

Elsevier required licence: © <2021>. This manuscript version is made available under the CC-BY-NC-ND 4.0 license <http://creativecommons.org/licenses/by-nc-nd/4.0/>  
The definitive publisher version is available online at <https://doi.org/10.1016/j.memsci.2020.118901>

1 **Inkjet Printed Single Walled Carbon Nanotube as an Interlayer for High**  
2 **Performance Thin Film Composite Nanofiltration Membrane**

3 Myoung Jun Park<sup>†1, a</sup>, Chen Wang<sup>†1, a</sup>, Dong Han Seo<sup>a</sup>, Ralph Rolly Gonzales<sup>a, b</sup>, Hideto  
4 Matsuyama<sup>b</sup>, Ho Kyong Shon<sup>a\*</sup>

5  
6 <sup>a</sup> *Centre for Technology in Water and Wastewater (CTWW), School of Civil and Environmental*  
7 *Engineering, University of Technology Sydney (UTS), New South Wales, Australia*

8 <sup>b</sup> *Center for Membrane and Film Technology, Kobe University, Kobe, Hyogo, Japan*

9  
10  
11  
12  
13  
14 <sup>†</sup> These authors contributed equally in this work

15 \*Corresponding authors: Ho Kyong Shon; Email: [hokyong.shon-1@uts.edu.au](mailto:hokyong.shon-1@uts.edu.au); Tel.: +61 2  
16 9514 2629; Fax: +61 2 9514 2633.

17  
18  
19

20 **Abstract**

21 Inkjet printing process enables rapid deposition of inks with precise amount and location.  
22 Moreover, the process can be automated and provide control such as repetitive printing of the  
23 inks. Utilizing the advantageous features of the inkjet printing process, we demonstrate the  
24 synthesis of thin film composite (TFC) flat-sheet membrane for NF application where single  
25 walled carbon nanotube (SWCNT) was deposited via an inkjet printing process, acting as an  
26 interlayer between the polyamide (PA) selective layer and polyethersulfone (PES) MF  
27 membrane support. By controlling the number of SWCNT printings on the PES membrane, we  
28 investigated how the SWCNT interlayer thickness influences the formation of PA selective  
29 layer. The best membrane performance was achieved from the TFC membrane synthesized  
30 using 15 cycles of SWCNT printing, where both high water flux ( $18.24 \pm 0.43 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$ )  
31 and the high  $\text{Na}_2\text{SO}_4$  salt rejection ( $97.88 \pm 0.33\%$ ) rates were demonstrated. SWCNT  
32 interlayer provided highly porous, interconnected structure with uniform pore size distribution  
33 which led to the formation of a defect-free ultrathin PA selective layer. Designing of TFC  
34 membrane using the SWCNT deposition via inkjet printing is the new approach and  
35 successfully demonstrated the significant improvement in the NF membrane performances.

36 **Keywords:**

37 Nanofiltration, Inkjet printing, Interlayer, Single walled carbon nanotube, Thin film  
38 composite

39

40

41

42

43

## 44 1. Introduction

45 Thin film composite (TFC) membranes are conventionally synthesized by interfacial  
46 polymerization (IP) which forms a thin active layer on top of a microfiltration (MF) or  
47 ultrafiltration (UF) membrane substrates, where two different monomers of m-  
48 phenylenediamine (MPD) or piperazine (PIP) and trimesoylchloride (TMC) are commonly  
49 utilized to synthesis a polyamide (PA) active layer [1-3]. Both water permeability and  
50 selectivity of the membranes are most crucially dependent on PA active layer properties, while  
51 porous membrane support provides a robust mechanical support for PA selective layer. To  
52 this date, nanofiltration (NF) membranes composed of a thin film PA layer on top of UF  
53 membrane have been successfully commercialized and currently being used in wide range of  
54 applications in desalination and wastewater treatments. However, there are still challenges  
55 remain when they are implemented in the real field, due to their trade-off dilemma between the  
56 intrinsic solvent permeability and solute selectivity [4].

57 An ideal NF membrane needs to exhibit both high water permeability and high removal rate  
58 of various dyes or multivalent salts and other contaminants [5]. It is well known that, the  
59 thickness of PA selective layer is inversely proportional to the solvent permeability. Therefore,  
60 a desired PA layer structure can be achieved by fabricating an ultra-thin selective layer which  
61 is less than 100 nm in thickness whereas conventional TFC PA membranes are composed of  
62 200-300 nm thin PA active layer with 150-300  $\mu\text{m}$  porous support layer. Importantly,  
63 properties of the PA layer could significantly be influenced by structure and the surface  
64 property of a porous support substrate [6-9]. Recently, various efforts have been made to  
65 improve the membrane performances (water flux and selectivity) and membrane stabilities.  
66 One of a notable strategy is by addition of an interlayer between the PA active layer and the  
67 microporous support substrate. For example, Livingston et al. successfully synthesized a  
68 ultrathin PA active layer with a thickness of 10 nm by utilizing a porous cadmium hydroxide

69 nanostrands as interlayer which covered the surface of polyimide ultrafiltration support  
70 membranes and a follow up IP reaction [6]. The smooth and uniform nanoporous structure of  
71 the nanostrands interlayer enabled the formation of a defect-free and ultrathin PA active layer,  
72 which achieved outstanding improvement in solvent permeability while retaining its excellent  
73 salt rejection capability. Inspired by this study, Zhu and co-workers used polydopamine (PDA)  
74 coated single-walled carbon nanotube (SWCNT) as an interlayer which was deposited via a  
75 simple vacuum filtration technique [10]. This hydrophilic and smooth PDA/SWCNT interlayer  
76 induced the formation of defect-free, highly crosslinked PA selective layer with a thickness of  
77 12 nm, which improved the NF membrane performances compared to the interlayer free TFC  
78 membrane.

79 As noted in previous studies, deposition of interlayer using different nanomaterials played  
80 an important role in improving the NF membrane performances [7-15]. However, those  
81 conventional approaches such as vacuum filtration, dip-coating, spin-coating and layer-by-  
82 layer (LBL) methods in deposition of materials, as an interlayer for TFC membrane  
83 fabrications, often lead to poor controllability of the deposited material surface properties or  
84 limited in scalability and in some cases producing unwanted wastes [7, 9, 10, 16, 17].  
85 Meanwhile, inkjet printing process could be a promising candidate which can enable the  
86 deposition of nanomaterial based interlayer uniformly. Inkjet printing is a versatile tool which  
87 can deliver precise and rapid deposition of organic, polymeric materials and nanomaterials at  
88 scale for various applications [18-22]. Moreover, conventional routes in depositing polymers  
89 or nanomaterials often generated chemical and nanomaterial wastes which remains a  
90 significant challenge. These material wastage issues can be minimized when depositing  
91 materials via inkjet printing process as precise amount of material deposition is possible in this  
92 process.

93 Therefore, such features of the inkjet printing process and inspired from the successful  
94 implementation of inkjet printing process in other applications, this work aims to take the  
95 advantage of the inkjet printing technology in membrane manufacturing, which will deliver  
96 deposition of uniform nanomaterial interlayer with good controllability for high performing  
97 TFC membrane synthesis. In general, inkjet printing process enable the deposition of picoliter  
98 (2~30 pL/drop) scale of liquid drops through the number of nozzles from a print-head, with  
99 frequencies of up to 2000 drops s<sup>-1</sup> per nozzle [23]. Moreover, inkjet printing process provided  
100 precise control in positioning of the polymer solution deposition at a high speed [24]. Due to  
101 these advantages of inkjet printing technique, recent studies successfully demonstrated the  
102 uniform coating of nanomaterials such as graphene, graphene oxide, metal organic frameworks  
103 (MOF) and CNTs on a paper substrate for patterning of conductive materials [19, 25-27].  
104 Furthermore, one study has successfully demonstrated the deposition of ultrathin and uniform  
105 graphene oxide layer on a polymeric support membrane to synthesize a NF membrane for water  
106 purification [28]. As such, use of inkjet printing in membrane manufacturing require further  
107 exploration and demonstrations in diverse membrane synthesis applications to fulfill its  
108 potential in bringing the efficient, precision controlled and scalable membrane manufacturing  
109 into reality.

110 In this study, we demonstrate the deposition of uniform, smooth SWCNT layer via inkjet  
111 printing process to serve as an interlayer between the PA active layer and PES MF membrane  
112 which is first demonstration for NF application. Multiple number of SWCNT printings on the  
113 PES membrane were conducted to investigate how SWCNT interlayers influenced the  
114 formation of PA active layer using various membrane characterizations. Moreover, the  
115 performance of fabricated TFC NF membranes were evaluated by water permeability and salt  
116 rejection tests to find an optimal fabrication condition. The different surface characteristics of  
117 SWCNT interlayers induced by different number of inkjet printing and the respective formation

118 of PA layer was further investigated. Our studies shed light on the control of PA selective layer  
119 in TFC membrane by introducing the uniform, nanomaterial based interlayer and  
120 demonstration the further use of inkjet printing process in membrane manufacturing which  
121 plays a crucial role in synthesis of high performing TFC membrane.

122

## 123 **2. Experimental**

### 124 *2.1 Materials and chemicals*

125 Hydrophilic PES microfiltration (MF) membrane filter with a pore size of 0.22  $\mu\text{m}$  was used  
126 as membrane support (Sterlitech, USA). Carboxylated SWCNT (SWCNT, Purity: > 95 wt%,  
127 outer diameter (OD): 1-2 nm) powder with a short length (1~3  $\mu\text{m}$ ) was purchased from Jiangsu  
128 XFNANO Materials Tech CO., Ltd, China. Sodium dodecyl sulfate (SDS,  $\geq$  99.9%) from  
129 Sigma-Aldrich was used as the surfactant for SWCNT dispersion. For PA active layer  
130 formation, piperazine (PIP, 99% purity) and trimesoyl chloride (TMC, 98% purity) were  
131 purchased from Sigma-Aldrich and hexane (99.9% purity) from Merck was used as solvent for  
132 TMC. For evaluating the membrane performance, sodium chloride (NaCl), magnesium sulfate  
133 ( $\text{MgSO}_4$ ), magnesium chloride ( $\text{MgCl}_2$ ) and sodium sulfate ( $\text{Na}_2\text{SO}_4$ ) were supplied by Chem-  
134 Supply Pty. Ltd., Australia. All chemicals in this study were used as received. A Milli-Q ultra-  
135 pure water system (Millipore) was used to produce deionized (DI) water and used in all  
136 experiments.

### 137 *2.2 Inkjet printing of SWCNT ink on PES MF support membrane*

138 The SWCNT ink was prepared by sonicating 200 mg of SWCNT powder in 200 mL of 1  
139  $\text{mg mL}^{-1}$  SDS water solution for 4 h using a probe type high power ultrasonicator under 80 W  
140 of power. Removal of impurities was conducted via a centrifugation of solution at 7,000 rpm  
141 for 30 min and followed by a supernatant dispersion was collected. This step was repeated 3~4

142 times until the stable solution is collected and the SWCNT solution with a final concentration  
143 of  $\approx 0.25 \text{ mg mL}^{-1}$  was obtained and directly used as a SWCNT ink without adding further  
144 additives.

145 A commercial Deskjet 2130 HP printer with a cartridge nozzle diameter of  $30 \mu\text{m}$  was used  
146 to print the SWCNT ink onto the surface of PES MF membrane support. The size and ejection  
147 of an ink droplet is controlled by a HP thermal inkjet print technology. To prevent the  
148 membrane surface damage, the front paper feed rollers and the rear roller at the middle of the  
149 printer were removed prior to inkjet printing process as indicated in Fig. S1. A black ink from  
150 a commercial black inkjet cartridge (HP 63 Genuie Black) was removed and carefully washed  
151 and filled with prepared SWCNT ink in the presence of a sponge which prevents the leakage  
152 of the ink through the nozzles (see Fig. 1A). Afterwards, the SWCNT ink cartridge was loaded  
153 onto the printer. The PES MF membrane (size:  $6 \text{ cm} \times 6 \text{ cm}$ ) was firmly bind to an A4-sized  
154 polyethylene terephthalate (PET) film and was loaded into the printer. A computer was  
155 connected to the printer and the printing software was set on maximum quality with  $1200 \times 1200$   
156 dpi. Then the SWCNT ink was subsequently printed on the surface of membrane substrate and  
157 then dried in a controlled room temperature for 2 min. The number of printing was varied from  
158 0, 5, 10, 15 and 20 repetitions to investigate the effect of SWCNT thickness coated on a  
159 microporous PES membrane substrate as a function of interlayer. According to the number of  
160 prints, SWCNT ink printed samples were denoted as P-0, P-5, P-10, P-15 and P-20 in this  
161 paper.

### 162 ***2.3 Fabrication of thin-film composite (TFC) membranes***

163 Fabrication of TFC membrane via and interfacial polymerization (IP) to form a PA layer on  
164 the SWCNT-free (PES MF membrane) support and SWCNT-coated membrane supports was  
165 conducted using two monomers of PIP and TMC (Fig. 1B), as similarly with our previous



166 studies [29, 30]. Prior to IP process, prepared membrane supports were first pre-wetted by  
167 water without any alcohol treatment and stored in DI water for overnight. The remaining water  
168 on the membrane surface was removed by a filter paper and then only one side of membrane  
169 surface was allowed for exposure using an acrylic frame for introduction of PIP and TMC  
170 monomers. Then a certain concentration of PIP aqueous solution (0.05– 0.2 wt%) was poured  
171 on a membrane surface which was exposed to the air for 1 minute and followed by removal of  
172 excess liquid by wiping them out using a filter paper. Subsequently, 0.1 w/v% of TMC in  
173 hexane was then introduced onto the membrane surface for 30 s to allow the formation of a  
174 thin film PA active layer via IP reaction. The membranes were then dried in air for 1 minute  
175 and heat-cured to facilitate higher cross-linking of amine reaction in the oven at 65°C for 5  
176 mins. The fabricated TFC membranes were then kept in DI water and stored in a refrigerator  
177 at 4°C before use. The PA layers fabricated on the P-0, P-5, P-10, P-15, and P-20 membrane  
178 samples were denoted as TP-0, TP-5, TP-10, TP-15 and TP-20, respectively.

#### 179 ***2.4 Characterization of membrane supports and TFC membranes***

180 The morphological investigations via a field emission scanning electron microscope (FE-  
181 SEM) (Zeiss Supra 55VP, Carl Zeiss AG) operated at 5 kV were performed for both membrane  
182 supports and TFC membranes. For observing cross-section SEM images of TFC membranes,  
183 a piece of TFC membrane was soaked in liquid nitrogen to fracture the samples. All membranes  
184 were sputtered with Pd/Au using a coating machine (EM ACE600, Leica) before the FE-SEM  
185 characterization. Surface hydrophilic property of membrane supports was estimated by water  
186 contact angle measurements using an optical tensiometer (Theta Lite 100, Republic of Korea)  
187 equipped with an image processing software. All support membranes were washed with DI  
188 water to remove any impurities and post treatment agents and then dried at room temperature  
189 prior to analysis. At least five measurements for each samples were examined and obtained an

190 average value. Surface mean roughness ( $R_a$ , nm) of SWCNT-free and SWCNT-coated  
191 membrane supports was measured by atomic force microscope (AFM, Park X7) images with a  
192 scanning area of  $5\ \mu\text{m} \times 5\ \mu\text{m}$  and three measurements for each samples were performed and  
193 their average values were obtained. Additionally, an overall average pore size of membrane  
194 supports were determined using a capillary flow porometry (Porolux 100) under dry-up/wet-  
195 up mode and a low surface tension Porefil ( $16\ \text{dynes cm}^{-1}$ ) was used as a membrane wetting  
196 agent. To determine the atomic composition and degree of cross-linking of the PA layer in each  
197 TFC membrane, X-ray photoelectron spectroscopy (XPS, JPS-9010 MC, JEOL, Japan)  
198 analysis was performed. Based on the atomic composition analysis, the ratio of O and N can  
199 provide the degree of cross-linkage of the PA layer. The O/N ratio is inversely proportional to  
200 the degree of cross-linkage, which can be calculated using Eqns. (1) and (2):

$$201 \quad a + b = 1 \quad (1)$$

$$202 \quad \frac{O}{N} = \frac{3a+4b}{2a+2b} \quad (2)$$

203 where a and b are the fractions of the crosslinked structure and linear structure components of  
204 PA layer, respectively.

205 The surface zeta potential of TFC membranes was evaluated using an Anton Paar Surpass  
206 solid-surface analysis. All zeta potential tests at different pH (3-10) were carried out with 1  
207 mM KCl background solution at  $25^\circ\text{C}$  and the solution pH values were adjusted by dosing 0.1  
208 M HCl or 0.1 M NaOH solution.

### 209 ***2.5 Evaluation of separation performance for TFC membranes***

210 TFC membrane performance such as water permeation and salts rejection was evaluated  
211 using a Lab-scale membrane testing machine under cross-flow operation mode (cross-flow

212 velocity = 8.3 cm s<sup>-1</sup>) with effective membrane area of 4 cm<sup>2</sup>. Permeate water flux and salt  
213 rejection rates were determined under the testing pressure of 4 bar at a temperature of 23°C ±  
214 1. Prior to performance tests, membrane samples were pre-compacted with DI water for 30 min  
215 to minimize the effect of membrane compaction on membrane performance. The permeate flux  
216  $J_w$  was calculated using Eq. (3):

$$217 \quad J_w = \frac{V}{A\Delta t} \quad (3)$$

218 where  $V$  is the volume of the permeate water (L),  $A$  is the effective membrane area (m<sup>2</sup>), and  
219  $\Delta t$  is the time interval (h).

220 For the evaluation of the salt rejection performance, each 1,000 mg L<sup>-1</sup> of Na<sub>2</sub>SO<sub>4</sub>, MgSO<sub>4</sub>,  
221 MgCl<sub>2</sub> and NaCl salts were used as feed solutions and the conductivity of the feed and permeate  
222 solutions were measure using a portable conductivity meter (D-74G, Horiba scientific, Kyoto,  
223 Japan) to evaluate the salt rejection performance of the TFC membranes.

224 Salt rejection  $R$  was calculated by Eq. (4):

$$225 \quad R (\%) = 100 \times \left(1 - \frac{C_p}{C_f}\right)$$

226 (4)

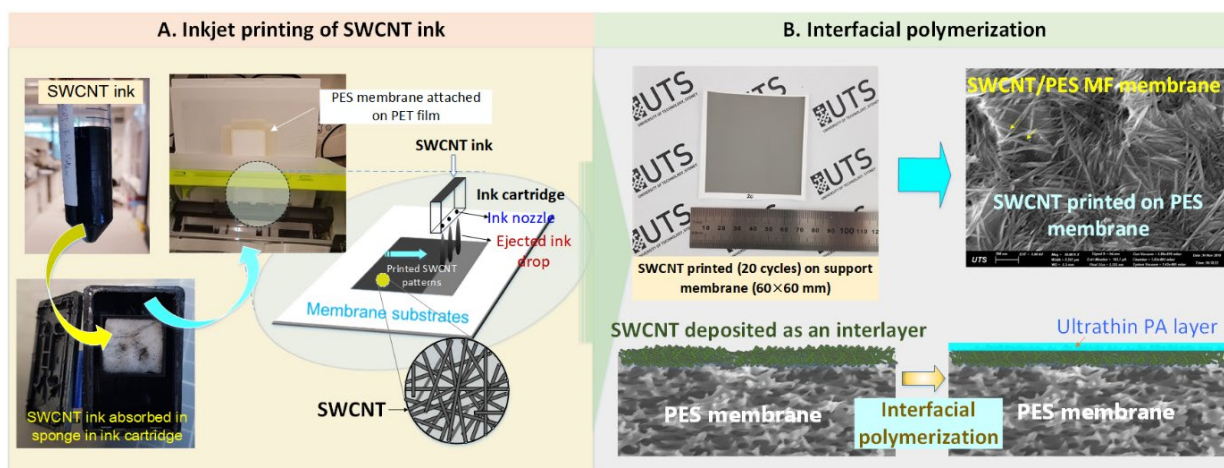
227 where  $C_f$  and  $C_p$  are the salt concentrations in feed and permeate, respectively.

228

### 229 **3. Results and discussion**

#### 230 ***3.1 Effect of SWCNT deposition via inkjet printing on PES MF membrane supports***

231 The SWCNT interlayer deposition on the PES MF support membrane was conducted via  
232 inkjet printing technology. The prepared SWCNT ink was smoothly printed on the membrane  
233 substrate and did not observe any blockage of nozzles in the cartridge head during the whole  
234 printing experiments (See supplementary video S1). The effects of coated SWCNT layer on  
235 the properties and morphology changes of PES membrane surface were investigated as these  
236 two parameters strongly influence the formation of PA layer during the IP process. Fig. 2 shows  
237 the FE-SEM and AFM images of support membranes without SWCNT interlayer and with  
238 SWCNT interlayer coating. Pristine PES (P-0) MF membrane surface reveals a plane  
239 polymeric surface with micron-sized open pores. However, as the numbers of SWCNT ink  
240 printed on the membrane support increased, the open pores on the membrane surface were  
241 covered by SWCNT network. When the 15 printings of SWCNT ink were performed, open  
242 pores on the PES membrane surface were fully-covered with SWCNT network. For instance,  
243 micro-pores on the PES membrane surface for P-15 and P-20 samples, disappeared over the 15  
244 cycle of SWCNT ink prints, where SEM images exhibit continuous and dense-compact  
245 SWCNT network formation on the surface of the PES membrane support. The volume of each  
246 ink drop of the ink cartridge 63 is around  $22 \times 10^{-12}$  L, and each drop covers an average surface  
247 area of  $90 \times 1,000 \mu\text{m}^2$  [28]. Therefore, 1 mL of SWCNT ink can covers about  $410 \text{ cm}^2$  area of  
248 membrane surface and for SWCNT ink with the concentration of  $\approx 0.25 \text{ mg ml}^{-1}$  can deposit  
249  $0.00061 \text{ mg cm}^{-1}$ . In case the printing of 15 and 20 cycles can deposit SWCNT of 0.0092 and  
250  $0.0122 \text{ mg cm}^{-2}$ , respectively, as indicated in Table 1. This calculation indicates that only small  
251 amount of SWCNT (0.01 mg) was needed to effectively form a SWCNT network with full  
252 coverage on the  $1 \text{ cm}^2$  area of PES membrane support demonstrating the material efficiency of  
253 the inkjet printing process. An accumulation of SWCNT in different printing numbers can also  
254 apparently be distinguishable from the optical images exhibited in Fig. S2. The PES membrane  
255 surface has revealed darker grey colors with increase in SWCNT printing numbers.



256

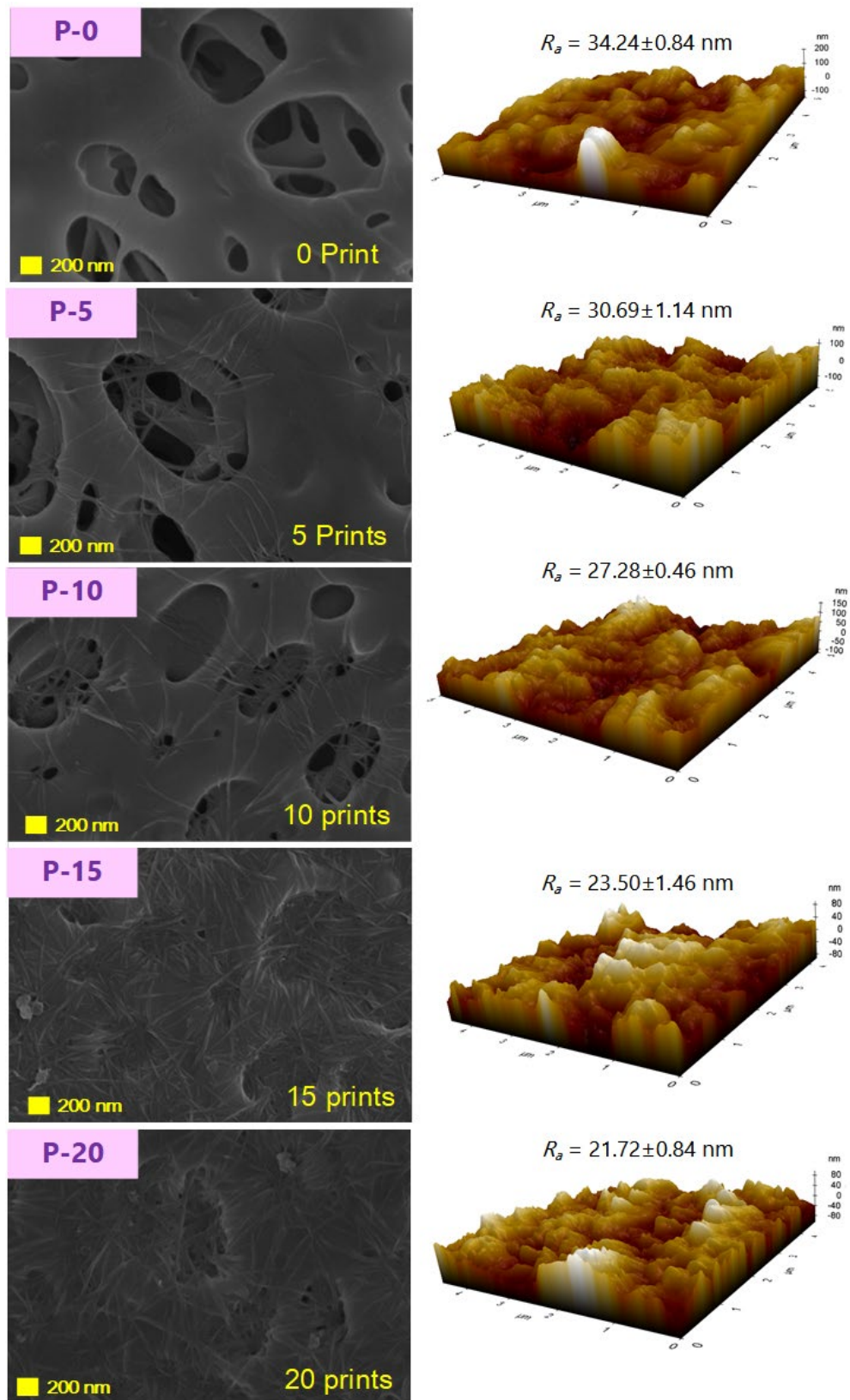
257 **Fig. 1.** Schematic of (A) SWCNT deposition on PES MF membrane via inkjet printing and  
 258 (B) ultrathin PA active layer deposition onto SWCNT coated PES membrane via interfacial  
 259 polymerization (IP).

260 **Table 1.** Pure water permeability, contact angle, average pore size and deposited SWCNT  
 261 amount of SWCNT-coated samples respect to the number of SWCNT ink prints.

Sample	Number of SWCNT ink prints	SWCNT amount (mg cm <sup>-2</sup> )	Average pore size (nm)	Pure water permeability (L m <sup>2</sup> h <sup>-1</sup> bar <sup>-1</sup> )	Contact angle <sup>(a)</sup> (Deg)
P-0	0	0	274.0	4505 ± 509	68.12 ± 2.20
P-5	5	0.0031	219.9	4057 ± 816	69.50 ± 3.13
P-10	10	0.0061	128.2	3427 ± 222	59.87 ± 2.69
P-15	15	0.0092	93.2	2332 ± 180	78.49 ± 4.16
P-20	20	0.0122	53.5	495 ± 42	83.19 ± 1.61

262 <sup>(a)</sup> Contact angle of water droplet measured at 0 sec.

263

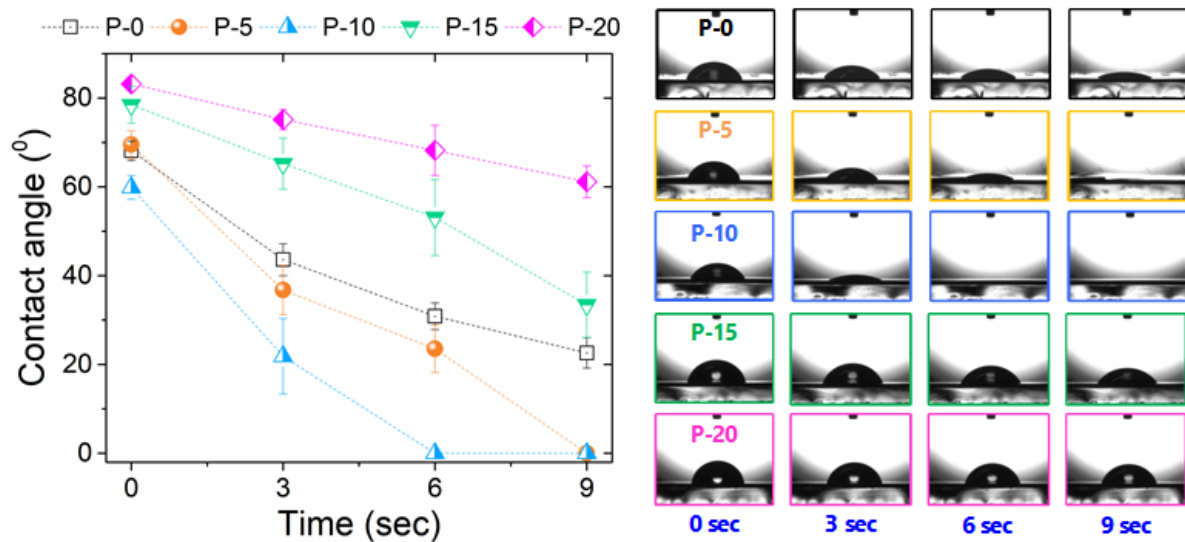


264 **Fig. 2.** FE-SEM and AFM images of the surfaces profile of PES MF membranes and the  
 265 SWCNT interlayer deposited PES membranes (P-0, P-5, P-10, P-15 and P-20).

266 From AFM images (right hand side figures from the Fig. 2), one can observe that with  
267 increasing number of SWCNT printing, the surface roughness ( $R_a$ ) value gradually decreased.  
268 The P-0 showed an average surface roughness value of  $34.24 \pm 0.84$  nm and then it decreased  
269 to  $30.69 \pm 1.14$  nm,  $27.28 \pm 0.46$  nm,  $23.50 \pm 1.46$  nm and  $21.72 \pm 0.84$  nm for P-5, P-10, P-  
270 15 and P-20, respectively. These results demonstrate that SWCNT layer provides a smoother  
271 and denser surface with increasing number of SWCNT deposition. Meanwhile, the initial water  
272 contact angle of the membranes (Table 1) slightly decreased as the number of SWCNT ink  
273 printings increased up to 10 cycles. Without SWCNT interlayer deposition, the initial water  
274 contact angle was  $68.12^\circ$ ; however, it was decreased to  $59.87^\circ$  after 10 cycles of SWCNT  
275 printing. The reduction of contact angle is mainly attributed to the presence of hydrophilic  
276 carboxylated SWCNT coating on the PES support, and the clear trend can be seen from the  
277 time profile measurement shown in Fig. 3. The P-5 ( $69.50^\circ$ ) membrane had the similar initial  
278 contact angle with the P-0. However, there is a sharper drop of the contact angle appeared for  
279 P-5 sample with time and the water droplet completely disappeared after 9 s, and more  
280 significant reduction was observed for P-10 sample. In contrast, it can be noted that when the  
281 number of SWCNT prints exceeded 15 cycles (P-15 and P-20 samples), the contact angles were  
282 increased compared to that of P-0 sample. This is due to the more densely packed SWCNT  
283 network structure with increased deposition amount of the SWCNT leading to significant  
284 decrease in pore size of the membrane (see Table 1). Thus, reduced pore size might hindered  
285 the rapid penetration of water droplet, resulting in slight increase of the water contact angle  
286 and similar trends are also observed from previous literatures [12, 31]. The pure water flux of  
287 the support membranes (before IP process) was also measured to see the impact of SWCNT  
288 deposition on the membrane performance. As shown in Table 1, the SWCNT-free PES support  
289 (P-0) revealed the pure water flux of  $4545.1 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$  which is typical permeability value  
290 for MF membranes and then there was a gradual flux decline observed from 4057.5 to 2332.5

291  $\text{L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$  with increasing number of SWCNT printings from 5 to 15 printing cycles,  
292 respectively. Further to this, it can be noted that there was a considerable drop in water flux for  
293 P-20, where 10 fold reduction in flux was observed ( $495.0 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$ ) compared to the P-  
294 0 membrane. This result is due to the significant decrease in membrane pore size by  
295 accumulation of SWCNT layer induced by repeated cycles of printing and these results are in  
296 good agreement with the contact angle measurement. Average pore size of support membranes  
297 was also measured for further confirmation and it is summarized in Table 1, and this result  
298 supports the pure water flux measurement results. As noted in Table 1, the average pore size  
299 was reduced when the printing number of SWCNT was increased. The average pore size of  
300  $274.0 \text{ nm}$  was obtained for pristine PES support membrane (P-0) and this value is well-matched  
301 with the manufacturer's information ( $220 \text{ nm}$ ). Eventually the pore size reached to  $53.5 \text{ nm}$  by  
302 20 cycles of SWCNT ink printing which represented similar pore size of typical UF membranes.  
303 These results support that SWCNT layer coated on the PES MF membrane, significantly  
304 changed the surface morphology, and induced by varying deposition amount of SWCNT which  
305 was controlled by the number of printing cycles. Such parameter altered the compactness of  
306 the SWCNT network on PES support, thus reducing the pure water flux, surface pore size and  
307 the surface roughness, while increasing the contact angle of the membrane support. All these  
308 results are also consistent comparing with the previous studies which used CNTs as an  
309 interlayer for high performance NF membrane fabrication [8, 10-12, 31, 32].





310

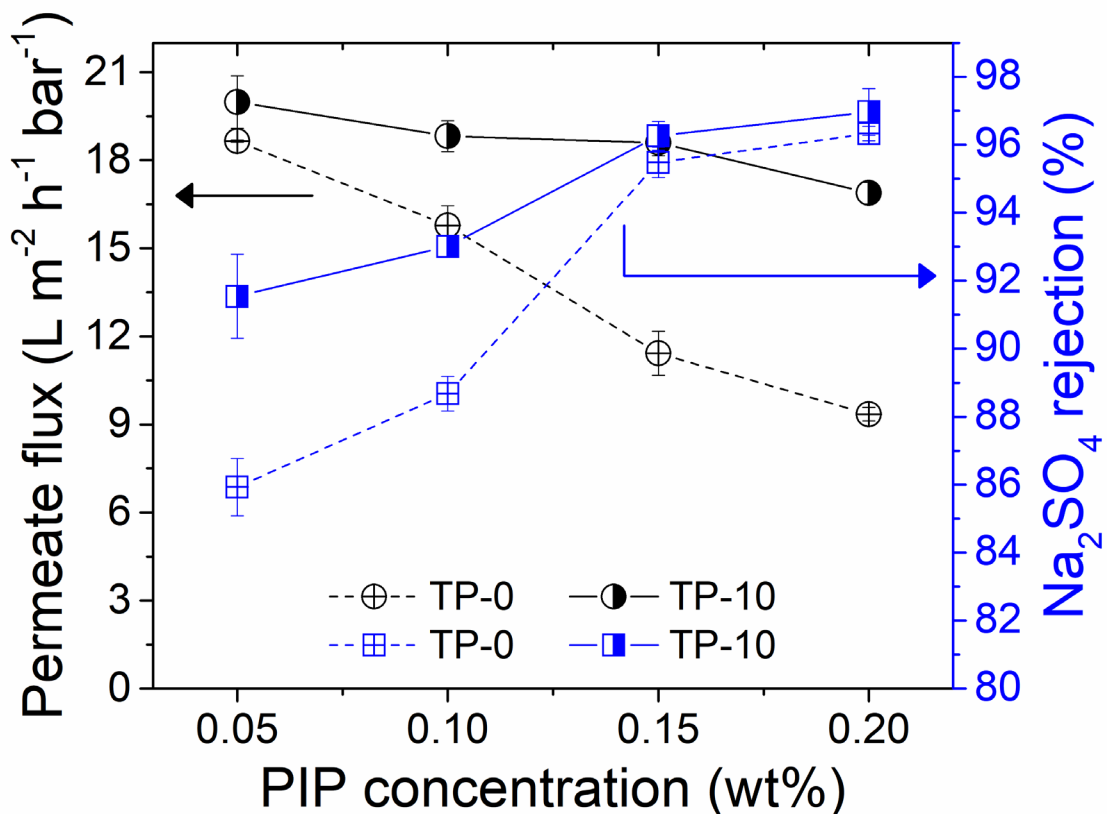
311 **Fig. 3.** Contact angle trend of membrane supports as a function of contact time.

312

### 313 **3.2 Optimization of IP condition at different PIP concentrations**

314 Effect of PIP concentrations on NF membrane performance was investigated to find out an  
 315 optimum IP condition as well as a role of SWCNT interlayer. Two samples of pristine PES MF  
 316 membrane support (P-0) and SWCNT deposited on PES support by 10 SWCNT ink printings  
 317 (P-10) were used to conduct the IP process to compare the NF performance and their  
 318 corresponding TFC membranes were denoted to TP-0 and TP-10, respectively. The PIP  
 319 monomer concentration was varied at 0.05, 0.1, 0.15 and 0.2 wt% while the TMC concentration  
 320 was fixed at 0.1 w/v% for the formation of PA layer on the membrane substrates. Fig. 4  
 321 represents the permeate water flux and salt rejection ( $\text{Na}_2\text{SO}_4$  1,000 mg L<sup>-1</sup> as feed solution)  
 322 performances of TP-0 and TP-10 TFC-NF membrane samples tested under applied pressure of  
 323 4 bar. Overall, both TP-0 and TP-10 TFC membranes exhibited similar water flux and salt  
 324 rejection trend as a function of different PIP concentrations in IP process, where the water flux  
 325 decreased while  $\text{Na}_2\text{SO}_4$  divalent salt rejection improved as PIP concentration was increased.  
 326 This is mainly attributed to the less defects are formed in the PA selective layers when PIP

327 monomer concentration is increased, which resulted in increasing water transport resistance  
 328 indicating the reduction of water flux but improving the salt retention across the thin PA  
 329 selective layer. Such observation is also supported by previous literatures [10, 14]. From the  
 330 performance trend shown in Fig. 4, TP-10 membrane was less affected by the PIP  
 331 concentrations compared to TP-0 membrane in membrane performances. Water flux of 19.98  
 332  $\text{L m}^{-2} \text{h}^{-1} \text{bar}^{-1}$  was observed for TP-10 membrane showing slightly higher value compared to  
 333 the TP-0 membrane ( $18.65 \text{ L m}^{-2} \text{h}^{-1} \text{bar}^{-1}$ ) at low PIP concentration of 0.05 wt%. However,  
 334 there is considerable decline in water flux for TP-0 membrane observed with increase in PIP  
 335 concentration, where water flux declined by 50% to  $9.35 \text{ L m}^{-2} \text{h}^{-1} \text{bar}^{-1}$  at the PIP concentration  
 336 of 0.2 wt%, while only 24% ( $16.88 \text{ L m}^{-2} \text{h}^{-1} \text{bar}^{-1}$ ) was reduced for TP-10 membrane under the  
 337 same PIP concentration.



338

339 **Fig. 4.** Permeate flux and salt rejection ( $\text{Na}_2\text{SO}_4$  1,000  $\text{mg L}^{-1}$ ) performance of NF  
340 membranes for TP-0 and TP-10 TFC membranes fabricated under different PIP  
341 concentrations (0.05, 0.1, 0.15 and 0.2 wt%).

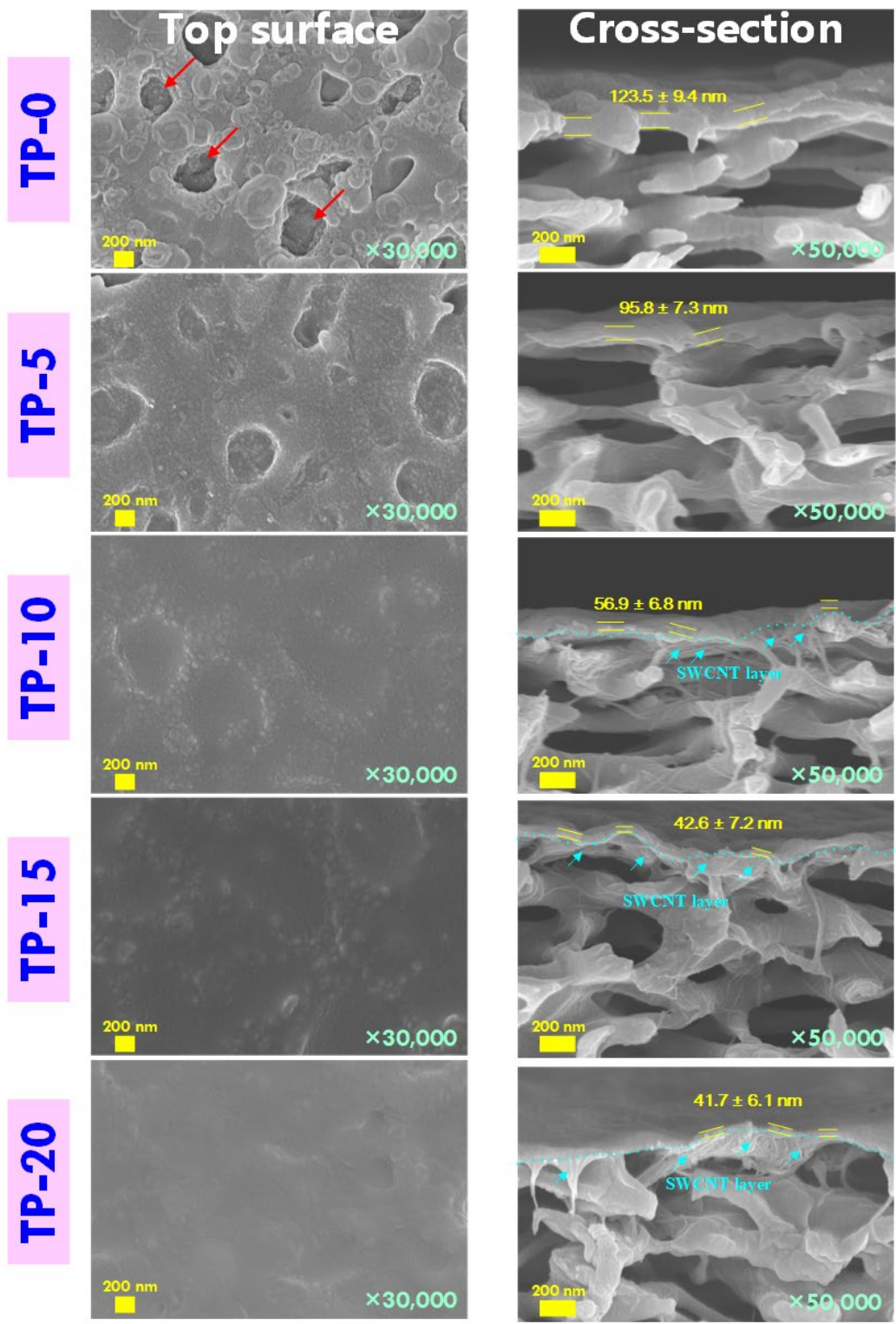
342 Meanwhile, a significant improvement in  $\text{Na}_2\text{SO}_4$  rejection was observed for TP-10 membrane  
343 with increase in PIP concentration. The result shows that salt rejection rate was increased from  
344 91.54% to 96.26% at PIP concentration ranging from 0.05 wt% to 0.15 wt%, respectively, and  
345 this result is comparable to the level of typical NF membranes performance. Although the TP-  
346 0 membrane also followed a similar trend, by showing improvements in salt rejection rate, yet  
347 its  $\text{Na}_2\text{SO}_4$  rejection rate was lower values than that of P-10 membrane at all PIP concentrations.  
348 From the above experimental results, it can be deduced that the membrane support surface  
349 modified with SWCNT interlayer with 10 cycle of prints, provided the surface condition for  
350 stable and enhanced polymerization to occur by reducing average pore sizes from 274 nm (P-  
351 0) to 128.2 nm (P-10) with porous and interconnected matrix, which helped the formation of  
352 defect-free and thin PA active layer even at relatively low PIP concentrations. Therefore, the  
353 optimum IP condition for this study was selected at the PIP concentration of 0.15 wt% which  
354 exhibited minimal decline in water flux while maintaining a good salt rejection rate (> 95%).

### 355 ***3.3 Effect of SWCNT as an interlayer on the PA active layer formation***

356 Formation of PA selective layer on the surface of membrane supports were performed via IP  
357 process using PIP (0.15 wt%) and TMC (0.1 wt%) monomers, and the surface morphologies  
358 and the thickness of PA layers were characterized by FE-SEM. Fig. 5 illustrates the top surface  
359 (left) and cross-sectional (right) images of PA layer for TFC-NF membranes without SWCNT  
360 deposition (TP-0) and with SWCNT deposition (TP-5–20) representing the different numbers  
361 of inkjet printing cycles. Considerably rough and nodular shapes of PA was formed on the top  
362 surface of the SWCNT-free membrane (TP-0) which is shown in Fig. 5 and one can expect that

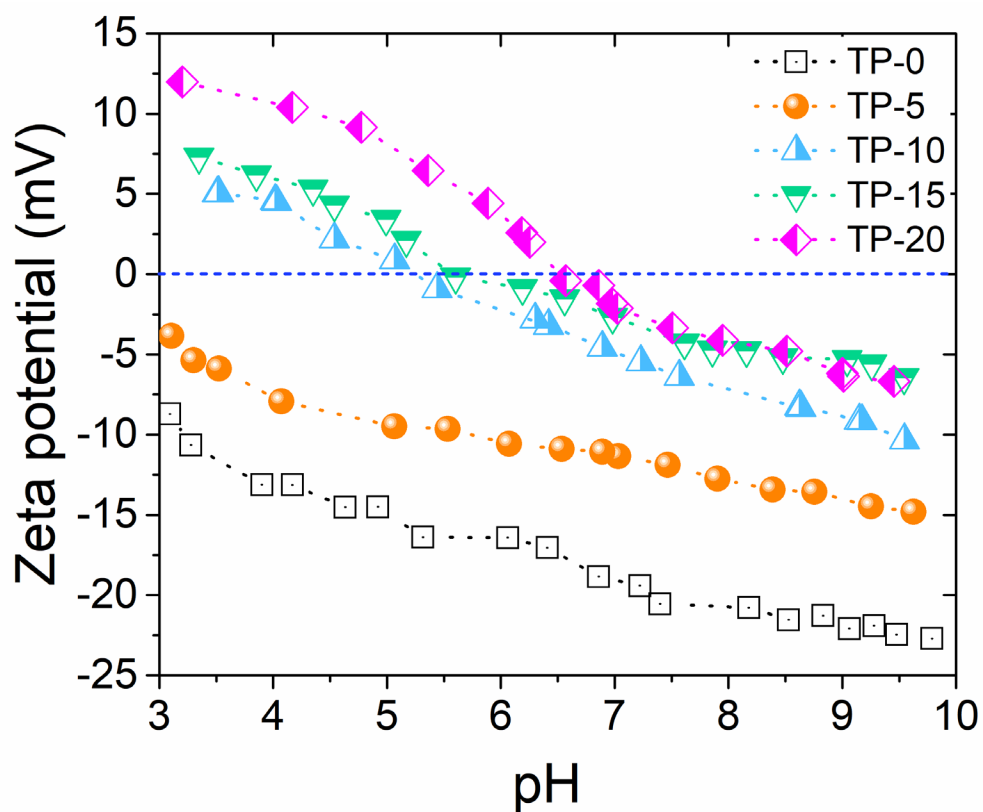
363 there would be some defects formed during the PA formation. Moreover, one can notice that  
364 the PA layer was formed inside the large pores of PES MF support (pore size of 274 nm) as  
365 indicated by red arrows on the top surface SEM image of TP-0. This might be formed from the  
366 remaining PIP monomer entrapped within the micropores, due to the large, rough, and  
367 discontinuous pore structure of the PES substrate. This resulted in the non-uniform distribution  
368 of PIP on the substrate, and subsequent formation of discontinuous, thick, and relatively rough  
369 PA surface layer [31, 32]. On the other hand, smoother and flatter PA layer is formed when the  
370 number of SWCNT interlayer depositions was increased as shown in Fig. 5. Patterns of  
371 micropore of the membrane surface became less obvious or disappeared in the orders of TP-5,  
372 TP-10, TP-15 and TP-20 membranes when covered with PA layer. It clearly indicates that  
373 uniformly-dispersed and deposited SWCNT interlayer led to the reduced pore size with smooth  
374 membrane surface, which helped the uniform diffusion of PIP solution, thus resulting in a  
375 formation of defect-free, continuous, and smooth PA active layer. More details on PA layer  
376 formation without and with SWCNT interlayers on PES membrane support will be discussed  
377 in Section 3.5.

378 Furthermore, the thickness of PA active layer was significantly reduced as SWCNT ink  
379 printing numbers increased, as revealed in the cross-sectional images in Fig. 5 (right hand side).  
380 The TP-0 sample (SWCNT free) exhibited PA layer thickness of  $123.5 \pm 9.4$  nm. However,  
381 when the SWCNT ink was printed more than 10 cycles, the thickness of PA active layer was  
382 observed to be less than  $< 60$  nm. Ultrathin PA active layer was consistently formed with  
383 thickness of  $\sim 42$  nm when the SWCNT ink printing exceeded 15 cycles as can be clearly seen  
384 in Fig. 5 and Fig. S3. SWCNT layer provided the reduced pore size and interconnected pore  
385 matrix with increased surface porosity which would facilitate the formation of ultrathin PA  
386 layer [32].



387

388 **Fig. 5.** Surface and cross-sectional FE-SEM images of the TFC NF membranes with different  
 389 number of SWCNT ink printings.



390

391 **Fig. 6.** Surface zeta potential of TFC membranes estimated at different pH (3-10).

392

393 **Table 2.** Atomic composition and the degree of cross-linking of PA layer in the TFC  
394 membranes.

Samples	C1s	O1s	N1s	O/N Ratio	Degree of cross-linking (%)
TP-0	74.83	15.44	9.73	1.59	32.04
TP-5	72.45	16.80	10.75	1.56	34.23
TP-10	76.15	14.47	9.38	1.54	36.09
TP-15	75.44	13.79	10.77	1.28	63.18
TP-20	74.66	14.07	11.27	1.25	66.91

395

396 As surface charge of the PA layer plays an important role in rejection of divalent anions due to  
397 the Donnan effects, surface zeta potential of TFC membranes at varying pH ranges (3-10) were

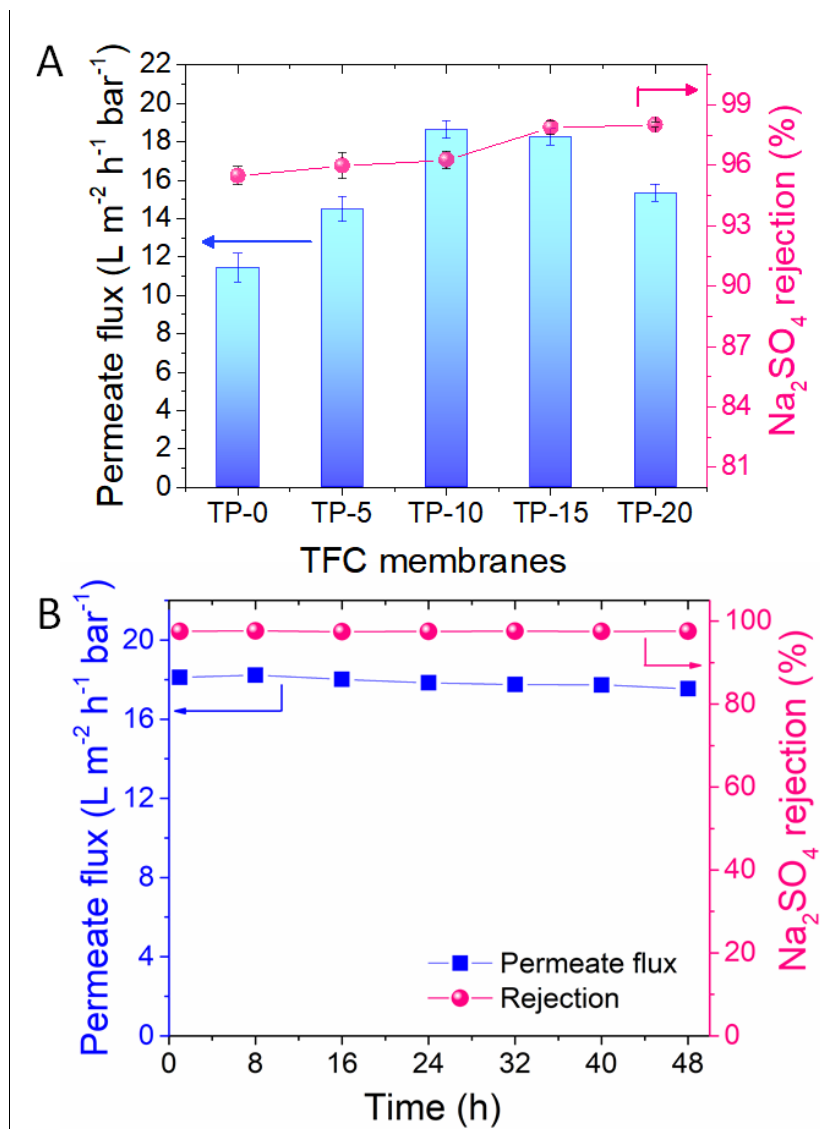
398 measured as shown in Fig. 6 [17]. The TP-0 membrane showed negatively charged surface  
399 across the entire pH range from 3 to 10 and the zeta potential value gradually decreased with  
400 increase of pH value. All TFC membranes revealed negative charges at an isoelectric point due  
401 to the presence of uncross-linked carboxyl groups of the acyl chloride from the IP process [12].  
402 It can be noted that the zeta potential values for PA layers were shifted from negative to positive  
403 with increased number of SWCNT prints. In case of TP-15 membrane, the isoelectric point  
404 (IEP) revealed at pH value of ~5.6 which is significantly increased as compared to the TP-0  
405 membrane, yet it still exhibit negative charges which is in good agreement with other literatures  
406 that PA layer formed on the SWCNTs intermediate layers, favorable IEP value for high  
407 rejection of anions [12, 31]. Additionally, overall zeta potential trend with different amount of  
408 SWCNT prints for the interlayer also well-matched with the degree of cross-linking (%) of PA  
409 layer determined from the XPS analysis (Table 2). The lowest degree of cross-linkage was  
410 obtained from TP-0 membrane (32.04%) which may correspond to the remaining of abundant  
411 uncross-linked carboxyl groups on the PA surface as zeta potential result also demonstrate  
412 significantly lower values across the pH ranges. However, as the SWCNT printing increased  
413 from 5 to 20 cycles on the PES support for TFC membranes, lower negative charge were  
414 exhibited and higher degrees of cross-linkage of PA layers were achieved at 34.23%, 36.09%,  
415 63.18%, and 66.91% for TP-5, TP-10, TP-15 and TP-20, respectively. Such formation of highly  
416 cross-linked PA layer was facilitated by SWCNT interlayer and could potentially be  
417 advantageous for high ion selectivity driven by size sieving effect.

### 418 ***3.4 Impact of SWCNT interlayer on TFC membrane performance***

419 In order to investigate the impact of varying number of SWCNT printings and interlayer  
420 condition on TFC membrane performances, a PA layer was fabricated under optimum IP  
421 condition of (PIP concentration of 0.15 wt% and TMC concentration of 0.1 w/v%) which was

422 obtained from the experimental results indicated in Fig. 4. The NF performance tests were  
423 performed using a divalent salt of  $\text{Na}_2\text{SO}_4$  for testing TFC membranes and water flux and salt  
424 rejection performance results are represented in Fig. 7(A). It can be clearly seen that water flux  
425 and  $\text{Na}_2\text{SO}_4$  rejection of  $11.42 \pm 0.74 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$  and  $95.48 \pm 0.45\%$  is achieved for TP-0  
426 sample and much enhanced performance where water flux of  $18.60 \pm 0.44 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$  and  
427 rejection of  $96.26 \pm 0.42\%$  is achieved for TP-10 membrane. The trend shows that the  
428 membrane performance steadily improved with increasing numbers of SWCNT prints from 0  
429 to 10 cycles. After 10 cycles of SWCNT printing, marginal reduction in water flux appeared at  
430 15 cycles of printings yet the salt rejection rate was further enhanced up to  $97.88 \pm 0.33\%$ .  
431 Particularly, significant enhancement in permeate water flux (increment in water flux of 61%  
432 from TP-0 to TP-10 membrane) was observed for TP-0 to TP-10 membrane, while salt rejection  
433 was also enhanced with increasing numbers of SWCNT printings. Improvement of water flux  
434 at higher printing numbers (between 0 to 10 cycles) could mainly be attributed to the formation  
435 of significantly thinner PA layer (see Fig. 5, reduced from  $123.5 \pm 9.4 \text{ nm}$  to  $56.9 \pm 6.8 \text{ nm}$ ).  
436 Thus, the thinner PA active layer subsequently reduced the water transport resistance and the  
437 porous SWCNT interlayer matrix provide increase in liquid transport channels, and such trend  
438 is in good agreement with other literatures [12, 15, 32]. Additionally, a higher degree of  
439 cross-linking of PA layers (Table 2) formed on the PES substrates containing SWCNT  
440 interlayers (i.e. TP-5 and TP-10), as compared to TP-0 (without SWCNT interlayer), could  
441 enhance the ion selectivity with minimized water permeance hindrance.





442

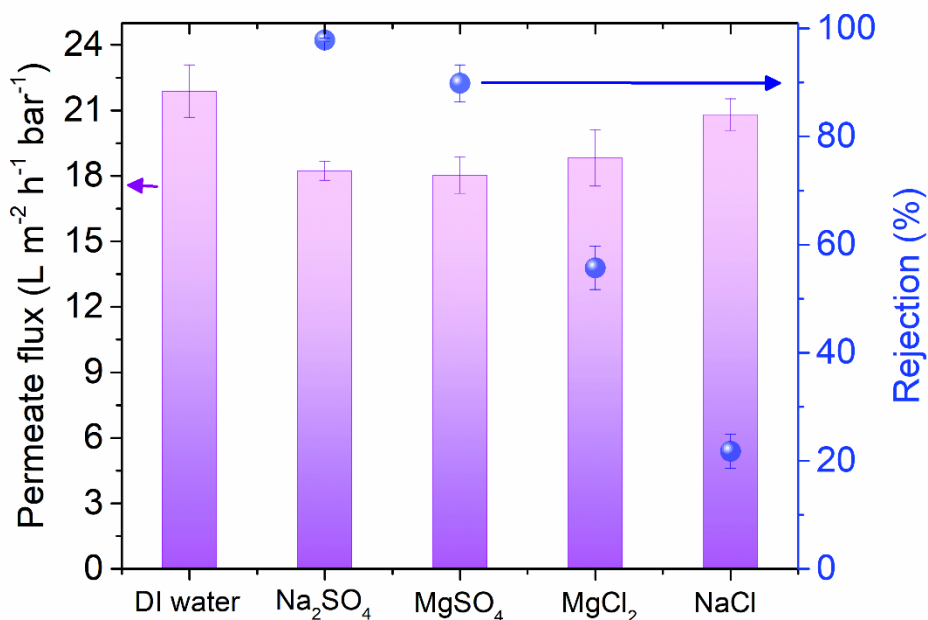
443 **Fig. 7.** (A) Permeate water flux and salt rejection performances of the TFC NF membranes  
 444 fabricated with different numbers of SWCNT prints and (B) long-term performance of the  
 445 TP-15 membrane (feed solution:  $Na_2SO_4$  1,000  $mg L^{-1}$ , applied pressure: 4 bar, and cross-  
 446 flow velocity:  $0.83 cm s^{-1}$ ).

447

448 Meanwhile, TP-20 membrane, exhibited the water flux of  $15.31 \pm 0.43 L m^{-2} h^{-1} bar^{-1}$  revealing  
 449 slight reduction in flux when compared with TP-10 or TP-15 membranes, yet higher than that  
 450 of TP-0 membrane. Moreover, TP-20 membrane exhibited further enhanced salt rejection of

451  $\text{Na}_2\text{SO}_4$  up to  $98.01 \pm 0.14\%$ . Further deposition of SWCNT interlayer on PES MF support  
 452 (e.g. 20 cycles of SWCNT prints) resulted in formation of thinnest PA active layer (41.7 nm)  
 453 among all TFC membranes (Fig. 5). However, this also led to the highest degree of PA layer  
 454 crosslinking (Table 2) which resulted in tightening of the membrane pore size attributing to the  
 455 slightly reduced water permeance [14]. Amongst all prepared TFC membranes with varying  
 456 number of SWCNT printing cycles, P-15 support membrane (15 cycle SWCNT prints)  
 457 provided the best support membrane condition for IP process which resulted in both high water  
 458 flux ( $18.24 \pm 0.43 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$ ) and excellent salt rejection rate compared to other membranes.  
 459 Further experiment using the TP-15 membrane was also conducted to investigate the  
 460 membrane stability under long-term operation. As shown in Fig. 7(B), both water permeability  
 461 and salt rejection performances remained constant during the operation for 48 hours,  
 462 confirming the good mechanical stability of the fabricated TFC membrane.

463

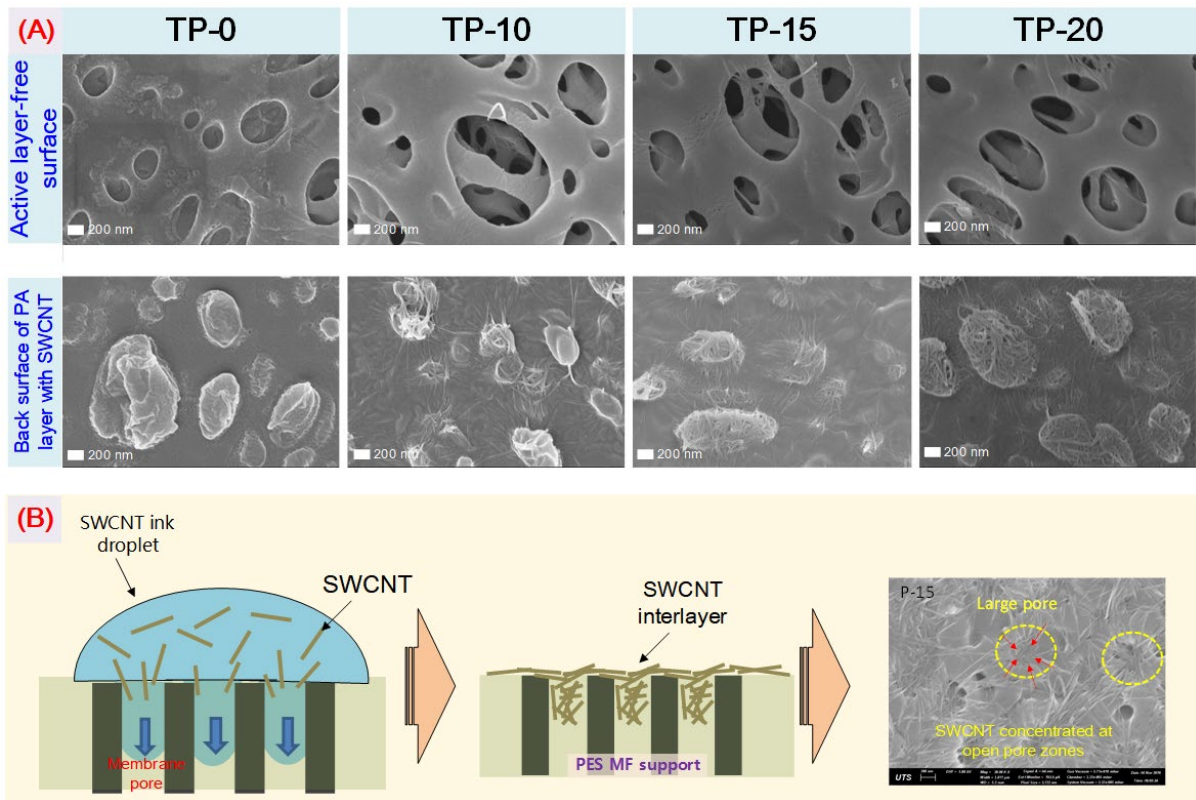


464

465 **Fig. 8.** Permeate water flux and rejection performances of TP-15 TFC NF membrane (15  
466 SWCNT prints) under varied salts as a feed solution ( $1,000 \text{ mg L}^{-1}$   $\text{Na}_2\text{SO}_4$ ,  $\text{MgSO}_4$ ,  $\text{MgCl}_2$   
467 and  $\text{NaCl}$ ) and DI water, applied pressure: 4 bar.

468 The NF separation performance for the TP-15 TFC membrane was further evaluated with  
469 different salts as well as DI water as feed waters and their permeate flux and salts rejection  
470 results can be seen in Fig. 8. It can be note that the rejection rate of salts by TP-15 TFC  
471 membrane showed in the order of  $\text{Na}_2\text{SO}_4$  ( $97.88 \pm 0.33\%$ ),  $\text{MgSO}_4$  ( $89.78 \pm 3.42\%$ ),  $\text{MgCl}_2$   
472 ( $55.71 \pm 4.02\%$ ) and  $\text{NaCl}$  ( $21.76 \pm 3.13\%$ ). The sulfate salts such as  $\text{Na}_2\text{SO}_4$  and  $\text{MgSO}_4$   
473 exhibited much higher rejection rates than that of chloride salts including  $\text{MgCl}_2$  and  $\text{NaCl}$   
474 because the synergistic effect of molecular size sieving and strong Donnan exclusion (IEP  $\approx 5.6$   
475 for TP-15) with the sulfate salts [10, 15, 31]. The TP-15 TFC membrane achieved the pure  
476 water flux (DI water as feed) of  $21.89 \pm 1.20 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$  and when saline solution was used  
477 as feed, lower permeate fluxes were observed for all cases of feed solution containing varying  
478 salts due to the hindrance by osmotic pressure of each salts and concentration polarization.

479



480

481 **Fig. 9.** Morphology changes of PA selective layers formed on varying number of SWCNT  
 482 printings characterized by FE-SEM (A) for active layer (PA or PA with SWCNT)-free  
 483 surface and back surface of PA layer with SWCNT interlayer, and (B) conceptual illustration  
 484 of SWCNT ink drop on PES MF support depositing the SWCNT interlayer.

485

### 486 **3.5 Implication and limitation of SWCNT interlayers utilized via inkjet printing**

487 To further explore the formation of PA active layers as well as their morphology changes on  
 488 different loadings of SWCNT coated via inkjet printing process, active layer (PA alone or PA  
 489 with SWCNT) on the TFC membranes were carefully removed using an adhesive tape. Then  
 490 the morphologies of active layer-free surfaces of PES membrane (active layer removed) and  
 491 the back surfaces of PA without SWCNT (TP-0) and PA with SWCNT (TP-10, TP-15 and TP-  
 492 20) layers were investigated by FE-SEM observation as shown in Fig. 9(A). Numbers of

493 nodular-shaped, non-porous particles appeared on the back surface of PA layer for TP-0  
494 membrane. This is due to the presence of large pores of PES surface, leading to uneven  
495 coverage by PIP aqueous solution allowing the facile penetration of TMC solvent into the  
496 larger pore structures during the IP process, causing the formation of PA particles inside the  
497 micropores of PES support [12, 32]. While, active layer-free surface image of TP-0 membrane  
498 revealed some remainder of the dense PA active layers formed inside the pores which were not  
499 fully detached from the surface of PES support by an adhesive tape. This indicates that the  
500 discontinuous PA layer was formed on the pure PES support. However, other samples which  
501 had SWCNT interlayer such as TP-10, -15 and -20 membranes, where active layers were  
502 composed of PA and SWCNT, revealed the typical surface structure of PES MF membrane  
503 when active layer was completely peeled-off. Interestingly, nodular shaped particles were also  
504 observed on the back surface from the membrane samples (TP-10~20) shown in FE-SEM  
505 images, where those particles were mainly composed of porous SWCNTs bundles. This trend  
506 clearly shows that, with increase of SWCNT printing numbers, the dense PA nodular particles,  
507 on the back surface of PA layer were non-visible when SWCNT prints exceeded 10 cycles (TP-  
508 15 and TP-20). This observation reinforces our claim that PES support membrane pores were  
509 fully covered and occupied with SWCNT matrix on the PES membrane surface, reducing the  
510 surface pore size and smoother surface with interconnected matrix, providing a buffer layer  
511 which facilitates the uniform distribution of PIP monomer in the membrane substrate, leading  
512 to formation of smoother and low-defect PA layer. Also substrate surface tuned by SWCNT  
513 deposition limits the diffusion of the PIP monomer during the IP process, leading to formation  
514 of thinner PA layer with higher degree of cross-linking (Table 1) [12].

515 We also noticed that the back surface structures of support membrane coated with SWCNT  
516 via inkjet printing serve as an interlayer, after the IP process. This new information reveals that  
517 the SWCNTs interlayer structure exhibits a flat-nodular shaped patterns which are slightly

518 different to other literatures which report flat surface on the back side of PA layer with low  
519 roughness and imprinted patterns of SWCNT matrix [12, 32]. In previous studies, CNTs were  
520 mostly coated on a MF support via vacuum filtration method [8, 10-12, 15], or other few studies  
521 used spray coating [32] or brush-painting [31] techniques. These nanomaterial coating  
522 techniques are mainly pressurized or force-driven techniques where most of the CNTs will be  
523 positioned and composed as interconnected matrix on the membrane surface covering the  
524 surface pores. However, as illustrated in Fig. 9(B), SWCNTs deposition via inkjet printing is  
525 sensitive to the surface morphology of microporous support membrane. When a pico-liter of  
526 SWCNTs ink droplet comes in contact with a surface of PES support, ink would first move to  
527 larger and inner pores which have lower capillary force and mass transport resistance. A high  
528 surface tension of SWCNT water based ink ( $\approx 72 \text{ dynes cm}^{-1}$ ) might also affect the water  
529 penetration behaviors. Thus, the SWCNTs will accumulate partially in the area of inner pores  
530 and when the pores sufficiently filled, then SWCNTs layer will fully cover the other regions  
531 on the PES membrane surface. This orderly deposited SWCNTs via inkjet printing resulted in  
532 slightly different patterns of the back surface of PA-SWCNT layers (see Fig. 9(A, B)). Such  
533 unique formation of PA-SWCNT selective layer would possibly aid in binding between the PA  
534 selective layer and PES support layer, forming a mechanically stable SWCNT intermediate  
535 layer between PES support and PA layer, as long-term experiment confirms the stability of  
536 TFC membranes (see Fig. 7(b)). Moreover, SWCNT with short lengths of 1~3  $\mu\text{m}$  was used as  
537 SWCNT ink in this study (in previous studies, SWCNT with size of 5~30  $\mu\text{m}$  were used), and  
538 this could be another reason for the ease in penetration of the SWCNTs into the pores of PES  
539 support. We also attempted to use the SWCNTs sizes of 5~30  $\mu\text{m}$  as an ink, however, easy  
540 blockage of ink nozzle head was observed even at low SWCNT concentration, as nozzle  
541 diameter was only 30  $\mu\text{m}$ . As we used a commercial HP home-office inkjet printer and inkjet  
542 cartridge, the nozzle size of cartridge could not be adjusted and caused the limitation in

543 designing and demonstration while changing other printing parameters. Nevertheless, we  
544 demonstrate the high potential of using inkjet printing technology to coat nanomaterials for  
545 membrane developments and further investigations are needed to develop suitable  
546 nanomaterial inks and printing devices optimization in near future.

### 547 ***3.6 Conclusions***

548 A high performance TFC NF membrane with ultrathin PA active layer was successfully  
549 synthesized by using SWCNTs as an interlayer between the PA active layer and PES MF  
550 membrane support. We first introduced a potential application of inkjet printing technology to  
551 deposit SWCNT ink on PES MF membrane to utilize them as an interlayer. SWCNT ink printed  
552 over 10 cycles efficiently modified the surface morphology of PES MF support membrane by  
553 reducing surface pore size and roughness, thereby achieving a formation of ultrathin PA active  
554 layer (PA layer thickness of TP-15 is ~42 nm). The TFC NF membrane fabricated at an optimal  
555 condition (15 cycle prints of SWCNT ink) exhibited significantly improved membrane  
556 performances including permeate water flux of  $18.24 \pm 0.43 \text{ L m}^{-2} \text{ h}^{-1} \text{ bar}^{-1}$  with a high salt  
557 rejection of  $\text{Na}_2\text{SO}_4$  divalent salts ( $97.88 \pm 0.33\%$ ) as compared to SWCNT-free TFC  
558 membrane. We also demonstrate that inkjet printing technique is an attractive route for  
559 depositing nanomaterials, which is simple and enable rapid deposition with potential scalability  
560 on the membranes surface not only for SWCNT ink, but which could also be applicable for  
561 depositing other nanomaterials. However, some challenges of inkjet printing technology yet  
562 remains to be overcome in future, such as further efforts in developing optimum nanomaterial  
563 inks and development of printing devices specialized for membrane manufacturing.

564

### 565 ***Acknowledgements***

566 We thank the research support of the Australian Research Council (ARC). D.H.S acknowledges  
567 the support of Chancellor's postdoctoral research fellow scheme from UTS.

568

569 **References**

- 570 [1] X. Hao, S. Gao, J. Tian, Y. Sun, F. Cui, C.Y. Tang, Calcium-Carboxyl Intrabridging during  
571 Interfacial Polymerization: A Novel Strategy to Improve Antifouling Performance of Thin  
572 Film Composite Membranes, *Environ Sci Technol*, 53 (2019) 4371-4379.
- 573 [2] K.P. Lee, J. Zheng, G. Bargeman, A.J.B. Kemperman, N.E. Benes, pH stable thin film  
574 composite polyamine nanofiltration membranes by interfacial polymerisation, *Journal of*  
575 *Membrane Science*, 478 (2015) 75-84.
- 576 [3] W. Choi, S. Jeon, S.J. Kwon, H. Park, Y.-I. Park, S.-E. Nam, P.S. Lee, J.S. Lee, J. Choi,  
577 S.J.J.o.M.S. Hong, Thin film composite reverse osmosis membranes prepared via layered  
578 interfacial polymerization, 527 (2017) 121-128.
- 579 [4] A.F. Ismail, M. Padaki, N. Hilal, T. Matsuura, W.J. Lau, Thin film composite membrane  
580 — Recent development and future potential, *Desalination*, 356 (2015) 140-148.
- 581 [5] A.W. Mohammad, Y.H. Teow, W.L. Ang, Y.T. Chung, D.L. Oatley-Radcliffe, N. Hilal,  
582 Nanofiltration membranes review: Recent advances and future prospects, *Desalination*, 356  
583 (2015) 226-254.
- 584 [6] S. Karan, Z. Jiang, A.G. Livingston, Sub-10 nm polyamide nanofilms with ultrafast solvent  
585 transport for molecular separation, *Science*, 348 (2015).
- 586 [7] Y. Liang, C. Li, S. Li, B. Su, M.Z. Hu, X. Gao, C. Gao, Graphene quantum dots (GQDs)-  
587 polyethyleneimine as interlayer for the fabrication of high performance organic solvent  
588 nanofiltration (OSN) membranes, *Chemical Engineering Journal*, 380 (2020).
- 589 [8] M.-B. Wu, Y. Lv, H.-C. Yang, L.-F. Liu, X. Zhang, Z.-K. Xu, Thin film composite  
590 membranes combining carbon nanotube intermediate layer and microfiltration support for high  
591 nanofiltration performances, *Journal of Membrane Science*, 515 (2016) 238-244.
- 592 [9] P. Gorgojo, S. Karan, H.C. Wong, M.F. Jimenez-Solomon, J.T. Cabral, A.G. Livingston,  
593 Ultrathin Polymer Films with Intrinsic Microporosity: Anomalous Solvent Permeation and  
594 High Flux Membranes, *Advanced Functional Materials*, 24 (2014) 4729-4737.
- 595 [10] Y. Zhu, W. Xie, S. Gao, F. Zhang, W. Zhang, Z. Liu, J. Jin, Single-Walled Carbon  
596 Nanotube Film Supported Nanofiltration Membrane with a Nearly 10 nm Thick Polyamide  
597 Selective Layer for High-Flux and High-Rejection Desalination, *Small*, 12 (2016) 5034-5041.
- 598 [11] K. Goh, L. Setiawan, L. Wei, W. Jiang, R. Wang, Y. Chen, Fabrication of novel  
599 functionalized multi-walled carbon nanotube immobilized hollow fiber membranes for  
600 enhanced performance in forward osmosis process, *Journal of Membrane Science*, 446 (2013)  
601 244-254.
- 602 [12] G. Gong, P. Wang, Z. Zhou, Y. Hu, New Insights into the Role of an Interlayer for the  
603 Fabrication of Highly Selective and Permeable Thin-Film Composite Nanofiltration  
604 Membrane, *ACS applied materials & interfaces*, 11 (2019) 7349-7356.
- 605 [13] M. Wu, J. Yuan, H. Wu, Y. Su, H. Yang, X. You, R. Zhang, X. He, N.A. Khan, R. Kasher,  
606 Z. Jiang, Ultrathin nanofiltration membrane with polydopamine-covalent organic framework  
607 interlayer for enhanced permeability and structural stability, *Journal of Membrane Science*,  
608 576 (2019) 131-141.
- 609 [14] J.-J. Wang, H.-C. Yang, M.-B. Wu, X. Zhang, Z.-K. Xu, Nanofiltration membranes with  
610 cellulose nanocrystals as an interlayer for unprecedented performance, *Journal of Materials*  
611 *Chemistry A*, 5 (2017) 16289-16295.



612 [15] Z. Wang, Z. Wang, S. Lin, H. Jin, S. Gao, Y. Zhu, J. Jin, Nanoparticle-templated  
613 nanofiltration membranes for ultrahigh performance desalination, *Nature Communications*, 9  
614 (2018) 2004.

615 [16] W. Choi, S. Jeon, S.J. Kwon, H. Park, Y.-I. Park, S.-E. Nam, P.S. Lee, J.S. Lee, J. Choi,  
616 S. Hong, E.P. Chan, J.-H. Lee, Thin film composite reverse osmosis membranes prepared via  
617 layered interfacial polymerization, *Journal of Membrane Science*, 527 (2017) 121-128.

618 [17] X. Zhang, Y. Lv, H.C. Yang, Y. Du, Z.K. Xu, Polyphenol Coating as an Interlayer for  
619 Thin-Film Composite Membranes with Enhanced Nanofiltration Performance, *ACS applied*  
620 *materials & interfaces*, 8 (2016) 32512-32519.

621 [18] M. Singh, H.M. Haverinen, P. Dhagat, G.E. Jabbour, Inkjet printing-process and its  
622 applications, *Advanced materials*, 22 (2010) 673-685.

623 [19] J.L. Zhuang, D. Ar, X.J. Yu, J.X. Liu, A. Terfort, Patterned deposition of metal-organic  
624 frameworks onto plastic, paper, and textile substrates by inkjet printing of a precursor solution,  
625 *Advanced materials*, 25 (2013) 4631-4635.

626 [20] C.J. Zhang, L. McKeon, M.P. Kremer, S.H. Park, O. Ronan, A. Seral-Ascaso, S. Barwich,  
627 C.O. Coileain, N. McEvoy, H.C. Nerl, B. Anasori, J.N. Coleman, Y. Gogotsi, V. Nicolosi,  
628 Additive-free MXene inks and direct printing of micro-supercapacitors, *Nat Commun*, 10  
629 (2019) 1795.

630 [21] N. Karim, S. Afroj, A. Malandraki, S. Butterworth, C. Beach, M. Rigout, K.S. Novoselov,  
631 A.J. Casson, S.G. Yeates, All inkjet-printed graphene-based conductive patterns for wearable  
632 e-textile applications, *Journal of Materials Chemistry C*, 5 (2017) 11640-11648.

633 [22] M. Zeng, Y. Zhang, Colloidal nanoparticle inks for printing functional devices: emerging  
634 trends and future prospects, *Journal of Materials Chemistry A*, 7 (2019) 23301-23336.

635 [23] B.J. de Gans, P.C. Duineveld, U.S. Schubert, Inkjet Printing of Polymers: State of the Art  
636 and Future Developments, *Advanced materials*, 16 (2004) 203-213.

637 [24] J. Li, F. Rossignol, J. Macdonald, Inkjet printing for biosensor fabrication: combining  
638 chemistry and technology for advanced manufacturing, *Lab Chip*, 15 (2015) 2538-2558.

639 [25] S. Kholghi Eshkalak, A. Chinnappan, W.A.D.M. Jayathilaka, M. Khatibzadeh, E.  
640 Kowsari, S. Ramakrishna, A review on inkjet printing of CNT composites for smart  
641 applications, *Applied Materials Today*, 9 (2017) 372-386.

642 [26] E.B. Secor, P.L. Prabhurashi, K. Puntambekar, M.L. Geier, M.C. Hersam, Inkjet  
643 Printing of High Conductivity, Flexible Graphene Patterns, *J Phys Chem Lett*, 4 (2013) 1347-  
644 1351.

645 [27] C. Wang, M.J. Park, D.H. Seo, H.K. Shon, Inkjet printing of graphene oxide and dopamine  
646 on nanofiltration membranes for improved anti-fouling properties and chlorine resistance,  
647 *Separation and Purification Technology*, 254 (2021).

648 [28] M. Fathizadeh, H.N. Tien, K. Khivantsev, J.-T. Chen, M. Yu, Printing ultrathin graphene  
649 oxide nanofiltration membranes for water purification, *J. Mater. Chem. A*, 5 (2017) 20860-  
650 20866.

651 [29] M.J. Park, S. Phuntsho, T. He, G.M. Nisola, L.D. Tijing, X.-M. Li, G. Chen, W.-J. Chung,  
652 H.K. Shon, Graphene oxide incorporated polysulfone substrate for the fabrication of flat-sheet  
653 thin-film composite forward osmosis membranes, *Journal of Membrane Science*, 493 (2015)  
654 496-507.

655 [30] M.J. Park, R.R. Gonzales, A. Abdel-Wahab, S. Phuntsho, H.K. Shon, Hydrophilic  
656 polyvinyl alcohol coating on hydrophobic electrospun nanofiber membrane for high  
657 performance thin film composite forward osmosis membrane, *Desalination*, 426 (2018) 50-59.

658 [31] S. Gao, Y. Zhu, Y. Gong, Z. Wang, W. Fang, J. Jin, Ultrathin Polyamide Nanofiltration  
659 Membrane Fabricated on Brush-Painted Single-Walled Carbon Nanotube Network Support for  
660 Ion Sieving, *ACS Nano*, 13 (2019) 5278-5290.

661 [32] Z. Zhou, Y. Hu, C. Boo, Z. Liu, J. Li, L. Deng, X. An, High-Performance Thin-Film  
662 Composite Membrane with an Ultrathin Spray-Coated Carbon Nanotube Interlayer,  
663 Environmental Science & Technology Letters, 5 (2018) 243-248.

664