

Tremor Suppression in the Human Hand and Forearm

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In the name of GOD

The Most Compassionate

The Most Merciful

DEDICATED TO

My husband and my parents

CERTIFICATE OF ORIGINAL AUTHORSHIP

I, Seyedeh Marzieh Hosseini, certify that the work in this thesis has not previously been submitted for a degree nor has it been submitted as part of requirements for a degree except as fully acknowledged within the text.

I also certify that the thesis has been written by me. Any help that I have received in my research work and the preparation of the thesis itself has been acknowledged. In addition, I certify that all information sources and literature used are indicated in the thesis.

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ABSTRACT

Tremor is a neurological disorder characterized by involuntary oscillations and poses a functional problem to a large number of patients. The most preferred description for tremor is an involuntary movement that is an approximately rhythmic and roughly sinusoidal movement. It results from a neurological disorder which can affect many daily activities. People who are affected by Parkinson's diseases (PD) have tremor on their upper limb especially in the forearm and hand. Difficulties associated with tremor in patients with PD have motivated the researchers to work on developing various methods for tremor suppression. There is some medical and non-medical treatment for tremor reduction. Despite the considerable experience in tremor management, current treatment based on drugs or surgery does not achieve an effective reduction in 25 % of patients.

For such case, many researchers concentrated on finding non-medical treatments for tremor diminution. Active force control (AFC) or active vibration control (AVC) is one of the most famous non-medical methods for tremor suppression and control. Active vibration control is an alternate way to control and attenuate the vibration. In this method a counter force which is equal to the original vibration force but in the opposite direction is applied to the vibrating structure to supress the vibration. Finally, the vibration of structures will be stopped as two opposite forces cancel each other. The AFC method for tremor attenuation in the human forearm and hand is considered in this thesis. An AFC system is proposed which has a piezoelectric actuator and a classic proportional-derivative (PD) controller. Tremor behavior is investigated in three different models. The first model is a four degreesof-freedom (4-DOF) biodynamic model of the human hand, which is the combination of mass-spring-damper system. The second model is a one degree-of-freedom (1-DOF) musculoskeletal model of the elbow joint with two links and one joint which includes two muscles, biceps, and triceps as the flexor and the extensor of the elbow joint. The third model is a three degrees-of-freedom (3-DOF) musculoskeletal model including wrist flexion-extension (FE), radial-ulnar deviation (RUD), and pronation supination (PS). The musculoskeletal model contains four muscles; extensor carpi radialis longus, extensor carpi

ulnaris, flexor carpi ulnaris and flexor carpi radialis. First, simulation of the tremor generation in the model is performed and then the performance of the AFC system for suppressing tremor is investigated in all three models. A single piezoelectric actuator is embedded in the AFC system for controlling the behavior of the PD controller. MATLAB Simulink is used to analyze the model. Results show that the proposed AFC-based system with a piezoelectric actuator and a PD controller is very effective in suppressing the tremor for the three models.

Using piezoelectric material as a smart material for AVC has been of interest to many researchers. Human forearm is modelled as a continuous beam which has a layer of piezoelectric actuator on its top surface and tremor is controlled actively. Also using piezoelectric material as an actuator and sensor in the closed loop control system has a very significant effect on tremor suppression. A closed loop active control system is developed and the human forearm is modeled as a beam which has two layers of piezoelectric on its top and bottom surface as an actuator and sensor respectively. Tremor behaviour of the model is studied in this control system to identify the effect of piezoelectric material on tremor suppression. Hamilton principle is used to obtain the equation of motion of both beam model. Thus, by employing the Galerkin procedure, the governing equation of motion which is a second order ordinary differential equation in time is derived. An external force as a tremor disturbance is applied to the beam by a sinusoidal force to analyse the beam behaviour. The response of the system to the force stimulation gives the analytical relations for natural frequency and amplitude of the vibration. Using the obtained analytical relations, the effects of different factors and piezoelectric properties on the vibration of this beam are examined. The results indicate that the piezoelectric layer as an actuator provides an effective tool for active control of vibration. Also using a piezoelectric layer as a sensor and actuator on the closed loop control system has a significant effect on tremor suppression.

Tremor characteristics help researchers to find the best treatment for its suppression. The frequency and amplitude of tremor have different level in patients. Some patients

experience a severe kind of tremor compared to others who have weak tremor. As a result, tremor classification for PD subjects provides beneficial information for the researchers.

Human hand tremor is recorded using electromyography (EMG) from 14 patients who are affected by Parkinson's disease. Different signal-processing including filtering and data segmentation, feature extraction, feature reduction and classification are applied to the raw EMG signal to get accurate and useful information from recorded signals. Extreme learning machine (ELM) was used to classify data into three different classifications; severe, moderate and weak. The results illustrate that the proposed system which consists of the PCA, ELM and the majority vote is successful to recognising the tremor severity in three different classes; weak, moderate and severe.

Abbreviations

AFC Active Force Control

ANN Artificial Neural Network

AR Autoregressive

AVC Active Vibration Control

BaSTO Barium Strontium Titanate

CR Crossing Rate

DBS Deep Brain Stimulation

DOF Degree of Freedom

ECG Electrocardiography

ECRL Extensor Carpi Radialis Longus

ECU Extensor carpi ulnaris

EEG Electroencephalography

ELM Extreme Learning Machine

EMG Electromyography

EMG-PR EMG-based Pattern Recognition

EMG-non-PR EMG-based non-Pattern Recognition

EOG Electrooculography
ET Essential Tremor

EWT Empirical Wavelet Transform

EWPT Empirical Wavelet Packet Transform

FCR Flexor Carpi Radialis
FCU Flexor Carpi Ulnaris
FD Frequency Domain

FE Flexion-Extension

FES Functional Electrical Stimulation

FGM Functionally Graded Material

FNN Feed-Forward Neural Networks

FP Feature Projection
FS Feature Selection

HAL Hybrid Assistive Limb

HMM Hidden Markov Model

HTD Hjorth Time Domain

I controller Integral controller

IEMG Integrated EMG

IMU Inertial Measurement Unit

KKT Karush-Khun-Tucker
KNN K-Nearest Neighbour

LDA Linear Discriminant Analysis

LFP Local Field Potentials
LH (Biceps) Long Head

LtH (Triceps) Lateral Head
MAV Mean Absolute Value

MDF Median Frequency
MES Myoelectric Signal

MLP Multiple Layer Perceptron

MNF Mean Frequency

MNP Mean Power
MU Motor Unit

OFNDA Orthogonal Fuzzy Neighbourhood Discriminant Analysis

P controller Proportional controller

PCA Principle Component Analysis

PD Parkinson's Disease

PD controller Proportional–Derivative controller

PI controller Proportional –Integral controller

PID controller Proportional–Integral–Derivative controller

PKF Peak Frequency

PLZT Lead Lanthanum Zirconate Titanate

PNN Probabilistic Neural Network

PS Pronation-Supination
PSD Power Spectral Density

PT Physical Therapy

PVDF Polyvinylidene Fluoride

PW Pulse Width

PZT Lead Zirconate Titanate

RBN Radial Basis Function Network

RUD Radial-Ulnar Deviation

SCI Spinal Cord Injury

sEMG Surface Electromyography

SLFNs Single-Hidden-Layer Feed-Forward Networks

SOM Self-Organizing Map

SRDA Spectral Regression Discriminant Analysis

SSC Slope Sign Changes

SVD Singular Value Decomposition

SVM Support Vector Machine

TD Time Domain

TFD Time-Frequency Domain

TMS Transcranial Magnetic Stimulation

WBV Whole Body Vibration

WL Waveform Length

WOTAS Wearable Orthosis for Tremor Assessment and Suppression

ZC Zero Crossings

2D Two-Dimensional

Nomenclature

A Area of cross-section

 A_s Area of the piezoelectric sensor

A(s) Transfer function of the actuator

a Muscle activation without fatigue

a_r Normalized muscle recruitment curve

 a_m Muscle activation with fatigue

a_p Feature vector

b Dimensionless frequency of the beam

bi Threshold for the ith hidden neuron

c User-specified parameter

 c_i Damping coefficients

D Displacement vector

D_T Delay time for electromyography control system

 d_{31} Piezoelectric constant that relates the mechanical tension to

electrical displacement

E Modulus of elasticity of the beam /Elasticity coefficient

matrix

ei Eigenvectors

e(t) Error in PD controller

*e*₃₁ Piezoelectric constant

 F_a Actuator force

 F_{Di} Dissipative force

 F_e Disturbance force

 F_e' Estimated disturbance force

 F_i Muscle force

 F_{ki} Restoring force

Muscle maximum isometric force

 F_{Oi} Excitation force

f Stimulation frequency

fi Normalized factor

 f_n Frequency of EMG signal

*f*_v Force -Velocity Factor

f(x,t) External force on the beam

G Shear modulus

Ga Feedback control gain

Gs Amplifier gain

G_T Control gain

g Gravitational constant

g(x) Activation function of the hidden node

H Hidden layer output matrix

 H^* Moore–Penrose generalized inverse of the matrix **G**

H(x) Heaviside function

h Coupling coefficients matrix

h_a Piezoelectric actuator thickness

*h*_b Beam thickness

 h_p Piezoelectric thickness

hs Piezoelectric sensor thickness

I Second moment of inertia

I' Vibratory inertia

J(x) Polar moment of inertia

K Shear correction factor

 K_d Derivative gain

 K_i Integral gain

 K_p Proportional gain

 k_i Linear stiffness

 k_s Spring stiffness

l Length

la Piezoelectric actuator length

*l*_b Beam length

ls Piezoelectric sensor length

l Normalized muscle length

M Bending moment

M' Estimated Mass

 m_a Mass of the piezoelectric actuator

 m_b Mass of the Euler- Bernoulli beam model

 m_i Mass in 4-DOF palm model

 m_s Mass of the piezoelectric sensor

m(x) Mass of the Timoshenko beam model

Nj Number of samples in class *j*

P Order of the AR model

P₁ Linear transformation for features

P_n Frequency power spectrum

 PW_d Threshold pulse width

PWs Saturation pulse width

p Muscle fatigue factor

p_{min} Minimum fitness

p(t) Applied voltage to the piezoelectric actuator

Q Electrical field vector

Qc Covariance matrix

 Q_n Non-linear piecewise continuous function

Q(t) Closed circuit charge

q Actual position in AFC system

 \ddot{q} Measured acceleration of the AFC system

q(f) Frequency characteristic factor

q(t) Time-dependent function

 r_i Moment arm

 S_{11} Elastic constant of piezoelectric material

T Kinetic energy

Transfer function of piezoelectric actuator

T_g Gravitational Moment

T_{inc} Increment of the window

T_P Internal passive moment

T_t Muscle generated Moment through active electrical

stimulation

Twl Length of the window

t Time

ti white noise error term

U Potential energy

 U_a Potential energy piezoelectric actuator

*U*_b Potential energy of the beam

 U_s Potential energy of the piezoelectric sensor

 U_{spring} Potential energy of the spring

V Shear force

V_a Applied external voltage to piezoelectric actuator

 V_s Applied external voltage to piezoelectric sensor

 v_a Volume of the piezoelectric actuator

 v_b Volume of the beam

 v_{max} Maximum contraction (shortening) velocity

 v_s Volume of the piezoelectric sensor

 \overline{v} Normalized muscle velocity

W Work

w_b Beam width

 w_a Piezoelectric actuator width w_s Piezoelectric sensor width

 $w_i = [w_{i1}, w_{i2}, ..., w_{im}]^T$ Vector of the weight for the ith hidden and input neurons

w_n Weighted window function

w_p Piezoelectric width

 $X = (x_1, ..., x_N)$ Feature set matrix with *t*-dimensional space

 χ_i^j The *i*th sample of class *j*

 $x_i = [x_{i1}, x_{i2}, ..., x_{im}]^T$ Input for SLFN

Y Vertical deflection in Euler-Bernoulli beam

Y(x) Fundamental vibration mode shape for Euler-Bernouli beam

y Lateral displacement in Euler-Bernoulli beam

 $y_i = [y_{i1}, y_{i2}, ..., y_{in}]^T$ Target for SLFN

z Electrical Pulse width

Z(x) Fundamental vibration mode shape in Timoshenko beam

 $\beta_i = [\beta_1, ..., \beta_n]$ Output weight linking the hidden layer and the jth output

node

 $\beta_{jL} = [\beta_{j1}, \beta_{j2}, ..., \beta_{jL}]^T$ Weight vector of jth hidden and output neuron

 β_s Shaping factor

$oldsymbol{eta}_{33}$	Impermittivity coefficients
$\gamma_{\scriptscriptstyle xy}$	Shear strain for Timoshenko beam
\mathcal{E}	Strain vector
$\zeta_{i}^{T} = [\zeta_{i,1}, \zeta_{i,2},, \zeta_{i,n}]^{T}$	Output vector error
heta	Joint angle
$\ddot{ heta}$	Angular acceleration
λ	Frequency factor on fatigue
λ_{i}	Eigenvalue associated with the eigenvector ei
μ_{j}	Mean of the class j
ξ ₃₃	Dielectric constant
ρ	Density
$ ho_a$	Density of piezoelectric actuator
$ ho_b$	Density of beam
$ ho_s$	Density of piezoelectric sensor
σ	Stress vector
τ	Processing time of pattern-recognition system
$ au_{ac}$	Activation time constant
$ au_{da}$	De-activation time constant
$ au_{\mathit{fat}}$	Fatigue time constant
$ au_{rec}$	Recovery time constant
$ au_{xy}$	Shear stress for Timoshenko
$ au_d'$	Estimated disturbance torque
Ø	Angle of rotation of the cross section due to bending
$\varphi(x)$	Fundamental vibration mode shapes

ψ	Bending slope of the beam
ω	Natural frequency
\in_z	Electric intensity in the z-direction
χ	Lateral displacement in Timoshenko beam

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