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# Circular-Polarized Substrate-Integrated-Waveguide Leaky-Wave Antenna with Wide-Angle and Consistent-Gain Continuous Beam Scanning

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**Abstract**—Circularly-polarized (CP) antennas are highly desired for future wireless communications. To advance the development of CP substrate-integrated-waveguide (SIW) leaky-wave antennas (LWAs) with the intent to meet this demand, a novel benzene-ring-shaped slot-loaded LWA with partially reflecting wall (PRW) vias is investigated and verified to realize wide-angle continuous beam scanning with consistent gain. The dispersion features of slot-loaded SIW LWAs with PRW vias are theoretically explored using an equivalent circuit model. The CP radiation feature is investigated numerically utilizing the E- and H-field distributions of an initial design and its equivalent magnetic currents. The results of these studies are used to demonstrate that improved CP performance over a wide-angle scan range can be attained with a change from a standard slot shape to a benzene-ring-shaped slot. The resulting benzene-ring-shaped slot-loaded CP SIW LWA was optimized, fabricated, and measured. The measured results verify that a CP beam was continuously scanned through a wide angle from backward to forward directions with a consistent gain. The prototype exhibits a continuous 97.1° CP beam scan with a gain variation between 8 and 11.3 dBic when the source frequency is swept from 9.35-11.75 GHz.

**Index Terms**—Circular polarization (CP), consistent gain, continuous beam scanning, leaky-wave antenna (LWA), substrate integrated waveguide (SIW).

## I. INTRODUCTION

**L**EAKY-wave antennas (LWAs) are highly promising candidates for future wireless communications and sensing systems based on emerging platforms such as drones and small satellites, where low-cost and low-profile antennas are required. Generally, they radiate power as a traveling wave propagates across “open” regions along its aperture. Their main beam directions can be steered by varying their source frequencies [1], [2]. Correspondingly, LWAs can bring significant benefits including a simple feed network, wide-angle beam scanning, a low profile and cost effectiveness [3]–[7]. However, for applications to radar and satellite communication systems, it is also preferred to radiate a circularly polarized

(CP) wave rather than a linearly polarized (LP) one, i.e., the CP LWAs are highly desired to avoid polarization mismatch and to suppress multi-path interference during beam scanning [8]–[10].

Some challenges exist in achieving frequency-dependent, continuous beam scanning from a CP LWA. First, it is known that for the LWAs working at frequency  $f$ , the main beam angle  $\theta(f)$  in its leaky region is determined with the relation:

$$\theta(f) = \sin^{-1}[\beta(f)/k_0(f)] \quad (1)$$

where  $\beta(f)$  is the phase constant of the leaky wave mode in the guiding structure, and  $k_0(f)$  is the corresponding propagation constant in air. In order for it to scan the main beam from the backward to the forward direction, a CP LWA must facilitate both positive and negative phase constants. Second, the radiated fields must have two perpendicular components with the same amplitude and a 90° phase difference to be CP waves. This feature must be maintained within the main beam direction as the frequency changes. Moreover, it is known that most periodic LWAs suffer from the open stopband (OSB) problem, i.e., when their beam points at the broadside direction, their realized gain drops significantly [11]–[13]. Furthermore, there are linkages between suppressing the OSB and the consequent CP performance [14]. On the other hand, even if one does suppress the OSB, it remains a challenge to maintain a consistent gain performance over the entire beam scanning range. Thus, a high performance CP LWA must also have solutions for all of these issues.

A planar-modulated surface-based CP LWA has been reported that suppresses the OSB. However, it is unable to scan its main beam [15]. There are some other interesting approaches that also accomplish continuous CP beam scanning through broadside. One technique is to introduce composite right/left-handed (CRLH) unit cells that satisfy their balanced condition. The OSB is suppressed, and the main beam can be scanned in its fundamental mode [16]–[18]. Moreover, by introducing a substrate-integrated-waveguide (SIW) or a microstrip line structure into these CRLH-based LWAs, continuous backward to forward CP beam scanning can be obtained [19]–[22]. Using a half-mode (HM) SIW etched with ramp-shaped slots, a wide-angle continuous backward-to-forward beam scanning was obtained in [21]. Another technique is to use axial-asymmetrical microstrip lines [14], [20]. These series-fed microstrip LWAs introduce an asymmetry in the

Manuscript received XXX. This work was supported by the Australian Research Council (ARC) Discovery Project (DP) 160102219 grant, the Discovery Early Career Researcher Award (DECRA) DE170101203 grant, and the National Natural Science Foundation of China under Grant 61771038. (Corresponding author: Shu-Lin Chen)

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transversal axis to radiate and scan the CP beam as the source frequency is varied. Nevertheless, it is still very challenging to simultaneously achieve good axial ratio (AR) values and a suppressed OSB over a wide angle scan range. A third technique is to employ spoof surface plasmon polaritons (SSPPs) [23], [24]. Circular patches located above a slow-wave SSPP line were reported in [23] to generate the CP wave, and the main beam was continuously scanned from  $-32^\circ$  to  $+34^\circ$  with gain variations between 12.8–14.2 dBic. Yet another popular approach is to use a periodic slot-loaded aperture in a SIW structure. These SIW LWAs have been widely investigated and used due to their easy integration and low loss [25], [26]. An H-shaped slot-loaded SIW reported in [27] realized beam scanning in the forward quadrant from  $20^\circ$  to  $50^\circ$  when the source frequency varied between 10.6 and 11.5 GHz. A slot-loaded periodic SIW CP LWA was reported in [28] that successfully realized continuous beam scanning from  $-40^\circ$  to  $+25^\circ$  through broadside by manipulating the etched slots on the SIW. Again, the realized gain had a large variation between 4.2 to 11 dBic within the scanning range. As all of these examples illustrate, it is a very challenging problem to achieve a wide-angle continuous CP beam scan with consistent gain performance.

In this paper, a novel CP LWA based on a periodic benzene-ring-shaped slot-loaded SIW with partially reflecting wall (PRW) vias is introduced. Analysis and simulation studies demonstrate that it achieves a wide-angle, consistent-gain, continuous beam scanning from backward to forward directions through broadside. A prototype of the optimized design was fabricated and tested. The measured results confirm that it can continuously scan the main beam through a wide angle, ranging from  $-42.8^\circ$  to  $+54.3^\circ$ , with only a 3.3 dB gain variation. The main contributions of this work include the incorporation of both PRW vias and slot elements to substantially enhance the radiation performance and a thorough investigation of the CP beam radiation performance with both equivalent circuits and equivalent radiating sources. Finally, when it is compared to most of the reported CP LWAs, the developed benzene-ring-shaped slot-loaded CP SIW LWA with PRW vias exhibits a better beam-scanning range and gain variation performance.

## II. UNIT CELL REQUIREMENTS TO ACHIEVE CONTINUOUS BEAM SCANNING

Initially, a non-slotted SIW unit cell with partially reflecting wall (PRW) vias was investigated. It is labelled as Unit A in Fig. 1. It is designed on a two-layer copper-clad substrate. The substrate is chosen as F4BM-2 produced by Wangling Company, and the permittivity ( $\epsilon_r$ ), loss tangent ( $\tan\delta$ ), width ( $w_{sub}$ ) and thickness are 3.02, 0.001, 30 mm and 1 mm, respectively. A main patch with a width of  $w_p$  is printed on top of the substrate, and a solid ground plane is placed at the bottom. Two rows of shorting vias are used for connecting the patch to the ground plane. The shorting vias in the upper row have a diameter  $d_1$  and a center-to-center distance  $S$ . They act as a electric wall of the SIW LWA. The shorting vias in the lower row have a diameter  $d_2$  and are separated by a larger distance  $P$  and serve as the PRW. The length of unit cell is also  $P$ .

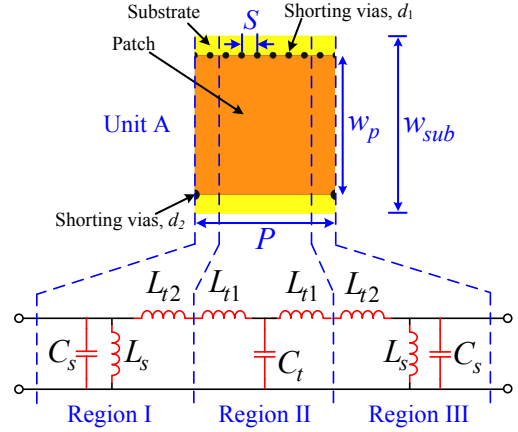


Fig. 1. Top view of the unit cell, Unit A, and its corresponding equivalent circuit.

The analysis of the unit cell is conducted using transmission line theory [29]. The corresponding Unit A equivalent circuit is depicted as shown in Fig. 1. For clearer explanations, the entire unit cell is divided into three regions, marked as Regions I, II and III. The series inductances  $L_{t1}$  and  $L_{t2}$  are introduced by the indicated regions of the main patch, and the shunt capacitances  $C_t$  and  $C_s$  are caused by the capacitive effects between the corresponding regions and the ground plane. The shunt inductance  $L_s$  is introduced by the shorting vias. Due to the placement of the series inductances  $L_{t1}$  and  $L_{t2}$ , a total inductance of  $L_t$  is used for simplicity in the analysis.

The transmission (ABCD) matrix of Unit A is then calculated as:

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1/(j\omega L_s) & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ j\omega C_s & 1 \end{bmatrix} \times \begin{bmatrix} 1 & j\omega L_t \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ j\omega C_t & 1 \end{bmatrix} \times \begin{bmatrix} 1 & j\omega L_t \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ j\omega C_s & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ 1/(j\omega L_s) & 1 \end{bmatrix} \quad (2)$$

where,  $\omega$  is the angular frequency  $\omega = 2\pi f$ , and  $L_t = L_{t1} + L_{t2}$ . The dispersion characteristic is expressed in terms of the transmission line parameters as [30]:

$$\beta = \frac{1}{P} \cos^{-1} \left( \frac{A+D}{2} \right) \quad (3)$$

By solving (2) and (3), the wave number  $\beta$  can be represented as:

$$\beta = \frac{1}{P} \cos^{-1} \left[ -C_t L_t^2 C_s \omega^4 - (2L_t C_s + L_t C_t + \frac{C_t L_t^2}{L_s}) \omega^2 + 2L_t L_s + 1 \right] \quad (4)$$

To obtain the circuit parameter values, one can extract the approximate total patch inductance  $L$  and total capacitance  $C$  of Unit A using the following equations [31]:

$$L \approx \mu_r \mu_0 P h / w_p, \quad \text{and} \quad C \approx \epsilon_r \epsilon_0 w_p P / h \quad (5)$$

where  $\mu_r$  is the relative permeability of the substrate,  $\mu_0$  is the permeability of free space,  $\epsilon_r$  is the relative permittivity

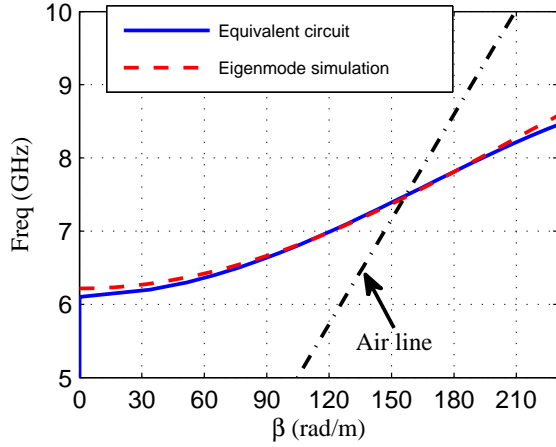


Fig. 2. Dispersion diagrams of the Unit A model obtained with equivalent circuit and eigenmode simulations.

of the substrate,  $\varepsilon_0$  is the permittivity of free space, and  $h$  is the thickness of the substrate. The values (in millimeters) of the Unit A parameters are:  $w_p = 10.7$ ,  $P = 10.8$ ,  $S = 1.2$ ,  $d_1 = 0.5$ ,  $d_2 = 1$ . Substituting these parameter values into (5), the resultant inductance  $L \approx 1$  nH and capacitance  $C \approx 3.3$  pF are obtained. As  $L = 2L_t$  and  $C = 2C_s + C_t$ , the values for  $L_t$ ,  $C_s$  and  $C_t$  become:  $C_s = 1$  pF,  $L_t = 0.5$  nH,  $C_t = 1.3$  pF. Furthermore, the inductance  $L_p$  of the PRW vias can be approximately calculated as [32]:

$$L_p \approx 0.2h \left( \ln \frac{4h}{d_2} + 1 \right) \times 10^{-6} \quad (6)$$

Then by substituting the values of  $h$  and  $d_2$  into it and considering the parallel inductive effects of the shorting vias in the upper row, the inductance  $L_s$  of the shorting vias is approximately obtained as:  $L_s \approx 0.3$  nH.

Applying these calculated circuit parameter values to (4), one can calculate its dispersion feature. The results are labeled as *Equivalent circuit* in Fig. 2. As a comparison, Unit A is also simulated using the eigenmode solver in the full-wave finite element (FEM) simulator ANSYS High Frequency Structure Simulator (HFSS). The resultant dispersion diagram is labeled as *Eigenmode simulation* in Fig. 2. It is seen that the dispersion diagram obtained from the equivalent circuit reasonably agrees with the one from the eigenmode simulation. Referring to Fig. 2, it is known that the left region of the air line is the leaky wave region, i.e.,  $\beta \leq k_0$ . Thus, the LWAs employing Unit A can only radiate forward beams at its fundamental ( $n = 0$ ) mode.

In our previous paper [33], a slot-loaded SIW LWA with PRW vias was reported that produced a continuously scanned LP beam. To achieve a continuous backward-to-forward scanned CP beam, a new unit cell (referred as Unit B) is developed; it is depicted in Fig. 3. Unit B has an I-shaped slot centered on the main patch. As indicated, the dimensions of the slot are  $w_s$ ,  $l_h$ , and  $l_v$ . Based on the Unit A analysis, the Unit B equivalent circuit is given in Fig. 3. The equivalent circuits corresponding to Regions I and III are the same as those of Unit A. In contrast, it is different in Region II. The shunt

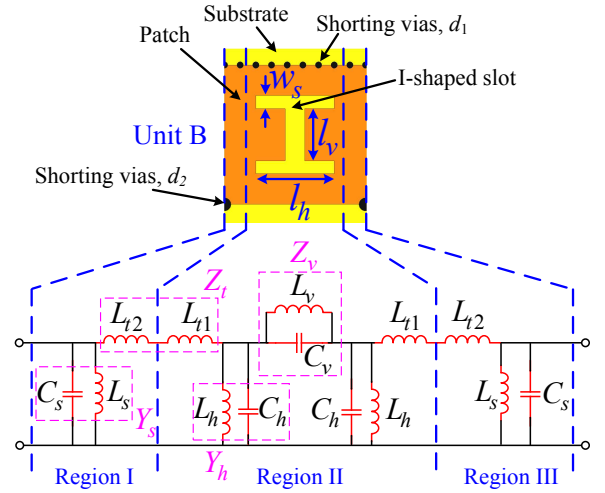


Fig. 3. Unit B model and its corresponding equivalent circuit.

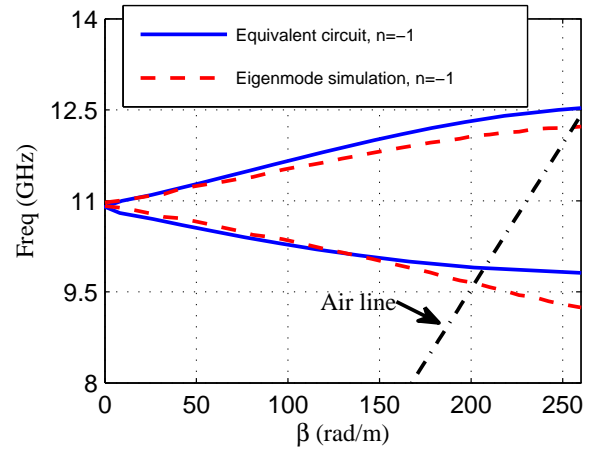


Fig. 4. Unit B dispersion diagrams obtained from its equivalent circuit and eigenmode simulation.

inductance  $L_h$  and shunt capacitance  $C_h$  are introduced by the horizontal part of the I-shaped slot; the series capacitance  $C_v$  is caused by its vertical part. For simplicity, the capacitance introduced between the patch and the ground plane is included in the shunt capacitance  $C_h$ . Again, the series inductances  $L_{t1}$ ,  $L_{t2}$ , and  $L_v$  are introduced by the main patch.

With these additional elements, the transmission (ABCD) matrix of Unit B becomes:

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ Y_s & 1 \end{bmatrix} \times \begin{bmatrix} 1 & Z_t \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ Y_h & 1 \end{bmatrix} \times \begin{bmatrix} 1 & Z_v \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ Y_h & 1 \end{bmatrix} \times \begin{bmatrix} 1 & Z_t \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ Y_s & 1 \end{bmatrix} \quad (7)$$

where element admittances and impedances are

$$\begin{aligned} Y_s &= j\omega C_s + \frac{1}{j\omega L_s}, & Z_t &= j\omega L_t \\ Y_h &= j\omega C_h + \frac{1}{j\omega L_h}, & Z_v &= 1/(j\omega C_v + \frac{1}{j\omega L_v}) \end{aligned} \quad (8)$$

TABLE I  
OPTIMIZED DESIGN PARAMETERS OF THE I-SHAPED SLOT-LOADED SIW LWA WITH PRW VIAS

Parameter	$l_s$	$W_a$	$W_b$	$L_t$	$S$	$d_1$	$d_2$	$P$
Value (mm)	82.8	1.5	7	5	1.2	0.5	0.8	10.8

By solving (3) and (7), the dispersion relation can be expressed in terms of the wave number as:

$$\beta = \frac{1}{P} \cos^{-1} [Z_t Z_v Y_s Y_h (Z_t Y_h + 2) + Z_t Y_h (2Z_t Y_s + Z_v Y_h) + (2Z_t + Z_v)(Y_s + Y_h) + 1] \quad (9)$$

To realize continuous beam scanning, the operating mode of any periodic SIW LWA should be a higher harmonic, such as  $n = -1$  harmonic. The optimized dimensions for the I-shaped slot (in millimeters) are:  $l_h = 6$ ,  $l_v = 4$ ,  $w_s = 1$ . The corresponding updated circuit parameters are:  $L_t = 0.52$  nH,  $L_h = 0.15$  nH,  $C_h = 0.6$  pF,  $L_v = 0.53$  pF, and  $C_v = 1$  pF, while  $L_s$  and  $C_s$  remain the same ( $L_s = 0.3$  nH,  $C_s = 1$  pF). Substituting these circuit parameter values into (8) and (9), the resulting dispersion relation of the  $n = -1$  mode dispersion of Unit B is shown in Fig. 4 and labeled as *Equivalent circuit*. The corresponding dispersion curve obtained from the eigenmode solver is also shown in Fig. 4 and labeled as *Eigenmode simulation*. Both curves agree reasonably well in Unit B's leaky wave region. One observes that there is a continuous transition between the negative and positive regions of the dispersion curves at 10.9 GHz, i.e., the matched condition has been satisfied. Consequently, Unit B has no OSB. This feature appears in contrast to Unit A because the etched I-shaped slot and the PRW vias co-excite the higher harmonic  $n = -1$  mode. Therefore, the Unit B-based SIW LWA can realize continuous beam scanning through broadside.

### III. I-SHAPED SLOT-LOADED SIW LWA WITH PRW VIAS

The continuous beam scanning and CP performance of the I-shaped slot-loaded SIW LWA with PRW vias is analyzed. Details of the antenna configuration are given. The resulting continuous beam scanning and CP features are simulated.

#### A. Antenna Configuration

An I-shaped slot-loaded SIW LWA with PRW vias is developed with six Unit B cells to illustrate its performance characteristics. Fig. 5 shows the top view of the entire antenna configuration. Its optimized dimensions (in millimeters) are summarized in Table I. It is also constructed with the aforementioned two-layer copper-clad F4BM-2 substrate. Two tapered pads, tapering from a width of  $w_a$  to a width of  $w_b$  over the length of  $l_t$ , are used to connect the  $50 \Omega$  feed line to the main patch over a wide bandwidth. The antenna is fed from the left end and terminated on the right end with a matching  $50 \Omega$  load.

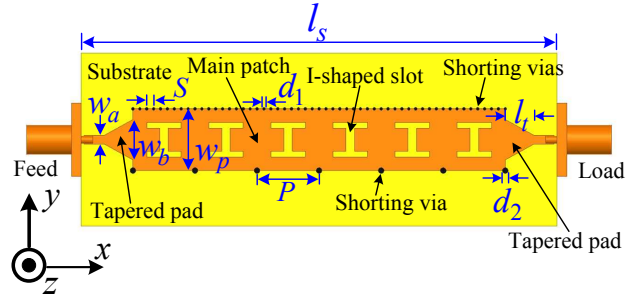


Fig. 5. I-shaped slot-loaded SIW LWA with PRW vias configuration.

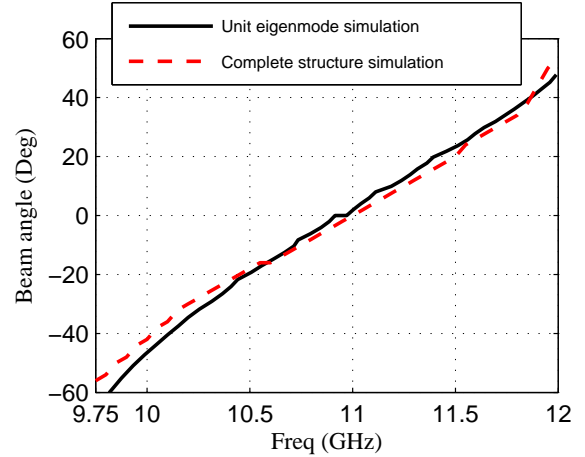


Fig. 6. Main beam angle when the source frequency is varied as calculated from the simulations of the eigenmode (infinite) and complete (finite) structure.

#### B. Beam Scanning

The main beam angle accomplished through the above complete six-cell system simulation is shown in Fig. 6, and the results are labeled as *Complete structure simulation*. Based on the dispersion properties obtained from the eigenmode simulation shown in Fig. 4, the main beam angles can be calculated using (1), and the corresponding results are labeled as *Unit eigenmode simulation* in Fig. 6 for comparison. It is seen that both results agree very well. The minor discrepancies arise from the difference between the finite length of the complete structure and the infinite length of the eigenmode-based results. Note that when the source frequency is swept from 9.75 to 12.0 GHz, the main beam of the finite structure is continuously scanned from  $-56^\circ$  to  $+54^\circ$ , through  $110^\circ$ .

The simulated directivity and AR values of the six-cell system are presented in Fig. 7. The directivity values vary between 6.8 and 11.5 dBic. The AR values are greater than 3 dB across the operating band except for a very narrow frequency range around 11.1 GHz where the AR is  $\leq 3$  dB.

#### C. Circular Polarization Analysis

To analyze the CP performance of the six-cell system, one can introduce its equivalent electric and magnetic current sources. According to Huygens' principle [34], the antenna's far-field radiation can be determined from these equivalent sources. Fig. 8 shows the simulated electric and magnetic

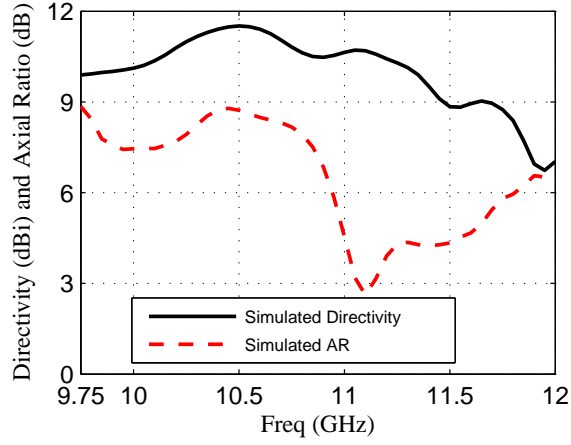


Fig. 7. Simulated directivity and axial ratio values of the six-cell I-shaped slot-loaded SIW LWA with PRW vias.

fields just above one Unit B in the system in Fig. 3 at  $t = 0$  and  $\pi/4$  for 10.5 GHz. It is seen that the magnetic fields are very small and negligible in comparison to the electric fields. Consequently, only these near-field electric fields are considered for the analysis of the far-field radiation performance. They are mainly distributed above the etched I-shaped slot and the PRW vias.

To emphasize this distribution more clearly, Fig. 9(a) shows the simulated E-field components  $\mathbf{E}_t$ ,  $\mathbf{E}_m$ ,  $\mathbf{E}_b$ , and  $\mathbf{E}_{prw}$  above one Unit B cell. As shown in Fig. 9 (b), the corresponding equivalent magnetic currents are calculated as:

$$\begin{aligned} \mathbf{M}_t &= \mathbf{E}_t \times \hat{\mathbf{n}}_z; & \mathbf{M}_m &= \mathbf{E}_m \times \hat{\mathbf{n}}_z; \\ \mathbf{M}_b &= \mathbf{E}_b \times \hat{\mathbf{n}}_z; & \mathbf{M}_{prw} &= -\mathbf{E}_{prw} \times \hat{\mathbf{n}}_y \end{aligned} \quad (10)$$

where  $\hat{\mathbf{n}}_y$ , and  $\hat{\mathbf{n}}_z$  are the unit vectors along the  $+y$  axis and  $+z$  axis, respectively. Note that the two horizontal magnetic currents  $\mathbf{M}_t$  and  $\mathbf{M}_b$  along the  $x$ -axis direction are introduced by the two horizontal parts of the etched I-shaped slot. Similarly, the horizontal magnetic current  $\mathbf{M}_{prw}$  along the  $x$ -axis direction is produced by the PRW vias. The vertical current  $\mathbf{M}_m$  along the  $y$ -axis direction is introduced by the vertical part of the etched I-shaped slot. Then, the total equivalent magnetic source  $\mathbf{M}_{tot}$  is:

$$\mathbf{M}_{tot} = \mathbf{M}_x + \mathbf{M}_y \quad (11)$$

where

$$\mathbf{M}_x = \mathbf{M}_t + \mathbf{M}_b + \mathbf{M}_{prw}, \quad \text{and} \quad \mathbf{M}_y = \mathbf{M}_m \quad (12)$$

It is obvious that to form a circularly polarized wave, the two magnetic current components, i.e.  $\mathbf{M}_x$  along the  $x$ -axis direction and  $\mathbf{M}_y$  along the  $y$ -axis direction, need to have the same amplitude and a  $90^\circ$  phase difference. It is found for this six-cell I-shaped slot-loaded system that  $\mathbf{M}_{prw}$  is approximately out of phase with  $\mathbf{M}_b$ , and  $\mathbf{M}_t$  is relatively small. As a consequence,  $\mathbf{M}_x$  is much smaller than  $\mathbf{M}_y$ . Therefore, the noted poor AR values are observed. To improve the AR performance, a different unit cell had to be developed.

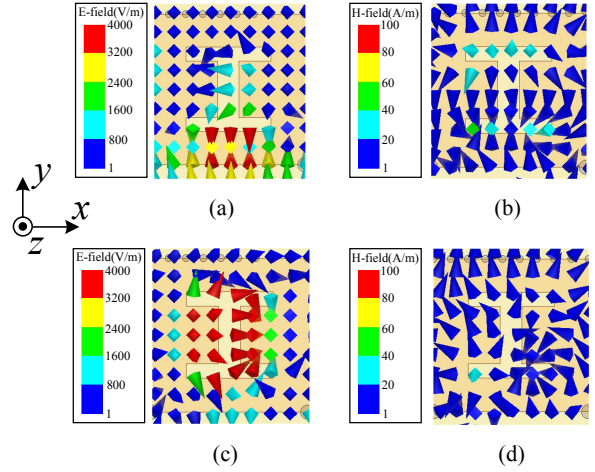


Fig. 8. Top view of the field distribution on the Unit B at 10.5 GHz. (a) E-fields distribution ( $t = 0$ ) (b) H-field distribution ( $t = 0$ ) (c) E-fields distribution ( $t = \pi/4$ ) (d) H-fields distribution ( $t = \pi/4$ ).

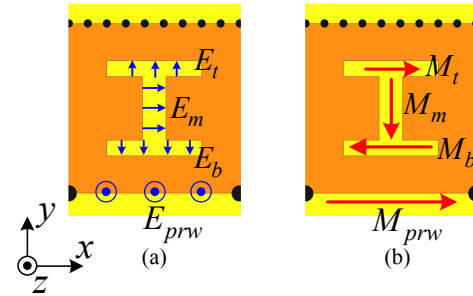


Fig. 9. Unit B radiation mechanism analysis. (a) E-fields distribution. (b) Equivalent magnetic current sources.

#### IV. BENZENE-RING-SHAPED SLOT-LOADED SIW CP LWA WITH PRW VIAS

The benzene-ring-shaped slot-loaded SIW CP LWA with PRW ViAs is introduced to achieve much improved AR values. Its continuous beam scanning and CP performance is demonstrated. Details of the antenna configuration are given. The resulting continuous beam scanning and CP features are analyzed and simulated.

##### A. Antenna Configuration

Guided by the field distribution analysis of the I-slots, it was found that one can manipulate the etched slots and optimize the PRW vias to improve the AR values. In particular, a new slot-loaded unit cell was developed. It is labelled as Unit C in the top right inset of Fig. 10(a). Its evolution from Unit B with the I-slot is depicted in the three subplots of Fig. 10(a). The top and bottom horizontal parts of the I-shaped slot were first rotated to an angle of  $\psi$  ( $\psi = 45^\circ$ ). This modification reduced the magnetic current contribution  $\mathbf{M}_b$  found in Fig. 9. These modified slots were then connected to the counterparts in the adjacent cells using additional horizontal slots on the upper side of the patch. These additional horizontal slots add another  $x$ -axis magnetic current component to balance  $\mathbf{M}_x$  and  $\mathbf{M}_y$ . The final shape is reminiscent of a benzene ring. Furthermore, by cascading these benzene-ring-shaped slot unit

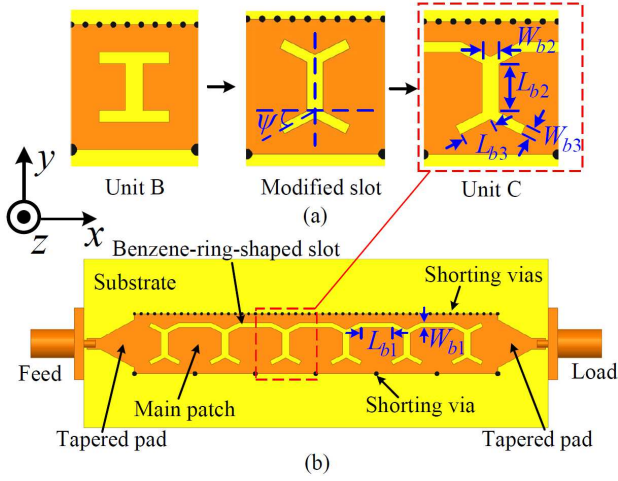


Fig. 10. Benzene-ring-shaped slot-loaded SIW CP LWA with PRW vias. (a) Evolution of Unit C from Unit B. (b) Complete six-cell based structure.

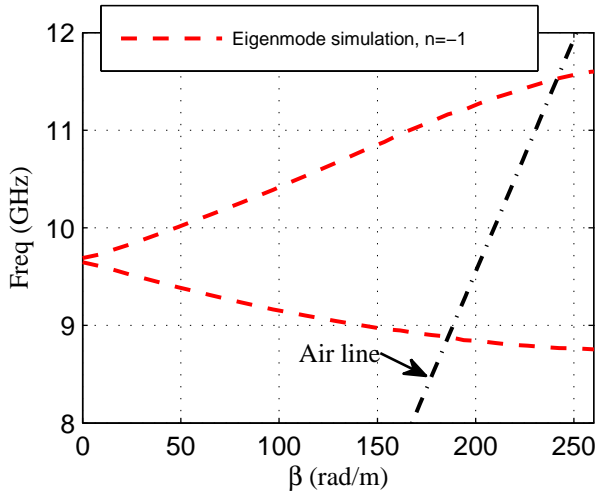


Fig. 11. Unit C dispersion diagrams obtained from its eigenmode simulation.

cells, it was found that their longer length slots enhance the guiding characteristics of the traveling wave in the SIW structure in comparison to their resonant I-shaped parent.

The dispersion diagram of the Unit C shown in Fig. 11 was obtained with an eigenmode simulation. It indicates that a continuous transition between the backward and forward curves is achieved. Six benzene-ring-shaped slot-loaded Unit C cells were then combined with the tapered feed and termination segments to form the SIW LWA with PRW vias shown in Fig. 10(b). The dimensions of the benzene-ring-shaped slots are represented by the parameters  $L_{b1}$ ,  $W_{b1}$ ,  $L_{b2}$ ,  $W_{b2}$ ,  $L_{b3}$ , and  $W_{b3}$  in Fig. 10.

### B. Design Parameter Study

With the knowledge that the CP performance of a slot-loaded SIW LWA with PRW vias is dependent on the precise shape of its etched slots and the PRW vias, the design parameters of the benzene-ring-shaped slot and PRW vias combination were carefully investigated and optimized. In particular, parameter studies of the slot widths  $W_{b1}$ ,  $W_{b2}$ , and

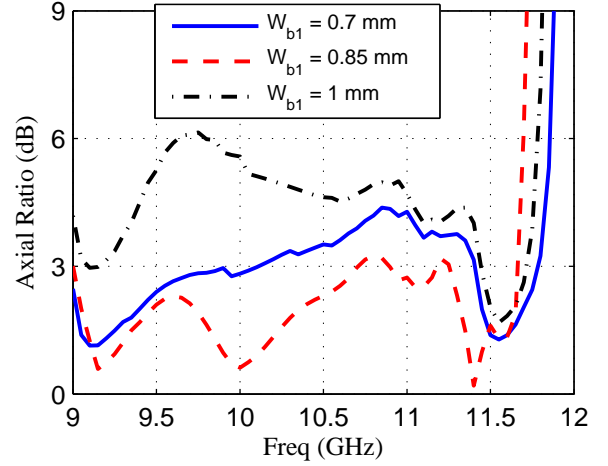


Fig. 12. The axial ratio (AR) values as a function of the source frequency for different values of  $W_{b1}$ .

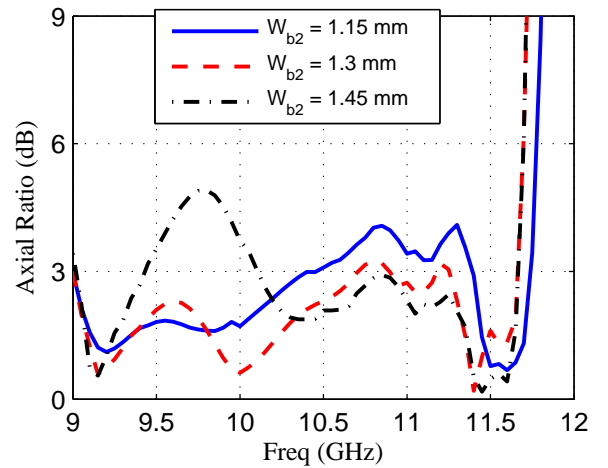


Fig. 13. The axial ratio (AR) values as a function of the source frequency for different values of  $W_{b2}$ .

the PRW via radius  $d_2$  were performed. When the value of the studied parameter was changed, the values for the other parameters were fixed.

Fig. 12 shows the AR values as a function of the source frequency for different values of  $W_{b1}$ . It is seen that when  $W_{b1} = 0.7$  mm, the AR values exceed 3 dB between 10.1 and 11.4 GHz. However, when the value of  $W_{b1}$  increases to 0.85 mm, good CP performance below 3.1 dB is obtained within the whole operating band from 9 to 11.5 GHz. With a further increase of  $W_{b1}$  to 1.0 mm, the overall CP performance again deteriorates, the AR values of AR being more than 3 dB. Consequently, it is seen that  $W_{b1}$  has a high impact on the antenna's CP performance.

Fig. 13 shows the AR values as a function of the source frequency for different values of  $W_{b2}$ . Good CP performance is obtained for  $W_{b2} = 1.3$  mm. In contrast, the AR values in the higher frequency band from 10.5 to 11.4 GHz becomes worse when the value of  $W_{b2}$  reduces to 1.15 mm. Similarly, the AR values in the lower frequency band from 9.45 to 10.1 GHz

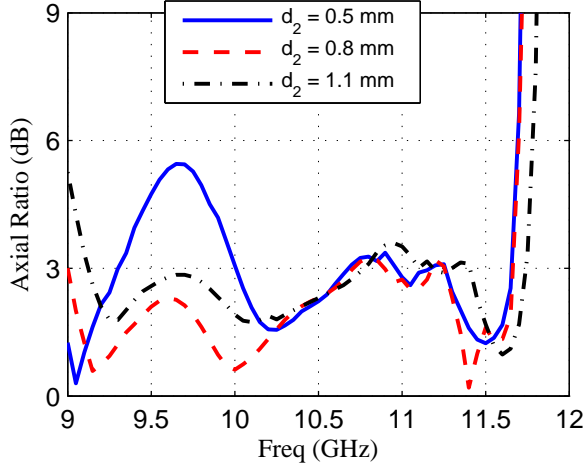


Fig. 14. The axial ratio (AR) as a function of the source frequency for different values of  $d_2$ .

TABLE II  
OPTIMIZED VALUES OF THE DESIGN PARAMETERS OF THE  
BENZENE-RING-SHAPED SLOT-LOADED SIW CP LWA WITH PRW VIAS

Parameter	$l_s$	$W_a$	$W_b$	$L_t$	$S$	$d_1$	$d_2$
Value (mm)	82.8	2	8.5	6	1.2	0.5	0.8
Parameter	$P$	$L_{b1}$	$W_{b1}$	$L_{b2}$	$W_{b2}$	$L_{b3}$	$W_{b3}$
Value (mm)	10.8	5.75	0.85	3.9	1.3	2.7	0.8

deteriorate when the value of  $W_{b2}$  increases to 1.45 mm. Thus,  $W_{b2} = 1.3$  mm was chosen to balance the CP performance in both the lower and higher frequency bands and yielded good CP performance over the entire operating band from 9 to 11.5 GHz.

Finally, Fig. 14 shows the AR values as a function of the source frequency for different values of  $d_2$ . It is seen that when  $d_2 = 0.5$  mm, the AR values remain below 3.2 dB except in the lower frequency band from 9.3 to 10 GHz. When  $d_2$  increases to 0.8 mm, the AR performance is improved and the AR values are all below 3.1 dB. When  $d_2$  further increases to 1.1 mm, the AR performance remains similar, but the operating band blue shifts to higher frequencies.

To observe the quadrature phase between the two main E-field components, two observation points were selected to extract each of their phase values. One was located at the center point of a slot and the other was located on the open edge at the center point of the two adjacent vias. The phase differences of the two E-field components at these points were found to be between  $78^\circ$  and  $108^\circ$  over the operating frequency band. Thus, they were close to the  $90^\circ$  value associated with the CP performance. The benzene-ring-shaped slot parameters  $W_{b1}$ ,  $W_{b2}$ , and  $d_2$  are the ones that mainly affected those phase differences.

The final optimized parameter values are listed in Table II.

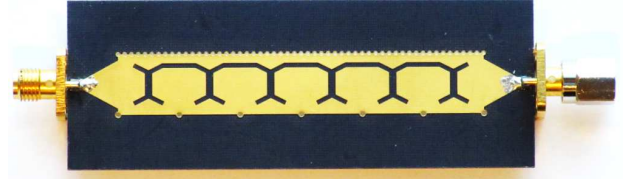


Fig. 15. Photograph of the fabricated benzene-ring-shaped slot-loaded CP SIW LWA with PRW vias prototype.

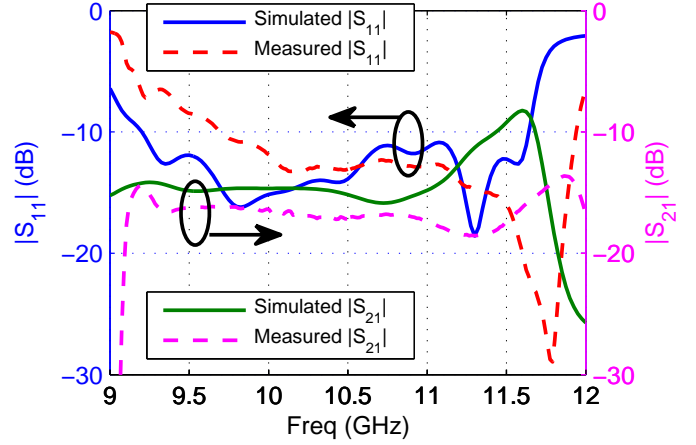


Fig. 16. Simulated and measured S-parameters of the benzene-ring-shaped slot-loaded CP SIW LWA with PRW vias.

### C. Simulated and Measured Results

Based on the optimum design parameter values, the benzene-ring-shaped slot-loaded CP SIW LWA with PRW vias was fabricated and measured. Fig. 15 shows a photograph of the fabricated prototype. The simulated and measured S-parameters are compared Fig. 16. It is seen that the simulated  $|S_{11}| \leq -10$  dB operating bandwidth is from 9.2 to 11.65 GHz. When the source frequency is reduces from 9.3 down to 9.0 GHz, the simulated  $|S_{11}|$  value remains below  $-6.4$  dB. The measured  $|S_{11}| \leq -10$  operating bandwidth is from 9.7 to 11.94 GHz. For frequencies between 9.35 and 9.7 GHz, the measured  $|S_{11}|$  is  $\leq -6.6$  dB. Noted that the measured  $|S_{11}|$  values show a blue shift to higher operating frequencies. Simulations indicate that this is caused by fabrication inaccuracies. The simulated  $|S_{21}|$  values are below  $-10$  dB for frequencies lower than 11.45 GHz. They peak at 11.6 GHz with the value of  $-8.23$  dB. The measured  $|S_{21}|$  values are always below  $-13.6$  dB. The simultaneously measured low  $|S_{11}|$  and  $|S_{21}|$  values indicate that the system has good radiation performance.

Fig. 17 displays the simulated radiation patterns at five different frequencies. It illustrates that the main beam can be continuously scanned from backward to forward directions through broadside. The main beam points in the backward direction at 9 GHz with the leftmost angle of  $-46^\circ$ . With the increase in the source frequency, the beam moves towards the broadside. For instance, the main beam angle is  $-26^\circ$  at 9.25 GHz. The main beam points in the broadside direction at 9.8 GHz. When the source frequency is further increased, the



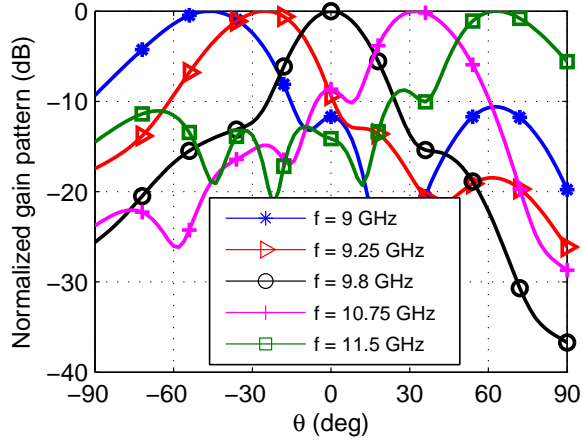


Fig. 17. Simulated radiation patterns of the optimized design at five different frequencies.

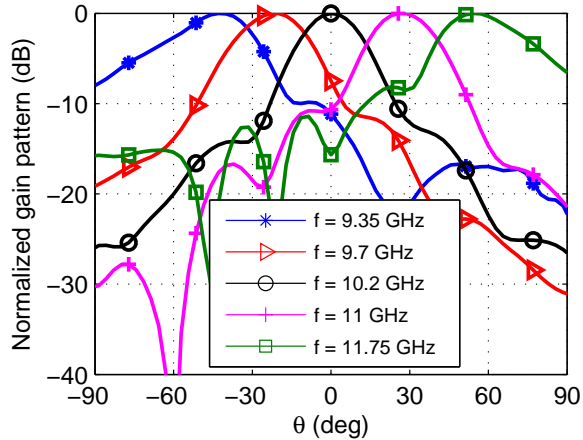


Fig. 18. Measured radiation patterns of the prototype at five different frequencies.

main beam moves into the forward directions, e.g., the main beam angle is  $+32^\circ$  at 10.75 GHz. The main beam points at the rightmost angle ( $+64^\circ$ ) at 11.5 GHz. Thus, the simulated beam scanning range is  $110^\circ$  as the source frequency is swept from 9 to 11.5 GHz. The simulated radiation efficiency of the antenna varies from 92.3% to 97.9% within the operating frequency band, 9.0 to 11.5 GHz.

The far-field radiation patterns of the prototype were measured using the Satimo multi-probe spherical near-field system StarLab-18 located at Xiamen University, China. The measured radiation patterns at five different frequencies are shown in Fig. 18. When the operating frequency is 9.35, 9.7, 10.2, 11, 11.75 GHz, the main beam angle is  $-42.8^\circ$ ,  $-22.8^\circ$ ,  $0^\circ$ ,  $+25.7^\circ$ , and  $+54.3^\circ$ , respectively. The measured beam scanning range is  $97.1^\circ$  as the source frequency varies from 9.35 to 11.75 GHz. The corresponding simulated (measured) cross-pol levels in the main beam directions at all of these frequencies are all smaller than  $-15.1$  ( $-12.7$ ) dB.

Fig. 19 compares the simulated and measured AR values along with the realized gain values as functions of the source frequency. As noted previously, the simulated AR values are

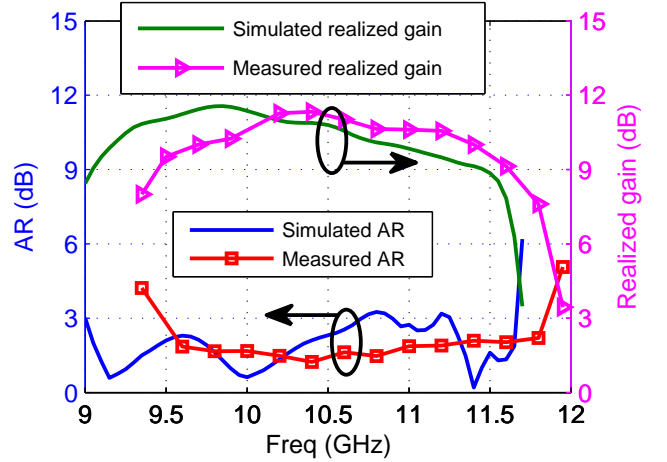


Fig. 19. Simulated and measured axial ratio (AR) values together with the corresponding realized gain values as functions of the source frequency.

below 3.1 dB within the operational frequency range from 9 to 11.5 GHz. The corresponding realized gain values vary between 8.44 and 11.56 dBic. Due to the shift of the measured results to higher frequencies, the AR values below 3 dB occur in the band from 9.45 to 11.75 GHz. The AR value below this band at 9.35 GHz, for example, is 4.1 dB. From 9.35 to 11.75 GHz, the measured realized gain is stable with only a 3.3 dB gain variation between 8 and 11.3 dBic.

## V. DISCUSSION

Considering its potential applications, the current study was focused on achieving a LWA system that realizes wide-angle CP beam scanning with a consistent gain. While there are examples of systems that can scan a CP beam over a large angular range, it generally remains a very challenging problem. Our goal was achieved by introducing a novel unit cell with a benzene-ring-shaped slot and using it to construct a six-cell SIW LWA with PRW vias. Continuous beam scanning in a wide angular range with consistent gain was realized with an optimized design. A complete comparison between this optimized design and previously reported CP LWAs is given in Table III. It is seen that when it is compared to these reference LWAs, the antenna system developed in this paper exhibits superior performance in terms of its beam scanning range and its realized gain consistency.

## VI. CONCLUSION

A benzene-ring-shaped slot-loaded CP SIW LWA with PRW vias was presented. It was demonstrated that it realizes continuous beam scanning from its backward to forward directions through a wide angular range with consistent realized gain. It was shown that an I-shaped slot-loaded LWA with PRW vias supports continuous beam scanning, but the AR values in the main beam directions are very high. To achieve the CP beam scanning in a wide angle range with consistent gain, a novel benzene-ring-shaped slot-loaded SIW LWA with PRW vias was developed and optimized. A prototype system was fabricated and tested. The measured results demonstrate

TABLE III  
COMPARISON BETWEEN THE ANTENNA DEVELOPED IN THIS PAPER AND THE REPORTED CP LWAS

Antenna Ref.	Antenna type	Operating band	Antenna length	AR $\leq$ 3 dB band	Beam scanning range	Gain range
[19]	Inspired-CRLH SIW (Single-layer)	4.2–4.85 GHz	$2.43\lambda_0$	4.2–4.85 GHz	$-25^\circ$ to $+26^\circ$	–1 to 1.5 dBic
[20]	CRLH microstrip (Single-layer)	23–25 GHz	$22.0\lambda_0$	Not given	$-6^\circ$ to $+6^\circ$	15 to 16 dBic
[21]	CRLH HMSIW (Single-layer)	7.4–13.5 GHz	$6.09\lambda_0$	Not given	$-70^\circ$ to $+70^\circ$	7.48 to 12.01 dBic
[22]	CRLH SIW (Single-layer)	7.35–10.15 GHz	$4.56\lambda_0$	7.5–9.25 GHz	$-19^\circ$ to $+84^\circ$	0 to 8.95 dBic
[23]	SSPP TL (Double-layer)	11–15 GHz	$5.72\lambda_0$	Not given	$-32^\circ$ to $+34^\circ$	12.8 to 14.2 dBic
[28]	Slot-loaded SIW (Single-layer)	10–14 GHz	$6.4\lambda_0$	10–13.8 GHz	$-40^\circ$ to $+25^\circ$	4.2 to 11 dBic
This work	Slot-loaded SIW with PRW (Single-layer)	9.35–11.75 GHz	$2.91\lambda_0$	9.45–11.75 GHz	$-42.8^\circ$ to $+54.3^\circ$	8 to 11.3 dBic

that the beam radiated by this system can be scanned from  $-42.8^\circ$  to  $+54.3^\circ$ , i.e., continuous beam scanning through  $97.1^\circ$ ) was realized, and it has a commensurate gain variation of 3.3 dBic between 8 and 11.3 dBic. The reported CP LWA is a highly promising candidate for future wireless communications systems for which there exists a prominent demand for high performance antennas that are low cost and exhibit multiple functionality.

#### ACKNOWLEDGMENT

The authors would like to thank Mr. Ming Li from Xiamen University in China for his assistance in the measurement campaign.

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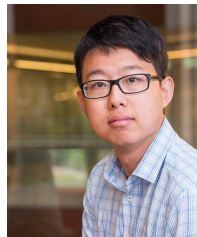
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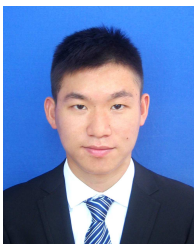
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