# Impact of evacuation design parameter on users' evacuation time using a multi-agent simulation

#### 3 Abstract

Emergency management is a fundamental issue in building management. Therefore, this study 4 5 was established to simulate the required times and movement conditions for user evacuation from Campus Infrastructure Building in a 3D environment. Eight simulations are carried out 6 by a multi-agent evacuation simulator, Pathfinder, considering 100% and 70% users capacity 7 with a combination of random, divide, zone 1 and zone 2 access selection. The users evacuated 8 were handled by the A\* algorithm in the steering mode of 3D evacuation simulation. The 9 evacuation flow was investigated with the user density heat map and Fruin's Level of Service 10 (LOS). This study found the best path planning obtained from the divide access factor and the 11 12 impact of the user's capacity is relying on total evacuation time. The critical space is caused by the access width fewer than 1.5 meters for every floor, and by widening some spaces helped to 13 improve the evacuation flow. 14

Keywords: Emergency management, evacuation planning, multi-agent simulation, 3D
 simulation, evacuation flow

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#### 18 1.0 Introduction

19 In tandem with the increase of elevated building development, the user evacuation activities have become a significant study, specifically for emergency management planners and 20 policymakers [1][2][3]. It is not easy to evacuate a mass volume of users in an efficient and 21 effective manner in an indoor environment due to complex individual behavior [4][5]-. The 22 evacuation activities in an indoor environment are difficult to forecast due to the different types 23 24 and locations of accidents that are too common [6][7][8]. In most cases, users need to be transferred as quickly as possible in difficult situations such as increasing user density at a time 25 and unclear knowledge of access selection [9][10]. The probability for the user to be stuck in 26 dangerous situations such as falling or being trapped in the building is high. In addition, the 27 distance to a safe place also cannot be estimated by the user because of planning limitations to 28 29 transfer the user [11][12]. When the priority of transferring users during emergencies is 30 essential, the knowledge of the best method to manage the movement of the user evacuation is necessary so that the activities can be carried out systematically and efficiently [13][14]. In 31 32 some instances, evacuation planning structure has to be identified to secure the safe environment of the building. This is because the nearest distance does not guarantee user 33 security due to the uncertainty of accident location within the building [15][16]. Therefore, it 34 is important to provide a user-friendly and highly efficient user transfer plan for user safety in 35 the indoor building environment such as the ability to accommodate large amounts of users at 36 one time [17][18]. 37

Currently, the evacuation path for an indoor environment is entirely dependent on the corridor and stairs of a building [19]. Corridors and stairs width are developed without taking into account the ability to accommodate large amounts of users at one time. For instance, there are several solutions for evacuation purposes such as Platform Rescue Systems (PRS), Controlled **Commented [BP1]:** The word "user" has been used four times in this sentence. Please revise it.

Descent Devices (CDD) and Escape Chutes [20][21]. The viewpoint of the alternative 42 evacuation method is based on the concept of an evacuation system that applies to oil and gas 43 industries. The system structure utilized for the PRS can be practical as the use of a safety 44 lifeboat for the ship during an evacuation crisis. As it is on the ship, the lifeboat is held tight 45 on the side of the boat and utilized just during the evacuation crisis. The details of the PRS 46 were discussed by Mansor et al. [22] and the first PRS model was introduced to a 21-story 47 48 building in Ramat Gan (Israel) in July 2004 [20][21]. The brake chute is barrel-shaped and made of heatproof texture or mesh. Each chute arrangement has its function to control the drop 49 speed of the evacuee [22]. In South Korea, the CDD is equipped in the hotel rooms. It contains 50 a set of tools with an abseil belt and plunge line associated with the window frame, and a 51 hammer to break glass in case of emergency. The application of CDD is wide around the globe, 52 mostly in Japan, Korea, Taiwan, Thailand, China, France, Spain, Germany, Italy, Sweden, 53 Finland, Mexico, Australia and Canada [20][22]. Furthermore, it was additionally announced 54 that the brake chute and CDD are mandated to be introduced in structures, for example in 55 control towers, hotels, and etc. in Japan and France [22]. Unfortunately, the PRS, CDD and 56 escape chutes are only suitable for high-rise buildings with a minimum of five floors. 57

58 There are some studies conducted to improve the user movement flow from the indoor 59 environment perspective. For example, Minegishi and Takeichi [23] focused on the evacuation 60 from the spectator stands, merging and on-ground situations where the exit access width and the on-ground situation being simulated for design method and crowd management policy. As 61 can be seen in the aforementioned literature, Tthe evacuation flow needs to be planned by 62 phases according to stands in order to avoid the accumulation of evacuees and the accumulation 63 of sequencing due to the limited exit access width and on-ground space due to large-scale 64 65 evacuees. Gwynne and Rosenbaum [24] have given recommendations for the interpretation and methods to calculate the effective width reduction under numerous circumstances based 66 3

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on the observation of user distribution. They discovered that the actual effective width of the
user evacuation path is generally more comprehensive than applied in design practices.
Lundstrom et al. [25] discussed the relationship between access width and user behavior during
the process of evacuation using the tunnel route model [7]. They found that the path with 1meter width led to higher motion speeds, and there was a linear relationship between dynamic
flows of users with access width.

Furthermore, the user's access width is recognized as a mandatory aspect of the evacuation regulation in many countries. Ji et al. [26] recommended that the exit access width should be the same as the access path width so that the user's evacuation flow can run smoothly [27][28]. They found out that at the point when the exit width is nearly the equivalent or more extensive than the width access path, the biggest limit of evacuation can be reached.

78 Generally, the path selection relies on the distance to the exit access and user capacity as both plays essential roles in reflecting the time taken to evacuate users [29][30]. Therefore, the 79 80 objective of this study is to identify the combined effect of the access selection and the user 81 capacity on evacuation time and examine the movement conditions aimed at recommending for evacuation planning improvements. The Campus Infrastructure Building (CIB) model that 82 located at Selangor, Malaysia was chosen to validate the proposed method, and the details of 83 84 the CIB are shown in Table 1. CIB was chosen for validation purposes because it is directly 85 involved with office management work as well as a storage place for electronic properties that 86 are vulnerable to fire. Review of legislation under Section 181, Street, Drainage and Building 87 Act 1974 (Act 133) (Amendment) 2012, Sel. P.U. (A) 142/2012 found that the access width within CIB was compliant for safety purposes with the minimum width of 552mm or 0.552m 88 width [31]. During the simulation process, the variables' values were adjusted to find out the 89 90 consequence on the evacuation process. The evacuation flow was investigated with the user

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- 91 heat map and Fruin's Level of Service (LOS) [26] both were used as an indicator to identify
- 92 the critical space to improve the evacuation flow.

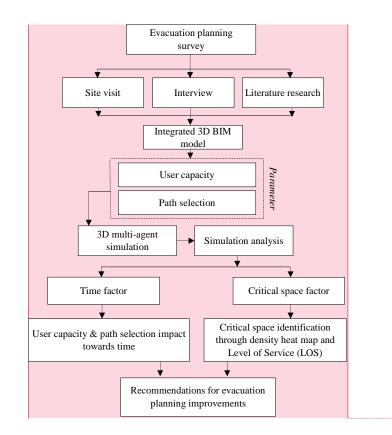
#### Table 1. Campus infrastructure building information

| Content  |
|--|
| Elevated building  |
| Three-level  |
| 2,112.115 meter square (m <sup>2</sup> )                     |
| Adjoining with office compartment                            |
| Open access  |
| Divided by door  |
| Two accesses in 1st floor                                    |
| One access in 2 <sup>nd</sup> floor                          |
| One stair connects 1st, 2nd and 3rd floor                    |
| One stair connects 2 <sup>nd</sup> and 3 <sup>rd</sup> floor |
|  |

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## 95 2.0 Methodology

The methodology of this study contains two parts, evacuation planning survey and evacuation
simulation process. The existing evacuation planning was surveyed based on the evacuation
guide used in CIB<sub>a</sub> while the user evacuation process was replicated by Pathfinder as a multiagent evacuating simulator. The framework for this study shown in Figure 1.



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#### 100

Figure 1. Framework of the impact of evacuation planning on user evacuation time using a
multi-agent simulation.

## 103 2.1 Evacuation planning survey

An evacuation planning survey was conducted to gain some basic information in order to support the building evacuation simulation model such as existing evacuation planning, user capacity conditions and the path structure design. These parts were separated into two main activities. First, interviews were conducted with the officer and operators of CIB. The information on path distribution within CIB, the usage of each compartment and the capacity of users that <u>areis</u> based on each worker's roles were deliberated and collected. Secondly, the existing evacuation path is surveyed on site to find the path connections from each
compartment to the exit access to gain an overview of the path space optimization and user
evacuation process. An example of the compartment arrangement within CIB is shown in
Figure 2.



#### 114

115 Figure 2. Compartment and corridor arrangement in 3<sup>rd</sup> floor of CIB

The distribution of user position within CIB is well distributed around each floor while the exit access is located at the edge of each floor. Therefore, the evacuation starts from all around the floor and the evacuation flow is a unidirectional scenario. It is presumed that no specific staff is take in charge to coordinate the evacuation process.

#### 120 2.2 Evacuation simulation process

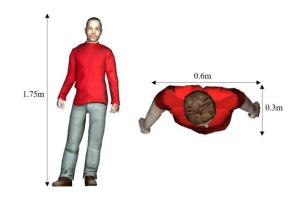
#### 121 2.2.1 Fundamental of model

Pathfinder is used for evacuation simulation to simulate user evacuation activities in an indoor
environment. It was used because of its capabilities in simulating the evacuation process more
efficiently without the need to set up a field experiment\_-with high-costs and risky conditions.
The steering mode which is a model based on Reynold's [32] steering behavior model and later

sophisticated by Heni et al. [33] was used in Pathfinder to handle the simulation of user
evacuation [34]. The user behavior was set up as an independent agent with dissimilar
characteristics such as age and pre-movement time [35]. The user speed calculation is set based
on Xiong et al. [36] equation as follows:

$$\mu i = \begin{cases} 1.4 & \rho \le 0.75 \\ 0.0412\rho^2 - 0.59\rho + 1.867 & 0.75 < \rho \le 4.2 \\ 0.1 & \rho > 4.2 \end{cases}$$
(1)

µi is user speed in m / s, and ρ is user density based on user / m<sup>2</sup> (Di). ρ can be calculated based
on the size and area of the site. The size taken is 0.6m x 0.30m based on the average individual
size and the site area is 0.38m x 0.38m as described by Xiong et al. [36] in Figure 3. As a result,
the most appropriate user speed is 1.19 m / s.

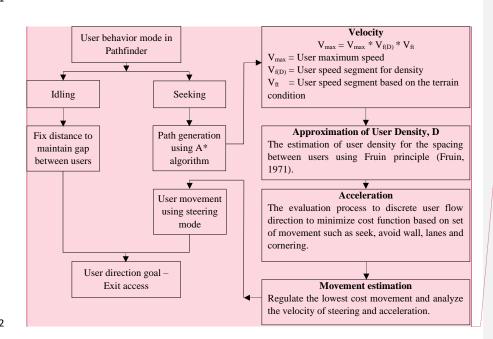


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Figure 3. Average individual size

Besides that, a combination of collision handling and steering mechanisms was applied in the steering mode in order to manage the users' flow towards their target exit access in an emergency situation. These mechanisms help to replicate the user movement to the safety exit by moving along the evacuation path and stray from any obstacle [37][38]. The principle of steering mode has been summarized in Figure 4.



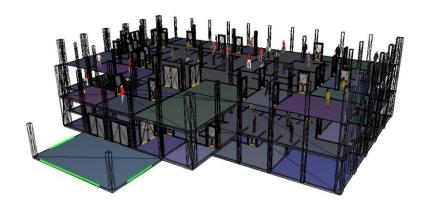
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Figure 4. User evacuation process through steering mode in Pathfinder.

The CIB environment is represented in a 3D geometry model where the 3D model was integrated from Building Information Modelling (BIM) model through the method suggested by Abdul Rahman and Abdul Maulud [39] to maintain the geometry structure and accuracy. In Pathfinder, the CIB demonstration in a 3D geometry mode where the navigation mesh is represented as a 2D triangulated surface within the 3D geometry model and shown in Figure 5.



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Figure 5. 3D geometry model of CIB.

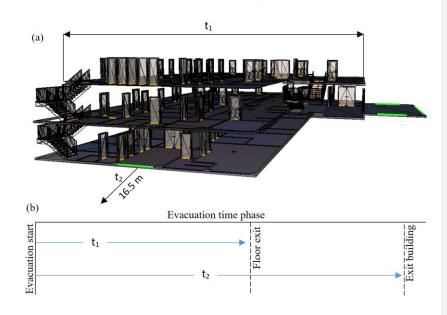
On top of that, the validation and verification of Pathfinder <u>have beenwere</u> conducted through several tests such as fundamental unidirectional flow, diagram tests and pedestrian behaviour tests at corridors and stairways by Thunderhead Engineering [40]. The result shows that Pathfinder can replicate an excellent representation of using actual movement with the real situation and it has been used widely in the research field for people evacuation simulation in recent years [41][42].

#### 158 2.2.2 Evacuation time measurement

Time taken to evacuate users is crucial in this study. It has become an indicator to identify if emergency management is good enough for implementation or not. There are two indicators measured based on the recorded time for user evacuation, which includes the impact of path selection over time and the effect of different user capacities over time. Therefore, the time taken is measured and evaluated through several measurements as follows:

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• t_1 = time taken for user to exit from the floor (risk zone).
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- $t_2$  = time taken for user to fully exit from building (16.5m from exit access as mentioned
- by Fire Prevention Standard for Building Design of China [7].



#### 167 The evacuation dimension and definitions are shown in Figure 6.

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#### 170 2.2.3 Evacuation simulation parameter

171 During the evacuation process, users have to transfer from the office compartment to the evacuation walkway quickly towards the exit access. In order to identify which aspect can 172 affect the evacuation time the most, two parameters tested in this study are the user capacity, 173  $d_1$  and path selection by the users,  $d_2$ . 174

Figure 6. (a) Evacuation time management measured, and (b) Evacuation time phase.

#### 175 User capacity parameter $(d_l)$

176 In terms of user capacity, the total number of users for the CIB is 155 users, with each level 177 having different capacities. Details of user capacity are as described in Table 2. Siikonen et al. 178 [43] in their his study used a percentage ratio of 50% of the total user capacity [44] for case 179 study in San Francisco but in this study, the testing for CIB was done in two stages. The first stage  $(d_{1a})$  involves 100% of total users while the second stage  $(d_{1b})$  goes for 70% of the total 180 11

users as high capacity is required as a precautionary measure and has a high impact on
emergency management as used by Pan et al. [7]. The breakdown of this percentage is to
determine the effect of the user's capacity on the simulation results.

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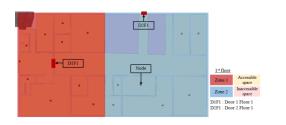
**Table 2.** User capacity consider<u>ation</u> for  $d_1$  parameter

| No.   | Floor                 | User capacity, $d_1$ (100%) | User capacity, $d_2$ (70%) |
|-------|-----------------------|-----------------------------|----------------------------|
| 1     | 1 <sup>st</sup> floor | 64                          | 45                         |
| 2     | 2 <sup>nd</sup> floor | 54                          | 38                         |
| 3     | 3 <sup>rd</sup> floor | 37                          | 26                         |
| Total |                       | 155                         | 109                        |

185

186 • Path selection  $(d_2)$ 

This aspect of path selection is used in assessing user behavior as described by Wang and Sun 187 [45] as the optimal segmentation path where testing is conducted in four stages. For the first 188 stage  $(d_{2a})$ , the exit access selection decision is set randomly while the second stage  $(d_{2b})$  of 189 exit access selection is divided by the user's proximity zone (zone 1 and zone 2) to exit access. 190 191 Each zone is evaluated by its proximity to the exit access based on the distance measured on 192 the field from one node to another. The distribution of nodes, zones and accesses are shown in 193 Figure 7. The third  $(d_{2c})$  and fourth  $(d_{2d})$  stage is performed using only one access per level for 194 each stage. The third stage will use D1F1, D1F2 and D1F3 while the fourth stage will use 195 D2F1, D2F2 and D2F3 as the exit accesses. This zone division is intended to test the result if 196 there is any restriction on either one of the accesses during emergencies.



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Figure 7. The exit access and zones fraction within each floor

By considering the parameters used in this study,  $d_1$  with two designed input ( $d_{1a}$  and  $d_{1b}$ ) and  $d_2$  with four designed input ( $d_{2a}$ ,  $d_{2b}$ ,  $d_{2c}$ , and  $d_{2d}$ ), a total of eight combinations of  $d_1$  and  $d_2$  were simulated. The parameters involved in the emergency evacuation model are listed in Table 3.

203

Table 3. Parameter in the simulation model

| Item                               | Content                  |                           |                           |                       |  |  |  |
|------------------------------------|--------------------------|---------------------------|---------------------------|-----------------------|--|--|--|
| User capacity $(d_l)$              | 100% (d <sub>1a</sub> )  | 1 <sup>st</sup> floor: 64 | 2 <sup>nd</sup> floor: 54 | 3rd floor: 37         |  |  |  |
|                                    | 70% ( <i>d</i> 1b)       | 1st floor: 45             | 2nd floor: 38             | 3rd floor: 26         |  |  |  |
| Access selection $(d_2)$           | Random access $(d_{2a})$ |                           |                           |                       |  |  |  |
|                                    | Divide access $(d_{2b})$ |                           |                           |                       |  |  |  |
|                                    | Zone 1 access $(d_{2c})$ |                           |                           |                       |  |  |  |
|                                    | Zone 2 access $(d_{2d})$ |                           |                           |                       |  |  |  |
| Parameter simulation $(d_1 + d_2)$ | $d_{1a} d_{2a} = S_1$    | $d_{1a} d_{2b} = S_2$     | $d_{1a} d_{2c} = S_3$     | $d_{1a} d_{2d} = S_4$ |  |  |  |
|                                    | $d_{1b} d_{2a} = S_5$    | $d_{1b} d_{2b} = S_6$     | $d_{1b} d_{2c} = S_7$     | $d_{1b} d_{2d} = S_8$ |  |  |  |

#### 204 2.2.4 Evacuation algorithm

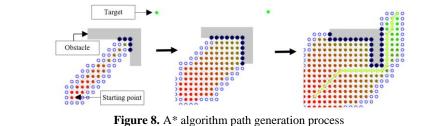
In performing 3D simulations, the A\* algorithm was used. The simulation aspect used is based 205 on the user's position to move from their starting location to the exit by choosing the path that 206 follows the arrangement route to their exit. This path selection process affects the overall 207 208 simulation results, as the time spent walking and waiting in the queue is taken into account in order to anticipate the path chosen to achieve the user's objectives. The A\* algorithm is used 209 to calculate the economical path so that users can select to get out of the model. An important 210 211 aspect of the A\* algorithm is F = G + H. F, G, and H are variables for each node point calculated 212 to obtain a new node. F is the total number of nodes, G is the distance between the current node 213 and the beginning node, while H is the approximate distance from the current node to the last node. Since F is the total number of nodes, the sum of F can be calculated based on Equation 214 215 2 as follows:

216 217 currentNode.f = currentNode.g + currentNode.h

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(2)

An example of the path generation process and pseudocodes of the A\* algorithm can be seen in Figure 8 and Figure 9. By using the A\* algorithm, the computation time to find the best path is shortened due to the fact that the best path is identified based on the nodes that provide the best chance of generating the most suitable path.



| // Initia | lize both open and closed list   |
|-----------|--|
| let the o | penList equal empty list of nodes  |
| let the c | losedList equal empty list of nodes  |
|           | he start node  |
| put the   | startNode on the openList (leave it's f at zero)   |
| // Loop   | until find the end   |
| while th  | e openList is not empty  |
| // Get tl | ne current node  |
| let the   | e currentNode equal the node with the least f value  |
|           | ve the currentNode from the openList   |
| add tl    | he currentNode to the closedList   |
|           | d the goal   |
| if cur    | rentNode is the goal   |
|           | rate children  |
| let the   | e children of the currentNode equal the adjacent nodes   |
| for ea    | ch child in the children   |
|           | // Child is on the closedList  |
|           | if child is in the closedList  |
|           | continue to beginning of for loop  |
|           | // Create the f, g, and h values   |
|           | child.g = currentNode.g + distance between child and currently currently between child and currently between chi |
|           | child.h = distance from child to end   |
|           | child.f = child.g + child.h  |
|           | // Child is already in openList  |
|           | if child.position is in the openList's nodes positions   |
|           | if the child.g is higher than the openList node's g  |
|           | continue to beginning of for loop  |
|           | // Add the child to the openList   |
|           | add the child to the openList  |

224 225

Figure 9. A\* algorithm pseudocodes

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226 3.0 Results
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227 Based on the results of the eight 3D simulations performed, the observation was carried out

228 based on two main factors, namely the time factor and critical space factor for user evacuation

229 activity.

#### 230 3.1 Time factor

Overall time comparisons become an indicator to ensure that the user's evacuation activity is smoothly conducted or otherwise. For this study, the period for the entire eight simulations was recorded and compared to identify the possible causes of time difference for the transfer process.

#### 235 3.1.1 The impact of user capacity towards time

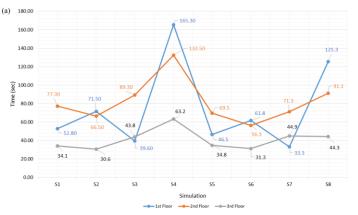
From the results, by considering the user capacity factor, it is found that the time difference 236 between  $S_1$  and  $S_5$  is a minimum of 7.80 seconds as shown in Table 4. This is in contrast to the 237 differences between the other simulations,  $S_2$  and  $S_6$ ,  $S_3$  and  $S_7$  and  $S_4$  and  $S_8$ , where the average 238 time difference is greater than 9.00 seconds. The results show that the higher the time spent on 239 240 evacuating the user, the higher the impact on the user's capacity during an emergency. In 241 addition, the aspect of access selection by the user is also influential because the random access option is free from the dependency on specific access selection. It allows users to decide to 242 243 evacuate through which access at a time, unlike other simulations, where the specific access is decided for the user. This is supported by findings from the time period of the last user through 244 specific access as shown in Figure 10(a). The duration of the last user through the D1F1 and 245 D1F2 exits for the  $S_2$  and  $S_6$  differs, even though both have the same specific exit access. The 246 247 reason is the uneven distribution of user positions that makes the movement of the user generally unmanageable. The distribution of users can be controlled through a restructuring of 248 249 office space to provide a specific path to exit access.

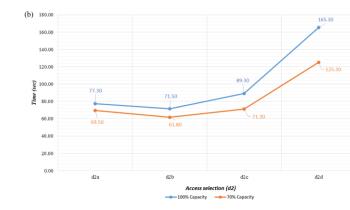
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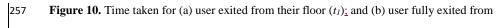
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# Table 4. Time difference due to differencet of user capacity

| Path selection (d <sub>2</sub> ) | User capa | city $(d_1)$ | Time orit | Different (acc) |                 |
|----------------------------------|-----------|--------------|-----------|-----------------|-----------------|
|                                  | 100%      | 70%          |           | ed, $t_2$ (sec) | Different (sec) |
| Random access                    | $S_I$     | $S_5$        | 77.30     | 69.50           | 7.80            |
| Divide access                    | $S_2$     | $S_6$        | 71.50     | 61.80           | 9.70            |
| Zone 1 access                    | $S_3$     | $S_7$        | 89.30     | 71.30           | 18.00           |
| Zone 2 access                    | $S_4$     | $S_8$        | 165.30    | 125.30          | 40.00           |







the building  $(t_2)$ 

#### 259 **3.1.2** The impact of path selection towards time

The overall time comparisons recorded for the eight simulations performed are shown in Figure 10(b). The results showed that  $S_2$  and  $S_6$  recorded the shortest amount of time to evacuate users as both simulations have similarities from the perspective of access selection, namely divide access.  $S_2$  recorded a time of 71.5 seconds and  $S_6$  61.8 seconds, which are shorter times than other simulations. The path selection of divide access not only provides the shortest time, but the density distribution of the path usage is also more appropriate, which causes the shortest amount of time recorded.

#### 267 **3.2** Critical space factor

Identifying critical spaces is important to ensure that the planning process for the user 268 269 evacuation process is implemented effectively. The identification of critical space based on the correlation between path density heat map and space usage LOS information [46] was 270 271 examined. Both user density and LOS flow information are important because the correlation 272 between these two identities can be used to improve the evacuation activities based on Equation 3 as stated by Wen and Chang [47] where Q is the space flow, P is the user density and C is 273 the user speed. Grid space allocation is performed to facilitate the identification of critical space 274 275 positions, as shown in Figure 11.

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$$Q = \frac{P_{n+1} - P_n}{C_{n+1} - C_n}$$
(3)

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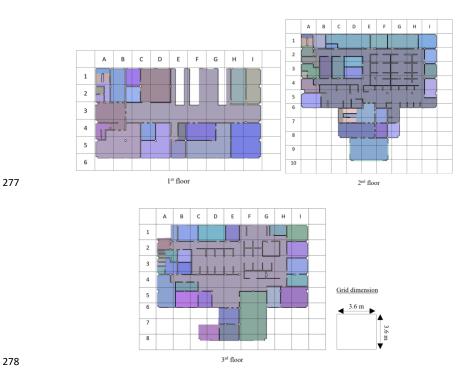


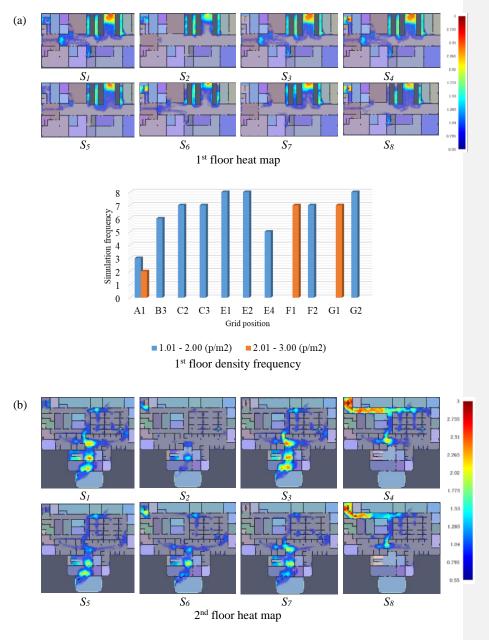


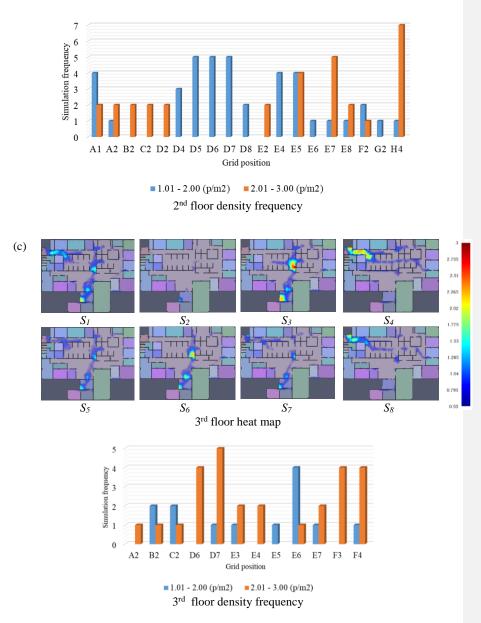
Figure 11. Grid space allocation for each floor

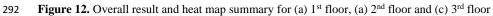
#### 280 3.3 Path density heat map

Detailing on heat maps are divided by floors and areas within in between 0.01 to 3.00 users per 281 282 square meter (p/m<sup>2</sup>). Ranges between 0.01 p/m<sup>2</sup> to 1.00 p/m<sup>2</sup> is classified as low density, 1.01 p/m<sup>2</sup> to 2.00 p/m<sup>2</sup> is classified as average density, and 2.01 p/m<sup>2</sup> to 3.00 p/m<sup>2</sup> is classified as 283 284 dense. For the 1st floor, the average user density is detected on grids, A1, F1 and G1. The focus on grid A1 is because the area involves a staircase that links between the 1st floor, 2nd floor and 285 3<sup>rd</sup> floor. As such, the A1 grid is indeed fundamental in the user's path. The next grids, F1 and 286 G1, cover the exit area for D2F1 access. This area is the centre of user density due to its 287 proximity to user-occupied office space. From this evaluation, it was found that the D1F1 288 289 access in the B3 grid only affects a user density of less than 2.00 p/m<sup>2</sup> and gives the impression  $\,$  that the flow of a user through the access is smooth. The overall findings of the heat map

291 information by the grid for the  $1^{st}$  floor is shown in Figure 12(a).







For the  $2^{nd}$  floor, the average user density is detected in two zones. For zone 1 it involves grids

E5, E7, E8 and H4 while zone 2 involves grids A1, A2, B2, C2, D2, E2 and F2. Density in

zone 1 is due to three main factors. First, the access in the H4 grid next to the office space is 295 too limited to accommodate the capacity of the users where visible frequencies occur for seven 296 297 simulations. The second factor is due to the closeness of the accesses to each other, such as the access to the E5 and E7 grids where the frequency occurs in four simulations for the E5 grid 298 and in five simulations for the E7 grid. The third factor involves the staircase area used by users 299 300 on the 3rd floor as in the E7 grid. Concurrently, the zone 2 density occurs due to the exit access 301 in relation to the staircase area used by the user from the 3rd floor in grid A1 and grid A2 where the frequency occurs in two simulations. The graphs of density heat map for the 2<sup>nd</sup> floor are 302 as shown in Figure 12(b). 303

For the 3<sup>rd</sup> floor, the user density is detected in three groups of regions. First in grids A2, B2, 304 C2. This area involves access to zone 2 where it provides access to stairs. However, the 305 306 frequency of this area involves only one simulation. Second in grids D6, D7, E6 and E7 where 307 this area is also the access to the stairs through zone 1 but has a high frequency of four simulations for grid D6, five simulations for grid D7, one simulation for grid E6 and two 308 309 simulations for grid E7. The third involves intermediate access in the middle of the 3<sup>rd</sup> floor, which is the main access involving the E3, E4, F3 and F4 grids. Frequency density is two 310 311 simulations for grid E3, two simulations for grid E4, four simulations for grid E7, and four simulations for grid E8. The graphs of grid heat density maps for the 3<sup>rd</sup> floor are as shown in 312 Figure 12(c). 313

#### 314 3.4 LOS on space usage

The LOS space utilization evaluation details are divided into six categories according to theFruin-based LOS model [46] as shown in Table 5.

317

Table 5. LOS categories according to the Fruin-based LOS model.

| LOS | Space (m <sup>2</sup> /p) | Access width (m) | Flow condition    |
|-----|---------------------------|------------------|-------------------|
| А   | ≥3.25                     | 1.93-1.80        | Free flow         |
| В   | 2.30-3.25                 | 1.80-1.67        | Small conflict    |
| С   | 1.39-2.30                 | 1.67-1.52        | Slow flow         |
| D   | 0.93-1.39                 | 1.52-1.36        | Partially limited |
| Е   | 0.46-0.93                 | 1.36-1.18        | Fully limited     |
| F   | ≤0.46                     | 0.95-0.68        | Compact           |

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Attention is given to access that disrupts the user evacuation flow based on space usage information involving the categories of flow conditions E and F LOS. This category was chosen as an indicator to indicate that the flow condition was not smooth for emergency situations as described by Campisi et al. [46].

For the 1st floor, on average, the flow condition E was detected due to D1F1 access for grid B3 325 326 and the flow condition F was derived from D2F1 for grid G1 as shown in Figure 13(a). The use of space above 2.17 p/m<sup>2</sup> is because D2F1 access cannot accommodate large numbers of 327 328 users at a time. A 1.2m wide access can only accommodate one user at a time. This is stated by Zegeer [48] where the Federal Highway Administration's (FHWA) Pedestrian Facilities Users 329 Guide states that a 1.5m wide access will allow two people to pass by in a smooth flow [49][50]. 330 This is also supported by a study conducted by Pan et al. [7] where the minimum recommended 331 332 access width for launching user transfer flows is 1.4m to 1.5m wide. That is also proved in this study when D2F1 access is extended to 1.5m, user density in D2F1 access decreases from flow 333 condition F to flow condition E. Expansion of D2F1 access also affects user density in D1F1 334 access where user density flow in D2F1 access decreases from flow condition E to flow 335 condition D. The difference in the use of space can be seen in Figure 14. 336

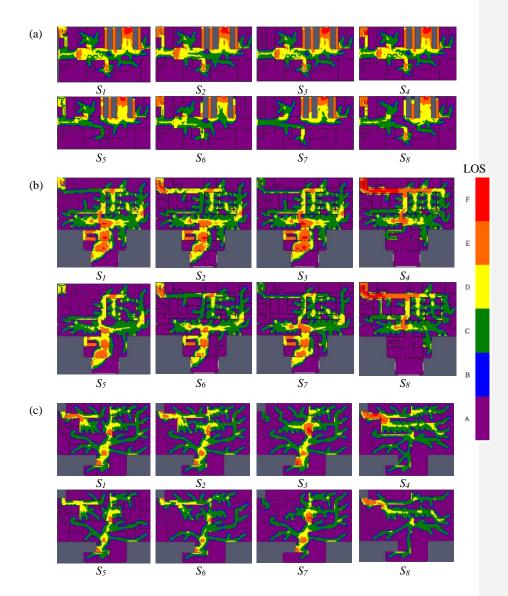


Figure 13. Overall result LOS for (a) 1st floor, (a) 2nd floor, and (c) 3rd floor

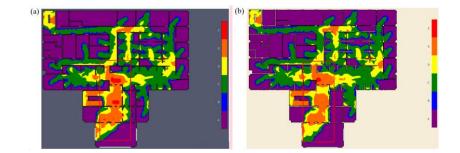
**Commented [BP9]:** Please increase the font size of (a) and (b) and make it bold.

Figure 14. Changes in LOS flow conditions in D1F1 and D2F1 before (a) and after (b)
access widening.

339

On average, for the 2<sup>nd</sup> floor, E and F flow conditions were detected as a result of access to 342 grids E5, E6, E7 and E8 as seen in Figure 13(b). The used space in the E5 grid above 2.17  $p/m^2$ 343 is due to access of the E5 grid as the main access to the 2<sup>nd</sup> floor that connects the building's 344 345 interior space to the exits of the building. It has two 0.8m wide access that can accommodate one user per access at a time. In order to optimize the space at a time, the user space allocation 346 can be implemented as done in  $S_2$ . Through the  $S_2$  evacuation method, it was found that the use 347 of space was in the flow condition E compared to other simulations that reached the flow 348 condition F. 349

As for access in the E6 grid, the user density is a continuation of the density that occurs in the 350 E7 grid. This is due to the density occurring in the E7 grid due to the combination of the 2<sup>nd</sup> 351 floor and 3<sup>rd</sup> floor user capacities that go down the stairs in the D7 grid. The number of users 352 353 doubled and the two 0.8m spreads on the E7 grid could not accommodate the overwhelming number of users. The solution can be achieved as described before by combining two 0.8m 354 widths to one 1.6m width access to allow two people to pass adjacent to the free flow as 355 described by Quezon and Kumala [50] and Pan et al. [7]. This is also proven in this study when 356 access to the E7 grid is consolidated, the flow of user density decreases to the flow condition 357 E. The difference in user density can be seen in Figure 15. 358



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**Figure 15.** Changes in LOS flow conditions in E7 grid before (a) and after (b) access widening.

**Commented [BP10]:** Please increase the font size of (a) and (b) and make it bold.

The average flow conditions for the 3rd floor, E and F, were detected as a result of access to 362 363 grids D7, E3, F3 and E6 as in Figure 13(c). The D7 grid density above 2.17 p/m<sup>2</sup> is due to the fact that the D7 grid access is the main access for 3<sup>rd</sup> floor users to get to the 2<sup>nd</sup> floor through 364 the stairs. The E3 and F3 grids are the main access points for D1F3 with a width of 0.8m and 365 can only load one user at a time. Obstacles caused by workers' cubic fractures can be rearranged 366 to allow them to accommodate more specialized users in emergency situations. For access 367 368 points on grid E6, the flow condition E is due to this space having two 0.8m wide access that can accommodate one user per access at a time. Combining two 0.8m width access to create 369 370 one 1.6m width access will allow two people to access adjacent to the free flow as described in the Pedestrian Facilities Users Guide and supported by a study conducted by Pan et al. [7] 371 372 where the recommended minimum access width is 1.4m to 1.5m wide to reduce user density 373 at a time. This is also evident in this study; when access to the E6 grid is consolidated, the user density of flow condition E decreases. The difference in user density can be seen in Figure 16. 374

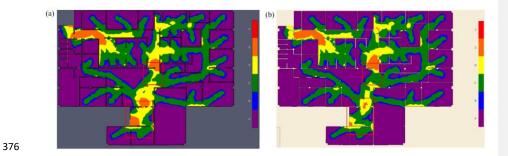


Figure 16. Changes in LOS flow conditions E in E6 grid before (a) and after (b) access
widening.

#### 379 4.0 Discussion

Based on the results obtained from input parameters and simulation validation, it is divided into two factors; the time factor and the critical space factor. The effects of the time factor based on eight simulations that were performed showed that the divided access recorded the fastest time in evacuating users.  $S_2$  recorded a time of 71.5 seconds which is 56.75% faster than the longest time recorded for 100% capacity and  $S_6$  recorded a time of 66.0 seconds which is 50.68% faster than the longest time recorded for 70% capacity. The information is shown in Table 6.

387

#### Table 6. Time different percentages

| User capacity (d <sub>1</sub> ) | Simulation | Time exited, $t_2$ (sec) | Time different percentages (%) |  |  |
|---------------------------------|------------|--------------------------|--------------------------------|--|--|
|                                 | $S_1$      | 77.30                    | 53.24                          |  |  |
| 1000/                           | $S_2$      | 71.50                    | 56.75                          |  |  |
| 100%                            | $S_3$      | 89.30                    | 45.98                          |  |  |
|                                 | $S_4$      | 165.30                   | 100.00                         |  |  |
|                                 | $S_5$      | 69.50                    | 44.53                          |  |  |
| 700/                            | $S_6$      | 61.80                    | 50.68                          |  |  |
| 70%                             | $S_7$      | 71.30                    | 43.10                          |  |  |
|                                 | $S_8$      | 125.30                   | 100.00                         |  |  |

389 As for the user capacity aspect, thise study found that the higher the time spent on user transfers, the higher the impact on user capacity in evacuation users. The distribution of users within the 390 391 compartment is also influencing and can be controlled through a restructuring of office space by providing a specific path to exit access to minimize the impact. The final result of the critical 392 space factor found to be 1st floor access on-grid G1, 2nd floor access on grids E5 and E7, 3rd 393 394 floor access on grids D7, E3, E6 and F3 should be given attention. This is because these 395 accesses affect the flow of the user evacuation process and user density is frequently detected in these areas. Some suggestions such as access widening and divide access have been made. 396 397 The following suggestions have also been tested and the results are shown in Figure 17, prove towhich would help improve the flow of the user evacuation process. The high rate of flow per 398 399 time is crucial in an emergency situation. These results are also in line with a study conducted 400 by Pan et al. [7] where the minimum recommended access width for smooth user transfer flows 401 is 1.4m to 1.5m wide.

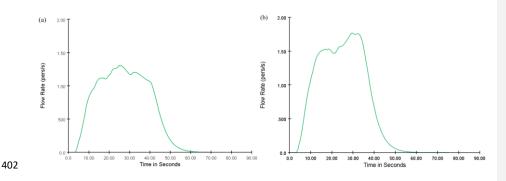




Figure 17. Changes in D2F1 flow rate before (a) and after (b) access widening.

404

#### 406 Conclusion

407 The basis of this study has been applied to evaluate the impact of evacuation planning structure on user evacuation time. An assessment has been conducted on the CIB and an understanding 408 was concluded of how different scenarios influence evacuation time. Significant findings in 409 this paper include the identification of critical space based on specific capacity and path 410 selection behaviour to improve the evacuation flow. In order to enhance the user evacuation 411 412 process, improvement measures should be implemented to minimize the impact of emergency 413 situations on users. A comprehensive solution can be implemented as a simulation testing 414 framework for the user evacuation process that can be used to replicate a real--world scenario 415 with the user. In addition, the seamless design of evacuation planning in the form of multiple 416 preferences of designs, the proper used equations while designing the evacuation path, the path 417 distance toward exits, and the location of the stairs needed to take into account. For example, 418 the division of access based on distance and time can be implemented to help facilitate the process of evacuating users. The action of improved access points such as the widening of exit 419 420 access space can be taken into account as the simulation results show that there is a positive impact on the widening of accesses that were identified as critical spaces. 421

422

#### 423 **Disclosure statement**

424 No potential conflict of interest was reported by the author.

#### 425 Data and Code Availability Statement

- 426 The data and codes that support the findings of this study are available figshare.com with the
- 427 identifier https://doi.org/10.6084/m9.figshare.12000540.v1
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