

Dynamic Behaviour of Ballasted Railway Track with Special Reference to Transition Zones

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Doctor of Philosophy

under the supervision of Dr. Sanjay Nimbalkar and Prof. Hadi Khabbaz

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CERTIFICATE OF ORIGINAL AUTHORSHIP

I, *Piyush Punetha* declare that this thesis, is submitted in fulfilment of the requirements for the award of *Doctor of Philosophy*, in the *School of Civil and Environmental Engineering (Faculty of Engineering and Information Technology, FEIT)* at the University of Technology Sydney.

This thesis is wholly my own work unless otherwise referenced or acknowledged. In addition, I certify that all information sources and literature used are indicated in the thesis.

This document has not been submitted for qualifications at any other academic institution.

This research is supported by the Australian Government Research Training Program.

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Dedicated to My Parents

मेरे माता-पिता को समर्पित

ABSTRACT

The poor performance of transition zones in railway tracks has long been a subject of concern for the rail infrastructure managers. These zones are the discontinuities along a railway line that are highly susceptible to differential settlement due to an abrupt variation in the support conditions over a short span. Consequently, these regions require frequent maintenance to ensure adequate levels of passenger safety and comfort. The rapid deterioration of track geometry in these zones is primarily ascribed to limited understanding of the underlying mechanism and scarcity of adequate tools to assess the severity of the potential issue. Therefore, a comprehensive evaluation of their behaviour is paramount to improve the design and ensure adequate service quality. With this objective, a novel methodology is developed which can predict the dynamic behaviour of the transition zones under train-induced repeated loading and assess the suitability of different countermeasures in improving the track performance.

To this end, an integrated approach is first developed by combining track loading, resiliency, and settlement models to evaluate the transient and irrecoverable response of the substructure layers of a standard ballasted railway track. The track substructure layers (ballast, subballast, and subgrade) in this model are simulated as an array of lumped masses that are connected by elastic springs and viscous dampers. The irrecoverable response of the track is evaluated using the empirical settlement models for substructure layers. The accuracy of the method is validated by comparing the predicted results against the field investigation data reported in the literature. Subsequently, the practical applicability of the aforementioned method under different traffic loading and soil conditions is improved by replacing the empirical approach with a mechanistic approach, in which, plastic slider elements are employed to predict the inelastic deformation in the substructure layers. To validate the approach, the predicted results are compared with the in-situ measurements reported in the literature. A good agreement between the predicted results and the field data verified the accuracy of the novel geotechnical rheological track model. A parametric investigation is conducted which highlights the significant influence of axle load, train speed, and granular layer thickness, on the accumulated settlement in the track layers.

The novel geotechnical rheological track model is then applied to an open-track bridge transition by incorporating the inhomogeneous support conditions associated with the critical zone and the adequacy of different countermeasures to mitigate the differential track settlements is examined. The approach is successfully validated with published field data and predictions from the finite element (FE) analysis. The results revealed that an increase in axle load exacerbates the track geometry degradation problem. The results also show that the performance of transition zones with weak subgrade can be improved by increasing the granular layer thickness. Interpretation of the predicted differential settlement for different countermeasures exemplified the practical significance of the proposed methodology.

Subsequently, the influence of principal stress rotation (PSR) experienced by the soil elements during a train passage is incorporated in the geotechnical rheological model. The results revealed that PSR causes significant cumulative deformation in the substructure layers, and disregarding it in the analysis leads to inaccurate predictions. Finally, the adequacy of using three-dimensional (3D) cellular geoinclusions to improve the performance of critical zones is investigated using the proposed methodology and FE analyses. A novel semi-empirical model is first developed to evaluate the magnitude of improvement provided by these inclusions under the 3D stress state. The proposed model is successfully validated against the experimental data. This model is then incorporated in the geotechnical rheological model and the effectiveness of 3D geoinclusions in improving the performance of an open track-bridge transition is investigated. The results show that the geoinclusions significantly reduce the magnitude of differential settlement and therefore, have a huge potential to be used in the transition zones to improve track performance.

The essential contribution of this thesis is that it provides reliable, practical, and adaptable techniques to assist the practising railway engineers in analysing the performance of various sections of ballasted railway tracks, identifying the most effective method to improve the track performance, planning the maintenance operations, and improving the design. The developed techniques are available in the form of MATLAB codes, which can readily be converted into an application that can be used by railway engineers. Nonetheless, the outcomes of this study have huge potential to influence the real-world

design implications of track transition zones. The approaches developed in this study are original, simple yet elegant, and can enhance, if not fully replace, present complex track modelling procedures for anticipating the behaviour of critical zones and adopting appropriate mitigation strategies.

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TABLE OF CONTENTS

CERTIFI	CATE	E OF ORIGINAL AUTHORSHIPi
ABSTRA	.CT	iii
ACKNOWLEDGEMENTSvi		
LIST OF	PUBI	LICATIONS RELATED TO THIS RESEARCHvii
STATEM	IENT	OF CONTRIBUTION OF AUTHORSix
TABLE C	OF CC	NTENTSxiv
LIST OF	FIGU	RESxviii
LIST OF	TABI	LESxxvi
LIST OF	NOT	ATIONSxxvii
CHAPTE	R 1 II	NTRODUCTION1
	1.1	Background1
	1.2	Research Significance
	1.3	Research Objectives
	1.4	Thesis Organisation7
CHAPTE	2R 2 L	ITERATURE REVIEW10
	2.1	Overview10
	2.2	Railway Track: Basic Concepts10
	2.3	Existing Approaches to Analyse Track Behaviour
	2.4	Critical Zones in Railway Tracks
	2.5	Effect of Principal Stress Rotation
	2.6	Discussion41
CHAPTE	2R 3	(PART-A) ANALYTICAL EVALUATION OF A BALLASTED
	I	RAILWAY TRACK RESPONSE UNDER REPEATED TRAIN LOADS
	3.1	General45
	3.2	Methodology for Prediction of Track Settlement
	3.3	Model Validation
	3.4	Results and Discussion
	3.5	Advantages, Limitations and Future Scope67
	3.6	Concluding Remarks

CHAPTER 3 (PART-B) I	REPLACING THE EMPIRICAL APPROACH WITH A
MECHANIS	TIC APPROACH TO EVALUATE TRACK RESPONSE70
3.7 General	
3.8 Background	
3.9 Model Desc	ription72
3.10 Model Valid	lation90
3.11 Results and	Discussion95
3.12 Advantages	, Limitations and Future Scope101
3.13 Concluding	Remarks
CHAPTER 4 PREDICTIO	N OF THE BEHAVIOUR OF TRANSITION ZONES IN
RAILWAY '	FRACKS USING A GEOTECHNICAL RHEOLOGICAL
MODEL	
4.1 General	
4.2 Background	
4.3 Methodolog	y
4.4 Model Valid	lation111
4.5 Results and	Discussion117
4.6 Importance	of Considering Material Plasticity in Track Transition
Models.	
4.7 Practical Re	levance and Potential Applications
4.8 Advantages	, Limitations and Future Scope126
4.9 Concluding	Remarks
CHAPTER 5 IMPACT O	F PRINCIPAL STRESS ROTATION ON BALLASTED
RAILWAY 7	TRACK RESPONSE129
5.1 General	
5.2 Background	
5.3 Geotechnica	Il Rheological Track Model131
5.4 Results and	Discussion
5.5 Application	to Transition Zones147
5.6 Practical R	elevance, Potential Applications, Limitations, and Future
Scope	
5.7 Concluding	Remarks

CHAPTER 6 (PART-A) IMPROVING THE PERFORMANCE OF RAILWAY
TRACKS USING THREE-DIMENSIONAL CELLULAR
GEOINCLUSIONS
6.1 General
6.2 Beneficial Role of Cellular Geoinclusions in Railways157
6.3 Additional Confinement
6.4 Irrecoverable Deformations
6.5 Field Performance of Geocells
6.6 Evaluation of Additional Confinement for 3D Geoinclusions under
General Stress State
6.7 Concluding Remarks
CHAPTER 6 (PART-B) ASSESSING THE EFFECTIVENESS OF GEOINCLUSION
IN IMPROVING THE PERFORMANCE OF TRANSITION ZONE
USING GEOTECHNICAL RHEOLOGICAL MODEL199
6.8 General
6.9 Response Prediction for Reinforced Track
6.10 Validation of Methodology
6.11 Results and Discussion
6.12 Application to Transition Zones
6.13 Economic and Environmental Aspects of 3D Cellular Geoinclusion
Reinforcement
6.14 Limitations and Future Scope
6.15 Concluding Remarks
CHAPTER 7 NUMERICAL MODELLING OF BALLASTED RAILWAY TRACKS
WITH SPECIAL REFERENCE TO TRANSITION ZONES220
7.1 General
7.2 3D FE Modelling of Ballasted Railway Track: Case Study of High-Speed
Track in Sweden
7.3 FE Modelling of Ballasted Railway Track: Case Study of a Bridge
Approach along Amtrak's North East Corridor224
7.4 3D FE Modelling of Transition Zones
7.5 Assessing the Adequacy of Geocells in Improving the Performance of an
Open Track-Bridge Transition Using 3D FE Modelling232

CHAPTER 8	CONCLUSIONS
8.1	Computational Methodology for Evaluating the Transient and Long-
	Term Performance of Railway Tracks
8.2	Improving the Accuracy of the Computational Methodology by
	Incorporating the Effect of Principal Stress Rotation
8.3	Performance Improvement of Ballasted Rail Tracks Using 3D Cellular
	Geoinclusions
8.4	Numerical Modelling of the Ballasted Rail Tracks244
8.5	Recommendations for Future Work
REFERENCE	S247
APPENDICES	5

LIST OF FIGURES

Figure 1.1 Ballasted railway track
Figure 1.2 Open track-bridge transition [Imagery © 2022 Google, Imagery © 2022 CNES
/ Airbus, Maxar Technologies, Map data © 2022; Image: © 2022 Google]5
Figure 2.1 Ballasted railway track structure
Figure 2.2 Impact loads generated near the bridge approach
Figure 2.3 Young's modulus and resilient modulus for soil
Figure 2.4 Flowchart for the design of conventional ballasted track
Figure 2.5 Examples of (a) 2D plane-strain; (b) 2.5D; (c) 3D FE model of ballasted
railway tracks
Figure 2.6 (a) Beam on elastic foundation model; (b) Vehicle-track coupled model 30
Figure 2.7 Transition zone between an open track and stiff structure such as a bridge or
underpass
Figure 3.1 (a) Configuration of the Thalys high-speed train; (b) calculation of track
deflection at time t_1 ; (c) calculation of track deflection at time t_2 ; (d) final rail seat load-
time history
Figure 3.2 Three-degree-of-freedom mass-spring-dashpot (MSD) model of track51
Figure 3.3 Overlapping along longitudinal direction in (a) ballast; (b) subballast; (c)
subgrade; transverse direction in (d) ballast; (e) subballast; (f) subgrade
Figure 3.4 Effective portion of substructure layers considered in analysis
Figure 3.5 Comparison of vertical displacement and acceleration time histories predicted
using the present method with field results reported by Takemiya & Bian (2005)60
Figure 3.6 Comparison of model predictions with the field results reported by Gräbe &
Shaw (2010)
Figure 3.7 Comparison of model predictions with results reported by Priest et al. (2010):
(a) resilient displacement for 26 t axle load coal wagons; (b) resilient displacement at
different depth below the sleeper; (c) resilient displacement for 20 t axle load coal wagons
(d) vertical stress at 800 mm below sleeper bottom
Figure 3.8 Comparison of model predictions with field results reported by Mishra et al.
(2014a)
Figure 3.9 Variation of average irrecoverable strain in substructure layers with (a)
thickness; (b) resilient modulus
Figure 3.10 Deflection profile during the passage of train wheels

Figure 3.11 (a) Wheel load measured between adjacent sleepers (Mishra et al. 2017); (b) wheel load measured at sleeper location; (c) sleeper reaction force or rail seat load73
Figure 3.12 Simplified geotechnical rheological model of the ballasted railway track.75
Figure 3.13 Effective region of the track substructure layers considered in the analysis

Figure 3.18 Flowchart to predict the track response under train-induced repeated loads

Figure 3.25 Variation of subgrade settlement with tonnage at different granular layer
thickness
Figure 3.26 Variation of settlement accumulated after a cumulative tonnage of 25 MGT,
with granular layer thickness, for (a) subgrade; (b) granular layers101
Figure 4.1 (a) Open track-bridge transition zone; (b) transition zone after multiple train
passages104
Figure 4.2 Rheological model of an open track-bridge transition zone
Figure 4.3 Effective acting region of track layers considered in the analysis at (a) softer
side; (b) stiffer side110
Figure 4.4 3D FE model of the open track-bridge transition zone112
Figure 4.5 Comparison of results predicted using the proposed method and FEM: (a)
variation of vertical displacement at ballast top with distance along the track; (b) variation
of vertical deformation with time for ballast, subballast and subgrade114
Figure 4.6 Comparison of predicted transient vertical displacement at sections S3 and S4
with the field data reported by Paixão et al. (2014a)115
Figure 4.7 Comparison of predicted settlement in substructure layers with the field data
reported by Mishra et al. (2017)116
Figure 4.8 Variation of settlement at different axle loads with (a) distance; (b) tonnage
at different locations
Figure 4.9 Variation of settlement with distance at different ballast layer thickness 119
Figure 4.10 Distribution of vertical stress with depth at 3.5 m from the bridge for different
ballast layer thickness
Figure 4.11 Variation of settlement with distance at different subballast layer thickness
Figure 4.12 Distribution of vertical stress with depth at 3.5 m from the bridge for different
subballast layer thickness
Figure 4.13 Variation of vertical displacement at ballast top with distance along the track
and depth for the two cases: when slider elements are considered (viscoelastic-plastic)
and when slider elements are ignored (viscoelastic)123
Figure 4.14 Variation of settlement with distance when ballast modulus in the improved
zone is increased from 200 MPa – 600 MPa124
Figure 4.15 Variation of settlement with distance when subballast modulus in the
improved zone is increased from 115 MPa – 345 MPa

Figure 4.16 Variation of settlement with distance when subgrade friction angle in the
improved zone is increased from $31^\circ - 40^\circ$
Figure 5.1 Yield surface in the characteristic stress space
Figure 5.2 Comparison of response predicted using the present model with the
experimental data reported by Cai et al. (2015) for subgrade soil under repeated loading
conditions: (a) cyclic stress waveforms corresponding to one load cycle; accumulation of
vertical strain with number of load cycles for (b) various $CVSR$ at $CSSR = 0$; different
CSSR at (c) CVSR = 0.15; (d) CVSR = 0.25
Figure 5.3 Comparison of the response predicted using the present model with the
experimental data reported by Wijewickreme & Vaid (2008): (a) variation of stress ratio
with deviatoric strain; (b) variation of volumetric strain with deviatoric strain
Figure 5.4 Comparison of the response predicted using the present model with the
experimental data reported by Yang (2013)138
Figure 5.5 Comparison of the response predicted using the present model with the
experimental data reported by Wu et al. (2020)139
Figure 5.6 Influence of constitutive parameters on the accumulation of vertical strain: (a)
effect of $s_{1\alpha}$; (b) effect of $s_{2\alpha}$
Figure 5.7 Stress variation experienced by the substructure layers below a sleeper due to
a moving wheel load
Figure 5.8 (a) Stress-time history for a soil element located 1,200 mm below the sleeper
bottom during a train passage; (b) variation of PSR angle with depth; variation of
deviatoric stress with PSR angle at (c) 100 mm; (d) 350 mm; (e) 1,200 mm below sleeper
bottom
Figure 5.9 Effect of principal stress rotation on cumulative settlement
Figure 5.10 Influence of axle load on the cumulative settlement with and without the
inclusion of PSR145
Figure 5.11 Influence of granular layer thickness on the cumulative settlement with and
without the inclusion of PSR: (a) for variation in ballast thickness; (b) for variation in
subballast thickness
Figure 5.12 Effect of considering PSR on the selection of granular layer thickness147
Figure 5.13 Geotechnical rheological model for an open track-bridge transition 148
Figure 5.14 Comparison of predicted vertical track displacement with the field data
reported by Paixão et al. (2014b) at 0.9 m and 14.7 m from the bridge149

Figure 5.15 Effect of axle load on the behaviour of transition zone with and without the
inclusion of PSR151
Figure 5.16 Effect of granular layer thickness on the behaviour of transition zone with
and without considering the PSR: (a) for variation in ballast thickness; (b) for variation
in subballast thickness
Figure 5.17 (a) Variation of settlement along the track length when subgrade friction
angle in the improved zone is increased from $36^{\circ} - 40^{\circ}$; (b) accumulation of settlement
with tonnage at different sections of the transition zone153
Figure 6.1 Key problems governing the instability of ballasted railway tracks
Figure 6.2 The vertical stress distribution in the subgrade for the ballasted track (a)
without geocell; (b) geocell near the top of ballast layer; (c) geocell near the bottom of
the ballast layer
Figure 6.3 Comparison of predicted and experimental results from previous studies.171
Figure 6.4 Installation of geocells at the railway bridge ends on the south coastline of
New South Wales, Australia
Figure 6.5 Track longitudinal profile showing the location of the geocells and
superstructure elements (pads, sleepers)174
Figure 6.6 Typical Fourier amplitude spectrum for field accelerometer data recorded at
the region with ordinary sleeper and stiffness transfer sleeper
Figure 6.7 Fourier amplitude spectrum for field accelerometer data recorded in the
geocell reinforced section and at the bridge end176
Figure 6.8 Fourier amplitude spectrum for field accelerometer data recorded at the bridge
and the ballast in geocell reinforced section
Figure 6.9 Variation in track geometry data along the rail bridge after the construction of
the transition zone
Figure 6.10 The behaviour of railway embankment under train traffic-induced loads: (a)
without cellular geoinclusion; (b) with cellular geoinclusion
Figure 6.11 Deformation of cellular geoinclusion under different stress states: (a)
general; (b) plane-strain; (c) axisymmetric182
Figure 6.12 Variation of additional confinement ratio (ACR) with (a) mobilised friction
angle ($\varphi'_{\rm m}$) and dilatancy rate ($D_{\rm r}$); (b) dilatancy rate ($D_{\rm r}$) for $b = 0.1, 0.2$ and 0.3; (c) $b/b_{\rm ps}$
ratio and $\varphi'_{\rm m}$

Figure 6.13 (a) Tensile load-strain curves for five different types of cellular geoinclusion
materials; (b) variation of normalised additional confinement ($k_{\sigma,2}$ and $k_{\sigma,3}$) with the
number of load cycles (N)192
Figure 6.14 Comparison of the additional confinement computed using the present model
with the experimental data under (a) axisymmetric condition; (b) plane-strain condition
Figure 6.15 Differential settlement in an open track-bridge transition and its potential
mitigation using 3D cellular geoinclusion
Figure 6.16 Comparison of track settlement computed using the present method with
results from FE analyses conducted by Satyal et al. (2018)
Figure 6.17 Comparison of results computed using the present method with experimental
data reported by Banerjee et al. (2020a)
Figure 6.18 (a) Load versus strain curves for five geoinclusion materials obtained from
tension tests; (b) accumulation of settlement with tonnage for tracks reinforced with
cellular inclusions manufactured using different materials
Figure 6.19 Variation of additional confinement with tonnage for tracks reinforced with
3D artificial inclusions manufactured using different materials207
Figure 6.20 Influence of opening or pocket size on track response for 3D cellular
inclusions manufactured using (a) HDPE; (b) woven coir geotextile; (c) nonwoven PP
geotextile
Figure 6.21 Influence of axle load on settlement for track reinforced with different
cellular inclusion types
Figure 6.22 (a) Equivalence of stresses in planar geosynthetic to additional confining
pressure in soil; (b) comparison of settlement accumulated in the unreinforced track and
track reinforced using planar and 3D geosynthetics
Figure 6.23 Geotechnical rheological model of a typical open track-bridge transition with
3D cellular geosynthetic reinforcement
Figure 6.24 Variation of settlement along the length for unreinforced and reinforced track
Figure 6.25 Influence of subgrade strength on the effectiveness of artificial inclusions
manufactured using: (a) HDPE; (b) woven coir geotextile; (c) nonwoven PP geotextile

Figure 6.26 Variation of settlement along the track length when 3D cellular inclusion is
provided at different positions within the track
Figure 6.27 Reduction in subgrade settlement when cellular geoinclusion is provided at
the top of the subgrade and when subballast thickness is increased from 0.15 m to 0.3 m .
Figure 7.1 3D FE model of the high-speed railway track in Sweden
Figure 7.2 Procedure used to calculate the moving wheel loads
Figure 7.3 Comparison of FE model results with the field data at different train speed
Figure 7.4 3D FE model of the ballasted track near the bridge approach
Figure 7.5 Comparison of model predictions with the field data reported by Boler et al.
(2018a)
Figure 7.6 Comparison of predicted vertical layer deformation with the field data
reported by Boler et al. (2018a)
Figure 7.7 Variation of vertical displacement with depth at different axle loads230
Figure 7.8 Variation of displacement along the length of the track at different train speeds
Figure 7.9 Variation of vertical displacement along the track length for different subgrade
types
Figure 7.10 Details of the placement of geocells in the transition zone
Figure 7.11 Variation of vertical displacement along the track length when geocell is
provided at different locations
Figure 7.12 Variation of vertical displacement along the track length when geocell with
different stiffness are provided in the subgrade
Figure 7.13 Formation of sleeper-ballast gaps near the bridge approach
Figure 7.14 Comparison of predicted results with the experimental data reported by
Satyal et al. (2018)
Figure A.1 Effective region of (a) ballast; (b) subballast; (c) subgrade layers
Figure C.1 Transfer of train-induced load from superstructure to the substructure layers
Figure E.1 Effective region of ballast in stiffer side for non-overlapped case

Figure F.1 (a) Train configuration; track response at time instant (b) t_1 ; (c) t_2 ; (d) t_3 ;
variation of rail seat load with time at (e) m^{th} sleeper; (f) n^{th} sleeper during one complete
train passage
Figure H.1 Yield surface during loading and unloading
Figure I.1 Stress profile of 3D cellular geoinclusion under general stress state275

LIST OF TABLES

Table 2.1 Empirical equations to calculate the impact factor
Table 2.2 Empirical models for the prediction of resilient modulus
Table 2.3 Summary of the existing modelling techniques for critical zones
Table 3.1 Parameters a' , b_g and m^* for different subgrade soils
Table 3.2 Parameters used for evaluation of track response 59
Table 3.3 Comparison of results reported by Gräbe et al. (2005) with model predictions
Table 3.4 Constitutive parameters for the plastic slider element for granular layers84
Table 3.5 Model parameters for the plastic slider element for subgrade soil
Table 3.6 Parameters for the simulation of viscoelasto-plastic track response
Table 4.1 Model parameters for evaluation of track response
Table 4.2 Constitutive parameters for granular layers 116
Table 4.3 Constitutive parameters for subgrade
Table 5.1 Constitutive parameters for plastic slider element for subgrade
Table 5.2 Input parameters for geotechnical rheological model (Zhai et al. 2004; Paixão
et al. 2014b; Li et al. 2016; Li et al. 2018)141
Table 6.1 Model parameters to predict permanent deformation
Table 6.2 Input parameters for the parametric study
Table 6.3 Parameters for predicting the additional confinement under the plane-strain and
axisymmetric conditions195
Table 6.4 Input parameters used in the validation
Table 6.5 Input parameters for parametric study
Table 7.1 Material parameters used for the simulation of the track response
Table 7.2 Material parameters used for the simulation of the response of track near the
bridge approach
Table 7.3 Material parameters used in the analysis
Table 7.4 Constitutive parameters for substructure layers 229
Table 7.5 Constitutive parameters for substructure layers (Satyal et al. 2018)

LIST OF NOTATIONS

Latin Symbols:

- $A_{\rm b}$ Equivalent area of ballast at a particular depth (m²)
- $A_{\rm b}^{\rm s}$ Equivalent shear area of ballast (m²)
- $A_{\rm d}$ Maximum normal operating cant deficiency angle (rad)
- Af Fourier amplitude
- $A_{\rm g}$ Equivalent area of subgrade at a particular depth (m²)
- A_g^s Equivalent shear area of subgrade (m²)
- $A_{\rm s}$ Equivalent area of subballast at a particular depth (m²)
- A_s^s Equivalent shear area of subballast (m²)
- $A_{\rm y}$ Angle of lateral ramp discontinuity (rad)
- a, a^r Equivalent radius of sleeper-ballast contact area in softer and stiffer side (m)
 - a^* Empirical coefficient
 - a' Material parameter for subgrade
 - a_h Cyclic hardening parameter
- a_{o}, b_{o} Locomotive and track maintenance factors
 - $a_{\rm t}$ Number of wheels considered
 - b Intermediate principal stress ratio
- b^*, b' Empirical coefficients
 - $b_{\rm g}$ Material parameter for subgrade
 - $b_{\rm ps}$ Intermediate principal stress ratio at plane-strain condition
 - $b_{\rm sl}$ Sleeper width (m)
 - $b_{\rm t}$ Track width (m)
 - C Coefficient in Japanese standard
 - c Cohesion (N/m²)

 $c_{\rm b}, c_{\rm s}, c_{\rm g}$ Viscous damping coefficients for ballast, subballast and subgrade (Ns/m)

 c_b^r Viscous damping coefficient for ballast in the stiffer side (Ns/m)

 c_b^s, c_s^s, c_g^s Shear damping coefficients for ballast, subballast and subgrade (Ns/m)

 $c_{\rm b}^{s,r}$ Shear damping coefficient for ballast in the stiffer side (Ns/m)

- D Dilatancy
- $D_{\rm g}$ Diameter of geoinclusion opening (m)

- $D_{\rm p}$ Plastic dilatancy
- $D_{\rm r}$ Dilatancy rate
- $D_{\rm w}$ Train wheel diameter (m)
- $d_{\rm s}$ Diameter of soil specimen in triaxial test (m)
- $dF_{b,n}^r$ Force increment acting on ballast layer in the stiffer side (N)

dF_{g,n}, dF_{s,n}, dF_{b,n} Force increment acting on subgrade, subballast and ballast (N)

- $d\hat{p}$ Hydrostatic stress increment in characteristic stress space
- dp_i Image mean effective stress increment (N/m²)
- $d\hat{q}$ Deviatoric stress increment in characteristic stress space
- dt Time step (s)
- *E* Young's modulus of infill (N/m^2)
- $E_{\rm b}, E_{\rm s}, E_{\rm g}$ Resilient modulus of ballast, subballast and subgrade (N/m²)
 - $E_{\rm b}^r$ Resilient modulus of ballast in the stiffer side (N/m²)
 - $E_{\rm i}$ Initial Young's modulus (N/m²)
 - $E_{\rm m}$ Young's modulus of geoinclusion (N/m²)
 - $E_{\rm R}$ Resilient modulus (N/m²)
 - $E_{\rm r}$ Young's modulus of rail (N/m²)
 - $E_{\rm sec}$ Secant Young's modulus (N/m²)
 - e_{0} , e_{0} Current and initial void ratio
 - $e_{\rm c}$ Void ratio on critical state line at the current mean effective stress
 - F Frequency (Hz)
 - $F_{\rm wr}$ Wheel-rail contact force (N)
 - f_c, f_r, f_t Current, reference and transitional surfaces
 - $f_{\rm g}, f_{\rm s}, f_{\rm b}$ Yield surface for subgrade, subballast and ballast
 - G Wheel-rail contact constant $(m/N^{2/3})$
 - g Acceleration due to gravity (m/s^2)
 - $g_{\rm p}$ Potential function
 - $g_{\rm t}$ Centre-to-centre distance between the rails (m)
 - H Hardening parameter in Nor-sand model
 - $H_{\rm L}$ Lateral load (N)
 - $H_{\rm m}$ Influence height of planar geosynthetic (m)

 H_{mean} Mean lateral load (N)

- $H_{\rm w}$ Crosswind force (N)
 - h Vertical distance from rail top to centre of gravity of train (m)
- $h_{\rm b}, h_{\rm s}, h_{\rm g}$ Ballast, subballast and subgrade thickness (m)
 - $h_{\rm b}^r$ Ballast thickness in the stiffer side (m)
- h_{bL}, h_{sL}, h_{gL} Overlap height in ballast, subballast and subgrade along longitudinal direction (m)
 - $h_{\rm bt}, h_{\rm st}, h_{\rm gt}$ Overlap height in ballast, subballast and subgrade along transverse direction (m)
 - $h_{\rm d}$ Cant or superelevation deficiency (m)
 - h_{eb}, h_{es} Equivalent thickness of ballast and subballast layers (m)
 - $h_{\rm gl}$ Granular layer thickness (m)
 - h_{i} Thickness of i^{th} substructure layer (m)
 - h_{se} Superelevation (m)
 - $I_{\rm r}$ Moment of inertia of rail (m⁴)
 - i_1, i_2 Empirical parameters for calculating dynamic amplification factor
 - K Coefficient representing the internal friction
- K_1, K_2, K_3, K_4 Fitting parameters that depend on type and physical state of the soil
 - K_j Track stiffness at joint (N/m)
 - K_y Effective lateral rail stiffness per wheel (N/m)
 - k Track modulus (N/m²)
 - k^r Track modulus for stiffer side of the transition (N/m²)
- k^*, k_1^*, k_2^*, k_3^* Empirical parameters
 - k_0 Lateral earth pressure coefficient
 - k_1, k_2, k_3, k_4 Empirical parameters
- $k_1^b, k_2^b, k_3^b, k_4^b$ Empirical parameters for calculating ballast deformation
- $k_1^s, k_2^s, k_3^s, k_4^s$ Empirical parameters for calculating subballast deformation
 - $k_{\rm b}, k_{\rm s}, k_{\rm g}$ Stiffness of ballast, subballast and subgrade (N/m)

 $k_{\rm b}^r$ Stiffness of ballast in the stiffer side (N/m)

- $k_{\rm b}^{\rm s}, k_{\rm s}^{\rm s}, k_{\rm g}^{\rm s}$ Shear stiffness of ballast, subballast and subgrade (N/m)
 - $k_{\rm b}^{s,r}$ Shear stiffness of ballast in the stiffer side (N/m)

- k_c Ratio of circumferential strain to the radial strain in the geocell
- k_p Stiffness of rail pad (N/m)
- k_p^r Rail pad stiffness in the stiffer side (N/m)
- $k_{\sigma,2}, k_{\sigma,3}$ Normalised additional confinement
 - L Characteristic length (m)
 - $l_{\rm c}$ Distance between rail top and centre of gravity of train (m)
 - $l_{\rm e}$ Effective length of sleeper (m)
 - $l_{\rm g}$ Gauge width (m)
 - $l_{\rm sl}$ Sleeper length (m)
 - $l_{\rm w}$ Distance between centre of rails and the resultant wind force (m)
 - M Critical stress ratio
 - \widehat{M} Critical stress ratio in characteristic stress space
 - $M_{\rm i}$ Critical stress ratio corresponding to image state
 - $M_{
 m itc}$ Critical stress ratio corresponding to the image state for triaxial compression
 - $M_{\rm m}$ Mobilised modulus of geocell (N/m)
 - $M_{\rm p}$ Peak stress ratio
 - $M_{\rm t}$ Tensile stiffness of the geocell (N/m)
 - $M_{\rm tc}$ Critical stress ratio under triaxial compression
 - $M_{\rm u}$ Effective lateral unsprung mass per axle (kg)
 - $M_{\rm v}$ Effective lateral rail mass per wheel (kg)
 - m, n Empirical coefficients
 - m^* Material parameter for subgrade
- $m_{\rm b}, m_{\rm s}, m_{\rm g}$ Vibrating mass of ballast, subballast and subgrade (kg)
 - $m_{\rm b}^r$ Vibrating mass of ballast in the stiffer side (kg)
 - N Number of load cycles
 - $N_{\rm d}$ Number of days
 - $N_{\rm lim}$ Number of load cycles required to reach stable zone
 - N_{limit} Number of load repetitions required to reach the resilient state
 - $N_{\rm v}$ Volumetric coupling coefficient
 - $P_{\rm a}$ Atmospheric pressure (N/m²)

- *p* Mean effective stress (N/m^2)
- p_i Image mean effective stress (N/m²)
- p_{ic} , p_{im} Hardening parameters
 - \hat{p}_{xg} Intersection of potential function with \hat{p} axis
- $\hat{p}_{xt}, \hat{p}_{xc}, \hat{p}_{xr}$ Intersection of transitional, current and reference surfaces with \hat{p} axis
 - Q, Q_a Static wheel and axle load (N)
 - $Q_{\rm d}$ Design wheel load (N)
 - Q_{dy} Dynamic component of load (N)
 - Q_{qs} Quasi-static wheel load (N)
 - $Q_{r,n}$ Vertical rail seat load at n^{th} sleeper (N)
 - $Q_{\rm t}$ Tensile load (N)
 - Q_{tv} Total vertical wheel load (N)
 - q Deviatoric stress (N/m^2)
 - \hat{q} and \hat{p} Deviatoric and hydrostatic stress invariants in the characteristic stress space
 - R Parameter that controls the magnitude of plastic volumetric strain increment
 - $R_{\rm c}$ Radius of curvature of track (m)
 - R_{i} Parameter that controls the magnitude of plastic strain accumulation
 - $R_{\rm s}$ Stress ratio
 - $R_{\rm w}$ Nominal radius of the wheel (m)
 - r Spacing ratio
 - S Sleeper spacing (m)
 - $s_{1\alpha}$, $s_{2\alpha}$ Constitutive parameters to account for the effects of principal stress rotation
 - s_{b} , s_{s} Settlement of ballast and subballast (m)
 - s_{g}, s_{gl} Settlement of subgrade and granular layers (m)
 - s_{ii} Deviatoric stress tensor
 - s_{t} Settlement of track substructure (m)
 - s_v^{r} Vertical resilient deformation (m)
 - T Cumulative tonnage (kg)
 - T_n^{s} Average shear stress vector
 - T_x , T_y Tensile stresses in planar geosynthetic along x and y directions (N/m)

- *t* Time instant (s)
- $t_{\rm g}$ Thickness of geoinclusion (m)
- $t_{\rm u}$ Factor that depends on the upper confidence limit
- V Train speed (m/s)
- V_m Maximum normal operating speed (m/s)
- $W_{\rm u}$ Unsprung weight at one wheel (N)
- $W_{\rm vd}$ Vertical deformation (m)
- $W_{\rm wr}$ Deformation at the wheel-rail contact point (m)
 - w Vertical track deflection (m)
- $W_{\rm b}$ Vertical displacement at ballast top (m)
- $W_{\rm bm}$ Mean value of track displacement in stiffer zone (m)
 - $W_{\rm t}$ Vertical track displacement (m)
 - x Distance along longitudinal direction (m)
- x_n^{j} Distance of n^{th} sleeper from j^{th} wheel (m)
- Z Plastic softening parameter
- z Depth (m)

$$\begin{split} z_{\mathrm{b,n}}, \dot{z}_{\mathrm{b,n}}, \ddot{z}_{\mathrm{b,n}} & \text{Displacement, velocity and acceleration of ballast below n^{th} sleeper \\ & z_{\mathrm{b,n}}^{p}, \dot{z}_{\mathrm{b,n}}^{p} & \text{Plastic displacement and velocity of ballast below n^{th} sleeper \\ & z_{\mathrm{s,n}}, \dot{z}_{\mathrm{s,n}}, \ddot{z}_{\mathrm{s,n}} & \text{Displacement, velocity and acceleration of subballast below n^{th} sleeper \\ & z_{\mathrm{s,n}}^{p}, \dot{z}_{\mathrm{s,n}}^{p} & \text{Plastic displacement and velocity of subballast below n^{th} sleeper \\ & z_{\mathrm{s,n}}^{p}, \dot{z}_{\mathrm{s,n}}^{p} & \text{Plastic displacement and velocity of subballast below n^{th} sleeper \\ & z_{\mathrm{g,n}}, \dot{z}_{\mathrm{g,n}}, \ddot{z}_{\mathrm{g,n}} & \text{Displacement, velocity and acceleration of subgrade below n^{th} sleeper \\ & z_{\mathrm{g,n}}^{p}, \dot{z}_{\mathrm{g,n}}^{p} & \text{Plastic displacement and velocity of subgrade below n^{th} sleeper \\ & z_{\mathrm{g,n}}^{p}, \dot{z}_{\mathrm{g,n}}^{p} & \text{Plastic displacement and velocity of subgrade below n^{th} sleeper \\ & z_{\mathrm{g,n}}^{p}, \dot{z}_{\mathrm{g,n}}^{p} & \text{Plastic displacement and velocity of subgrade below n^{th} sleeper \\ & z_{\mathrm{g,n}}^{p}, \dot{z}_{\mathrm{g,n}}^{p} & \text{Plastic displacement and velocity of subgrade below n^{th} sleeper \\ & z_{\mathrm{g,n}}^{p}, \dot{z}_{\mathrm{g,n}}^{p} & \text{Plastic displacement and velocity of subgrade below n^{th} sleeper \\ & z_{\mathrm{g,n}}^{p}, z_{\mathrm{g,n}}^{p} & \text{Viscoelastic displacement in subgrade, subballast and ballast (m) \\ & z_{\mathrm{g,n}}^{p}, z_{\mathrm{g,n}}^{p}, z_{\mathrm{g,n}}^{p}, z_{\mathrm{g,n}}^{p} & z_{\mathrm{g,n}}^{p}, z_{\mathrm{g,n}}^{p},$$

Greek Symbols:

- α Stress distribution angle for ballast (°)
- α^* Empirical parameter
- α' Coefficient relating track irregularities, train suspension and speed
- α^r Stress distribution angle for ballast in the stiffer side (°)
- α_0 Reference stress distribution angle in ballast (°)
- $\alpha_{\rm m}$ Bonding coefficient for planar geosynthetic

- α_{v} Angle between major principal stress direction and vertical (°)
- β Stress distribution angle for subballast (°)
- β' Coefficient accounting for the movement of train along a curve
- β_0 Reference stress distribution angle in subballast (°)
- Γ Critical void ratio at p = 1 kPa
- $\hat{\Gamma}$, \hat{N} Void ratio of critical state line and normal compression line at $\hat{p}=1$ kPa
 - γ Stress distribution angle for subgrade (°)
 - γ' Coefficient that depends on speed and design of train, and track condition
 - $\Delta \sigma$ Increase in stress (N/m²)
- $\Delta \sigma'_2$, $\Delta \sigma'_3$ Effective additional confining stress in the direction of σ'_2 and σ'_3 (N/m²)
 - $\Delta \sigma_3$ Additional confining stress in the direction of σ_3 (N/m²)
 - $\Delta \sigma_x$, $\Delta \sigma_y$ Additional confining pressure along x and y directions (N/m²)

 $d\boldsymbol{\varepsilon}_{ij}^{p}, \boldsymbol{\varepsilon}_{v}^{p}$ Plastic strain increment and cumulative plastic volumetric strain

 $d\varepsilon_{\rm v}, d\varepsilon_{\rm q}$ Volumetric and deviatoric strain increments

- $d\varepsilon_v^p, d\varepsilon_q^p$ Plastic volumetric and deviatoric strain increments
 - $d\varepsilon_z^p$ Plastic strain increment in vertical direction
 - δ_{ij} Kronecker delta
 - δ_t Factor that depends on the track condition

 $\varepsilon_0/\varepsilon_r, \rho_p, \beta_p$ Fitting parameters

- $\varepsilon_1, \varepsilon_2, \varepsilon_3$ Major, intermediate and minor principal strains
- $\varepsilon_1^e, \varepsilon_2^e, \varepsilon_3^e$ Resilient components of major, intermediate and minor principal strains
- $\varepsilon_1^{p}, \varepsilon_2^{p}, \varepsilon_3^{p}$ Plastic components of major, intermediate and minor principal strains
 - $\varepsilon_{1,1}^{p}$ Plastic axial strain after the first load cycle
 - ε_{a} Axial strain
 - ε_{a}^{p} Accumulated plastic axial strain

 $\varepsilon_{\rm b}^{p}, \varepsilon_{\rm s}^{p}, \varepsilon_{\rm g}^{p}$ Cumulative plastic strain in ballast, subballast and subgrade

- $\varepsilon_{\rm c}$ Circumferential strain
- ε_{q} Deviatoric strain
- ε_r Radial strain
- $\varepsilon_{\rm t}$ Tensile strain

 $\varepsilon_x, \varepsilon_y$ Strain along x and y directions

 $\varepsilon_x^m, \varepsilon_y^m$ Strains in geosynthetic in x and y directions

 ε_z^p Cumulative plastic strain in vertical direction

 η Stress ratio

- $\hat{\eta}$ Stress ratio in characteristic stress space
- $\eta_{\rm v}$ Factor that depends on the speed of vehicle

 θ Bulk stress (N/m²)

 $\theta_1 + \theta_2$ Total dip angle of the rail joint (rad)

J Tensorial invariant

 Λ_s , Λ_g Scalars

 λ , κ Slope of critical state line and swelling line in e-ln p space

 $v_{\rm b}$, $v_{\rm s}$, $v_{\rm g}$ Poisson's ratio of ballast, subballast and subgrade

- $v_{\rm b}^r$ Poisson's ratio of ballast in the stiffer side
- v_i Poisson's ratio of infill
- $v_{\rm m}$ Poisson's ratio of geoinclusion material
- ξ , A Dimensionless material parameters
- $\rho_{\rm b}, \rho_{\rm s}, \rho_{\rm g}$ Density of ballast, subballast and subgrade (kg/m³)
 - $\rho_{\rm b}^r$ Density of ballast in the stiffer side (kg/m³)

 $\sigma_1, \sigma_2, \sigma_3$ Major, intermediate and minor principal stresses (N/m²)

 σ_{bb}^{r} Vertical stress at the bottom of substructure layer in the stiffer side (N/m²)

 $\sigma_{\rm C,2}, \sigma_{\rm C,3}$ Circumferential stresses in the direction of σ'_2 and σ'_3 (N/m²)

 $\sigma_{\rm c}$ Confining pressure in triaxial tests (N/m²)

 $\sigma'_{\rm c}$ Effective confining pressure (N/m²)

- $\sigma_{\rm cyc}$ Cyclic deviator stress (N/m²)
 - $\sigma_{\rm d}$ Deviator stress (N/m²)
- $\sigma'_{\rm d}$ Effective deviatoric stress (N/m²)
- σ_{di} Deviator stress at which slope of E_R versus σ_d curve changes (N/m²)
- σ_{g} Compressive strength of the soil (N/m²)
- σ_{ii} Stress tensor
- $\widehat{\boldsymbol{\sigma}}_{ij}$ Characteristic stress tensor

 $\sigma_{\rm i}$ Principal stress (N/m²)

 $\sigma_{\rm oct}$ Octahedral normal stress (N/m²)

 $\sigma_{\rm ref}$ Reference stress (N/m²)

- σ_{sb} , σ_{sg} , σ_{go} Vertical stresses at the sleeper-ballast, ballast-subballast, subballastsubgrade interfaces and bottom of subgrade layer (N/m²)
 - $\sigma_{\rm v}$ Vertical stress (N/m²)
 - σ'_x , σ'_y , σ'_z Effective stresses along *x*, *y* and *z* directions (N/m²)
 - $\tau_{\rm cyc}$ Cyclic shear stress amplitude (N/m²)
 - $\tau_{\rm oct}$ Octahedral shear stress (N/m²)
 - φ Friction angle (°)
 - $\varphi_{\rm c}, \varphi_{\rm e}$ Critical state friction angles under triaxial compression and extension (°)
 - φ_d Dynamic amplification factor
 - $\varphi'_{\rm m}$ Mobilised friction angle (°)
 - χ_i, χ_{tc} Dilatancy parameter corresponding to image state and triaxial compression
 - ψ State parameter
 - $\Psi_{\rm d}$ Dilation angle (°)
 - Ψ_i Image state parameter
 - $\Psi_{\rm m}$ Mobilised dilation angle (°)

Abbreviations:

- 2D Two-dimensional
- 2.5D Two and a half dimensional
 - 3D Three-dimensional
- ACR Additional confinement ratio
- AREA American Railway Engineering Association
- ARTC Australian Rail Track Corporation
- BEM Boundary element method
- BoEF Beam on elastic foundation
- CBM Cement bound mixture
- CBR California Bearing Ratio
- CG Coir geotextile

- CSL Critical state line
- CSSR Cyclic shear stress ratio
- CVSR Cyclic vertical stress ratio
- DEM Discrete element method
- FDM Finite difference method
- FEM Finite element method
 - GB Geocell reinforced ballast
 - GG Geocell reinforced subgrade
 - GS Geocell reinforced subballast
- HDPE High-density polyethylene
- HMA Hot-mix asphalt
- LVDT Linear variable displacement transformer
- MDD Multi-depth deflectometers
- MGT Million gross tonnes
- MSD Mass-spring-dashpot
- NCL Normal compression line
- ORE Office for Research and Experiments
 - PE Polyethylene
 - PP Polypropylene
- PSR Principal stress rotation
- RAP Recycled asphalt pavement
 - SS Silica sand
- UGM Unbound granular material
 - UR Unreinforced
 - US United States
- WMATA Washington Metropolitan Area Transit Authority