2016). **Fig. 7e** shows the Fe/C weight ratio of each nZVI membrane by EDS analysis in the SEM images and the results are highly consistent with the SEM images. The Fe/C ratio of neat PVDF was extremely low at 0.02, approximately 1/50 lower than those on PVDF-GO membranes, which indicates that the neat PVDF membrane failed to immobilize nZVI particles. In contrast to PVDF-GO membranes, with the ratio of GO added into PVDF membrane, the Fe/C ratio increased significantly. PVDF-GO3-nZVI (**Fig. 7d**) had the highest Fe/C ratio at 2.03 on its membrane surface, around 1.5 times higher than that on PVDF-GO1-nZVI (**Fig. 7c**).

 Figure 7. Surface SEM images of: (a) PVDF-nZVI; (b) PVDF-GO0.5-nZVI; (c) PVDF-GO1- nZVI; (d) PVDF-GO3-nZVI electrospun nanofiber membranes; and (e) the weight ratio of Fe/C on the surface of the four nZVI-immobilized electrospun nanofiber membranes based from EDS analysis.

261 The pore size of PVDF-GO membranes before and after nZVI immobilization are presented in **Table 3**. Before the immobilization of nZVI, the mean pore size increased with the GO content (from 0.8 μm to 1.21 μm) due to the increase of fiber size (Wang et al., 2014b). After nZVI immobilization, all the membrane pore sizes decreased and the pore size of the membrane with a higher GO ratio reduced more significantly. This is mainly because the nZVI particles were deposited on the surface of fibers and then occupied the voids among the fibers. Membrane with high GO ratio immobilized more nZVI particles and hence the pore size reduced more.

Table 3. Mean pore sizes of PVDF-GO membranes before/after nZVI immobilization

	Mean pore size (μm)		Mean pore size (μm)
PVDF	0.8	PVDF-nZVI	0.79
PVDF-GO0.5	0.99	PVDF-GO0.5-nZVI	0.95
PVDF-GO1	1.13	PVDF-GO1-nZVI	1.06
PVDF-GO3	21	PVDF-GO3-nZVI	

285 on the surface (**Fig. 7d**), its pore size decreased significantly by nZVI blocking and hence 286 hindering the generation of nZVI inside the membrane, leading to a lower Fe/C ratio inside.

17 288 **Figure 8.** Cross-sectional SEM images of (a) PVDF-nZVI; (b) PVDF-GO0.5-nZVI; (c) PVDF-289 GO1-nZVI; (d) PVDF-GO3-nZVI electrospun nanofiber membranes and (e) the weight ratio 290 of Fe/C on the cross-sectional of the four nZVI immobilized electrospun nanofiber membranes 291 XRD results of nZVI-incorporated PVDF-GO electrospun nanofiber membranes are 292 presented in **Fig. 9**. The peak at 45° represents the crystal structure of α-Fe (110), indicating

 the existence of nZVI onto PVDF-GO membranes (Gu et al., 2018), although the intensity of the peak was not very high due to a less mass ratio of nZVI on the nanocomposites and the strong peak of amorphous structure of PVDF-GO electrospun nanofiber membranes.

Figure 9. XRD pattern of all the PVDF-GO-nZVI electrospun nanofiber membranes

 TGA was used to characterize the loading capacity of nZVI particles immobilized onto the dual-crosslinked nanofiber membranes (**Fig. 10**). The weight loss on each membrane on the temperature range from 150 to 400℃ indicates the decomposition of GO (Issa et al., 2016; 301 Sinoforoğlu et al., 2013). Afterwards, the major weight loss at the region from 400 to 500 °C is attributed to the decomposition of the PVDF polymers(Thakur et al., 2011). Obviously, the neat PVDF without GO decreased the most weight percentage.

 At 800℃, all the polymeric nanofibers had already been decomposed, leaving carbons and nZVI particles as the residual mass (Sharma et al., 2015). Neat PVDF remained only carbon and few nZVI particles at 9.6 wt%. PVDF-GO3 immobilized the most nZVI with about 37.8 wt%, while PVDF-GO1 immobilized the second most nZVI around 33.1 wt%, around 28.2% and 23.5% higher than the neat PVDF. Basically, PVDF with a higher GO ratio immobilized more nZVI particle, which is consistent with SEM results.

312 **Figure 10.** TGA of all the PVDF-GO-nZVI electrospun nanofiber membranes

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315 Contact angles after nZVI immobilization on the membranes are presented in **Fig. 11**. 316 All the membranes reduced contact angle after nZVI immobilization due to the hydrophilicity 317 of the oxide shell on the nZVI surface. With the least nZVI immobilized, the PVDF-nZVI 318 remained the highest contact angle at $139 \pm 2.2^{\circ}$. There is relative larger improvement of 319 hydrophilicity on PVDF-GO membranes. The contact angle of PVDF-GO0.5-nZVI was $125±$ 320 2.9°, around 6° lower than that before nZVI immobilization. PVDF-GO1-nZVI was improved 321 the most, whose contact angle reduced by 8° from $119 \pm 2.4^{\circ}$ to $111 \pm 2.7^{\circ}$. However, the 322 contact angle of PVDF-GO3-nZVI only decreased around 4° which did not show a better improvement than PVDF-GO1-nZVI. Although PVDF-GO3 membrane immobilized the most amount of nZVI particles, those nZVI particles are more aggregated, leading to increase surface roughness, which can only improve the hydrophilicity on the part where the nZVI particles gathered.

3.3 Performance of PVDF-GO-nZVI membrane in removing contaminants via gravity-driven membrane filtration

 All the nZVI-immobilized electrospun nanofiber membranes were tested via gravity- driven membrane filtration, with water head controlled at 0.4 m. Two typical nZVI-targeted contaminants (Cd(II) and TCE) were employed to test the permeability and removal performance of nZVI-immobilized electrospun nanofiber membranes.

 Fig. 12 shows the evolution of flux and Cd(II) removal with the increase of filtration volume. The flux of each membrane decreased with the filtration of Cd(II) solution (**Fig. 12a**). PVDF-nZVI (i.e., without GO) had the lowest flux (from 98 LMH to 70 LMH) among the four membranes due to the smallest membrane pore size and the strongest hydrophobicity. In contrast, with the increase of GO content, the mean pore size and the hydrophilicity of PVDF- GO membranes increased remarkably, thereby contributing to a better permeability. PVDF- GO3-nZVI had the highest initial flux at 269 LMH followed by PVDF-GO1-nZVI at 255 LHM. However, the flux of PVDF-GO3-nZVI declined significantly. After 100 mL filtration, the flux of PVDF-GO3-nZVI was lower than that of PVDF-GO1-nZVI. This is because, with the adsorption of Cd(II) on the surface of nZVI particles, the size-increased nZVI made the membrane pore volume and pore size reduced. Furthermore, nZVI particles on the PVDF-GO3 are more aggregated and hence the pore size reduced more significantly. In **Fig. 12b**, the PVDF-nZVI had a very little removal lower than 8% over the whole filtration test while all the PVDF-GO-nZVI membranes had 100% initial removals of Cd(II). PVDF-GO1-nZVI kept the

 Figure 12. Performances of PVDF-GO-nZVI electrospun nanofiber membranes in gravity-driven membrane filtration test for Cd(II) removal: (a) Flux and (b) Cd(II) removal ratio

 In terms of TCE filtration test (**Fig. 13**), the flux of each membrane (**Fig. 13a**) was obviously higher than the flux in Cd(II) filtration test (**Fig. 12a**). Meanwhile, the flux decline of each nZVI membrane in TCE filtration was slower than those in Cd filtration. These could be respectively explained by the followed two reasons: (1) TCE itself is a hydrophobic liquid (Kiruthika et al., 2014), which has a similar hydrophobicity with the PVDF fibers (Woo et al., 2016). Therefore, it had a higher flux for TCE than Cd(II) solution (2) In contrast to the adsorption of nZVI to Cd(II), the mechanism of TCE removal was the dechlorination process (**Fig. 14b**), which means TCE would not deposit on the surface of nZVI particles. It is reported that TCE was first broken by electron attack originating from the surface of nZVI, and dichloroethylenes (DCE) are formed as intermediates (Tian et al., 2018). Subsequently, DCE was dechlorinated to vinyl chloride (VC) and eventually all dichloroethylene formed was completely dechlorinated to ethylene and ethane (Hara et al., 2005). nZVI was reduced to Fe(OH)₂ in the anaerobic groundwater ambience (Tian et al., 2018). Therefore, TCE molecule would not adsorb on nZVI surface and hence remained higher pore sizes, fluxes and removal. Particularly, PVDF-GO3-nZVI with the largest mean pore size had the highest initial flux at 317 LMH and PVDF-nZVI with the smallest mean pore size had the lowest initial flux at 123 LMH. It is noticed that the flux of PVDF-GO1-nZVI is just a bit lower than that of PVDF- GO3-nZVI but much higher than those of PVDF-GO0.5-nZVI and PVDF-nZVI. Nevertheless, the PVDF-GO3-nZVI had a higher pore size, its flux is still limited by the undesirable aggregation of nZVI. On the other hand, the TCE removals of all the membranes (**Fig. 13b**) were obviously lower than their removals for Cd(II) (**Fig.12b**). This may be caused by two reasons: 1) the higher flux of membrane made TCE molecules have less hydraulic retention time to contact and react with nZVI particles. 2) The dechlorination process of TCE was multi- steps (**Fig.14b**), which had a lower total reaction rate than Cd(II) and requires more reaction time. Specifically, PVDF-nZVI had the lowest removal no more than 4% over the whole filtration test and PVDF-GO0.5-nZVI had a very little removal lower than 10% after 100ml. In contrast, PVDF-GO1-nZVI had the highest removal at 82% at the 100 ml. Although PVDF-GO3-nZVI had a slightly higher flux over 500 ml, PVDF-GO1-nZVI with the overwhelming removal had a better performance in the filtration test. Generally, PVDF-GO1-nZVI had the

Figure 13. Performances of PVDF-GO-nZVI electrospun nanofiber membranes in gravity-

driven membrane filtration test for TCE removal: (a) Flux and (b) TCE removal ratio

Figure 14. Mechanism of (a) Cd^{2+} and (b) TCE removal by PVDF-GO-nZVI electrospun

nanofiber membranes

4. Concluding remarks

- > The more ratio of GO added in PVDF membrane, the more nZVI can be immobilized, but too high GO ratio could make an uneven fiber size distribution in electrospinning process
- and hence can lead to nZVI aggregation.
- 411 \triangleright For Cd removal, as the adsorption mechanism made the Cd(II) deposited on the surface of nZVI, PVDF-GO1-nZVI had a better nZVI distribution against the agglomeration, leading to a better removal (100%) and flux (255 LMH).
- 414 \triangleright For TCE removal, although PVDF-GO3-nZVI had a slightly higher flux (317 LMH), PVDF-GO1-nZVI with the overwhelming removal (82%) had a better performance in the
- filtration test.

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