

Article **Multi-Object Tracking with mmWave Radar: A Review**

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Abstract: The boundaries of tracking and sensing solutions are continuously being pushed. A ¹ stimulation in this field over recent years is exploiting the properties of millimeter wave (mmWave) 2 radar to achieve simultaneous tracking and sensing of multiple objects. This paper aims to provide a ³ critical analysis of the current literature surrounding multi-object tracking and sensing with short- ⁴ range mmWave radar. There is significant literature available regarding single-object tracking using ⁵ mmWave radar, demonstrating the maturity of single-object tracking systems. However, innovative ⁶ research and advancements are also needed in the field of mmWave radar multi-object tracking, ⁷ specifically with respect to uniquely identifying multiple target tracks across an interrupted field of 8 view. In this article, we aim to provide an overview of the latest progress in multi-target tracking. In ⁹ particular, an attempt to phrase the problem space is made by firstly defining a typical multi-object 10 tracking architecture. We then highlight the areas for potential advancements. These areas include 11 sensor fusion, micro-Doppler feature analysis, specialized and generalized activity recognition, gait, 12 tagging and shape profile. Potential multi-object tracking advancements are reviewed and compared 13 with respect to adaptability, performance, accuracy and specificity. Although the majority of the 14 literature reviewed has a focus on human targets, most of the methodologies can be applied to targets 15 consisting of different profiles and characteristics to that of humans. Lastly, future research directions ¹⁶ are also discussed to shed light on research opportunities and potential approaches in the open **research areas.** 18 and 1

Keywords: mmWave, tracking, sensing, multi-object, micro-Doppler, sensor fusion, activity recogni- ¹⁹ tion $\frac{1}{2}$

1. Introduction 21

Millimeter wave (mmWave) radars have been widely studied over recent years for 22 multi-object tracking and sensing. The potential and motivation for mmWave radars in $\frac{23}{2}$ this field is primarily driven by the micro-Doppler information that can be extrapolated. $_{24}$ Micro-Doppler generally refers to the Doppler information generated by movements of $\frac{25}{25}$ individual parts of a particular target [\[1\]](#page-18-0). The micro-Doppler features can be exploited to $\frac{26}{5}$ determine characteristics of multiple targets for tracking and sensing purposes. The identified characteristics can ultimately be translated into sub-millimeter individual movements $\frac{28}{28}$ of the targets. This is attributed to the high sensitivity of mmWave radars empowered by 29 their extremely short wavelength. $\frac{30}{20}$

The research and techniques available for achieving robust and reliable multi-object $_31$ tracking and sensing, specifically with mmWave radar, are yet to be consolidated into 32 a unified architecture. Complications, such as harsh signal propagation environments, ₃₃ make the task of multi-object tracking and sensing quite difficult [\[2\]](#page-18-1). However, it should $\frac{34}{4}$ be highlighted that tracking and sensing, unspecific to mmWave, is not a new concept ³⁵ in regards to radio in general. This concept has been proven successful in other types 36 of radios, such as impulse radio ultra-wide band (IR-UWB) [\[3\]](#page-18-2). Therefore, the findings $\frac{37}{2}$ from multi-object tracking and sensing with alternate types of radios can be assessed for 38 potential applications of similar techniques to mmWave radars.

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MmWave radars can be found in continuous and discontinuous multi-object tracking $\frac{40}{40}$ literature. Continuous tracking refers to the ability to track multiple targets in an environment only whilst it is in the current field of view of the radar. Discontinuous tracking on 42 the other hand is an extension on continuous tracking, whereby the targets can be tracked 43 whilst in the current field of view and also correlated to a previous track if it re-appears $\frac{44}{4}$ in the future field of view of the radar. To clarify the difference between the two types of 45 tracking, Fig. [1](#page-1-0) is provided; an individual, who is currently not in the field of view of the ⁴⁶ radar, performing the following sequence of events: $\frac{47}{47}$

- 1. Moving into the radar's field of view $\frac{48}{48}$
- 2. Leaving the radar's field of view 49
- 3. Moving back into the radar's field of view $50₅₀$

In the described scenario, a solution that is capable of continuous tracking is one $\frac{51}{12}$ that is capable of detecting and tracking multiple individuals in both event 1 and event 3. ₅₂ However, a continuous tracking solution would not be capable of correlating individuals ⁵³ that have been tracked in event 3 with their previous tracks in event 1. On the other hand, a solution that is capable of discontinuous tracking is one that is capable of detecting and 55 tracking individuals in both event 1 and 3, as well as recognizing if the same individual is $\frac{56}{10}$ being tracked across the two events. Thus, a discontinuous tracking solution is one that $\frac{57}{2}$ can correlate and track multiple targets across a discontinuous sequence of events.

A sophisticated combination of tracking and sensing in multi-object scenarios are 59 capable of reliably discontinuously tracking, and have found a number of applications. A 60 new level of security and surveillance systems could potentially be achieved by a mmWave 61 tracking and sensing system to expose and detect threats or concerns that cannot easily 62 be identified in vision-based security systems. It is also achieved without compromising 63 individual privacy. Furthermore, a mmWave multi-object tracking and sensing system 64 could also be adapted to provide a means of mass patient monitoring in the health care 65 industry. Passive and respectful monitoring of patients with a system of this nature could 666 provide a means of continuous monitoring of metrics that would usually require a nurse 67 to manually measure. This, in turn, could lead to earlier insight and awareness of patient ϵ complications. Lastly, a mmWave multi-object tracking and sensing solution can also $\overline{}$ provide a means of an affordable wide-scale generalized analytical and auditing platform σ that can monitor fine-grain people movement and activities within public spaces, such as $\frac{1}{71}$ shopping centers, parks, etc. This could lead to better optimization and utilization of space $\frac{72}{2}$

Figure 2. mmWave tracking architecture block diagram.

layout, particularly in a space where congestion occurs or where specific behaviors are $\frac{1}{2}$ exhibited by individuals when given environmental events occur.

The major contributions of this paper are to provide an overview of the literature 75 surrounding multi-object tracking with mmWave radar systems, highlighting key advanced $\frac{1}{76}$ technologies and hinting future research opportunities. We first present a typical general- η ized mmWave multi-object tracking architecture. Then, we provide a detailed review and $\frac{1}{78}$ comparison of potential advancements that can contribute to further developing the multiobject tracking architecture. Future research opportunities are then discussed to enhance $\frac{80}{100}$ and evolve mmWave multi-object tracking. The context of mmWave radar in this paper $\frac{81}{10}$ specifically relates to short-range applications, both indoors and outdoors. Furthermore, az the intended usage of mmWave radar in this paper is to focus on multi-object tracking of $\frac{1}{8}$ targets traveling at low speeds that are within natural human capability. The methodologies ⁸⁴ and models explored and presented in this paper are not specifically intended to be applied ⁸⁵ to targets traveling at speeds greater than general human motion, such as automotive $\frac{1}{100}$ α targets. The state of the state of

2. Typical Tracking System Architecture 888 and 888

An overview of how multi-object tracking with mmWave can be modeled architec- ⁸⁹ turally from data collection through to tracked target information is illustrated in figure [2.](#page-2-0) \Box The intention of the architecture model depicted in figure [2](#page-2-0) is to provide a foundation to $\frac{91}{12}$ compare and contrast mmWave tracking research, both continuous and discontinuous in ⁹² $\frac{1}{3}$ fashion.

In order to help understand the events that take place to successfully perform discontinuous multi-object tracking with mmWave, the system can be illustrated as a series ⁹⁵ of five chained components. These five components and the sequence in which they are $\frac{1}{96}$ invoked is illustrated in figure [2.](#page-2-0) The generalized aim of the system is to comprehend the $\frac{97}{2}$ influence multiple targets simultaneously have on radar chirps. This signal disturbance translates to information being exploited to initiate or resume a maintained track on an object whilst it is in the radars field of view. The system should ultimately produce a $_{100}$ stream of uniquely identifiable objects along with their corresponding tracking context. 101 The overall system architecture and sequence of components is a well established pattern in $_{102}$ radar tracking literature. The uniqueness of a mmWave tracking system is ultimately held 103 in the implementation of the system components and the mechanisms that are employed $_{104}$ to characterize the tracked objects. The remainder of this section will explore and describe 105 the purpose of each stage illustrated in the generalized architecture shown in figure [2.](#page-2-0) 106

2.1. Radar Architecture 107

The radar architecture of a typical tracking system consists of the components required $_{108}$ to ultimately collect the data describing the observed environment. This usually involves 109 the hardware utilized, the antenna configuration, and the signal configuration employed. 110 Over the last couple of years, single board general-purpose mmWave radars have become ₁₁₁ readily available as off the shelf products. However, prior to this hardware advancement 112

Figure 3. Signal chirp components.

mmWave radar hardware architectures were primarily designed for their specific industrial 113 or research application. Such an architecture is demonstrated in the research performed ¹¹⁴ by [\[4\]](#page-18-3). The authors of [4] implement a frequency-modulated continuous-wave (FMCW) 115 module with a custom designed data acquisition and intermediate frequency (IF) digitizer 116 and signal amplifier. The hardware implementation details of the acquisition board used in 117 the research presented in $[4]$ are lacking. As a result, it can be difficult to obtain consistent $\frac{118}{118}$ results across research due to hardware implementation differences. ¹¹⁹

The advancement and availability of single board multi-purpose mmWave radars has ¹²⁰ been promising in ensuring consistency across research in the regard of radar hardware ₁₂₁ implementation. This in turn ensures the primary focus of the research remains on the $_{122}$ intended research challenge being addressed and not questioned by any discrepancies that 123 might be present in the radar hardware implementation. The most commonly used off $_{124}$ the shelf mmWave radars are Texas Instrument's (TI) family of industrial and automotive 125 mmWave radar sensors. The TI mmWave radar sensors have gained popularity in academia ¹²⁶ due to their reliability and plethora of support.

There are a number of considerations to be made when determining the antenna 128 configuration to employ for a mmWave radar multi-object tracking system. Specifically, ¹²⁹ an acknowledgment should be made regarding the components that contribute to the 130 instability and non-ideal nature of the transmitted signal [\[5\]](#page-18-4). A multiple-input multipleoutput (MIMO) antenna array is the most commonly utilized antenna configuration in 132 radar systems. This is primarily due to its spatial diversity characteristics, ultimately 133 resulting in a more superior detection performance, compared to traditional directional 134 or phased-array antenna configurations $[6]$ [\[7\]](#page-18-6). A study conducted in [7] demonstrates $\frac{135}{135}$ statistically the performance advantages of MIMO systems in comparison to alternate 136 antenna models. The study presented in $[7]$ highlights the ability to exploit the spatial 137 diversity of a MIMO system to ultimately overcome target fading in radar applications. ¹³⁸ One of the most important characteristics that dictates the dimensionality of the measured 139 data is the antenna array's vertical and/or horizontal placement. In order to simultaneously $_{140}$ obtain 3-dimensional real-world coordinate data points for detected objects, the antenna ¹⁴¹ array must have both horizontally and vertically placed arrays. The literature discussed in $_{142}$ this paper, unless otherwise noted, assumes an antenna configuration that only has either $\frac{143}{143}$ horizontal or vertical placement.

Lastly, the final component to consider when discussing the radar architecture for an 145 mmWave multi-object tracking system is the transmit (TX) signal characteristics. Specif- ¹⁴⁶ ically, the linear change in frequency of a single tone over time, referred to as the signal $_{147}$ chirp. The contract of the con

The signal components encapsulated and described by the chirp are illustrated in $_{149}$ figure [3.](#page-3-0) The signal chirp in an mmWave radar system indirectly impacts the measurability $_{150}$ and resolution of range and velocity $[8]$.

$$
\mathbf{R}_{\mathbf{max}} = \frac{\mathbf{IF}_{\mathbf{max}}c}{2S} \tag{1}
$$

Figure 4. Typical FMCW radar system.

The equation illustrated in [\(1\)](#page-3-1) demonstrates the relationship between the signal chirp $_{152}$ slope and the maximum possible measurable range (**Rmax**). In equation [\(1\)](#page-3-1), **IFmax** refers to ¹⁵³ the maximum IF supported by the mmWave radar hardware, *c* refers to the speed of light 154 $(3 \times 10^8 m/s)$ and *S* corresponds to the frequency slope of the signal illustrated in figure [3.](#page-3-0) 155

$$
\mathbf{R}_{\text{res}} = \frac{c}{2B} \tag{2}
$$

The equation shown in (2) highlights the indirect correlation between the chirp sweep $_{156}$ bandwidth and the maximum resolution of the measurable range (**Rres**). In equation [\(2\)](#page-4-0), *B* ¹⁵⁷ corresponds to the sweep bandwidth, also illustrated in figure [3.](#page-3-0) 158

$$
V_{max} = \frac{\lambda}{4C_t}
$$
 (3)

The maximum radial velocity that can be measured without ambiguity (**Vmax**) is calculated using equation [\(3\)](#page-4-1). In equation (3), λ refers to the wavelength of the TX signal and C_t corresponds to the total chirp time, which can also be seen in figure [3.](#page-3-0)

$$
V_{res} = \frac{\lambda}{2C_t C_n} \tag{4}
$$

Lastly, the unambiguous velocity resolution can be calculated using equation (4) , $_{159}$ where C_n is the number of chirps in a single frame. A frame simply refers to a sequence of 160 chirps, followed by a delay before beginning the next frame. The frame can be considered $_{161}$ as the window of observation that is operated on. 162

2.2. Position and Velocity Estimation 163

Once the appropriate radar architecture has been decided, a strategy for calculating $_{164}$ the estimated position and velocity of reflected points should be determined. It should be 165 acknowledged that the position of a reflected point is comprised of the range and azimuth 166 of the reflected point, with respect to the radar. Consider a typical FMCW radar system 167 illustrated in figure [4.](#page-4-3) In figure [4,](#page-4-3) the synthesizer is responsible for generating the chirp TX_{168} signal, the reflections of the transmitted chirp are captured by the receiver and mixed with 169 the TX signal to ultimately produce the IF signal. 170

Assuming the transmitted chirp (C_{Tx}) is sinusoidal, the waveform that is transmitted $\frac{1}{171}$ and the corresponding received (RX) signal (C_{Rx}) can be described as equations [\(5\)](#page-4-4) and 172 [\(6\)](#page-4-5) respectively. Furthermore, the IF signal (**IF**) of the transmitted and received sinusoidal ¹⁷³ chirps is described as equation (7) .

$$
C_{Tx} = \sin(\omega_{Tx}t + \phi_{Tx})
$$
\n(5)

$$
C_{Rx} = \sin(\omega_{Rx}t + \phi_{Rx})
$$
 (6)

$$
\mathbf{IF} = \sin((\omega_{\text{Tx}} - \omega_{\text{Rx}})t + (\phi_{\text{Tx}} - \phi_{\text{Rx}}))
$$
\n(7)

where ω_{Tx} and ω_{Rx} are the instantaneous frequencies of the TX and RX signals respectively, $\frac{175}{175}$ and ϕ_{Tx} and ϕ_{Rx} are the phase of the TX and RX signals respectively.

In an environment where multiple objects are presently causing an influence on the $\frac{177}{177}$ IF signal, a fast Fourier transformation (FFT) of the IF signal can be performed to express 178 the signal so that the signal can then be expressed in the frequency domain. As a result, 179 each frequency peak evident in this form can be assumed to be associated with a particular $_{180}$ detected object. The distance of each detected object, denoted as R_x , can then be calculated $\frac{181}{181}$ using the given frequency present in the IF signal, expressed in equation (8) .

$$
R_x = \frac{f_{IF}c}{2S} \tag{8}
$$

where f_{IF} is the frequency of the detected object in the IF signal.

The velocity of a detected object can ultimately be obtained by analyzing the phase $_{184}$ difference between consecutive chirps corresponding to the same object. In the situation 185 where multiple objects are present at the same distance from the radar, the phase difference 186 of the FFT of the IF signal will have multiple objects encoded within it. As a result, a second 187 FFT should be performed, labeled as the Doppler-FFT, which will ultimately reveal peaks $_{188}$ of phase differences corresponding to the number of detected objects. The velocity of a ¹⁸⁹ given object (V_x) revealed using a Doppler-FFT can then be evaluated with equation (9) . 190

$$
V_x = \frac{\lambda \omega_x}{4\pi C_t} \tag{9}
$$

where ω_x is the phase difference of the detected object in the IF signal.

The last component of interest that can be derived from the reflected signal is the $_{192}$ horizontal angle, relative to radar, of the object that caused the signal reflection. This is 193 termed as the Angle of Arrival (AoA). The AoA can fundamentally be derived from the 194 phase change in a detected object's peak in the Doppler-FFT or range-FFT. This phase ¹⁹⁵ change is ultimately caused by a change in the distance of the detected object. Using ¹⁹⁶ this observation, the AoA of an object can be determined by acknowledging that a single 197 object's distance from two RX antennas will differentiate and therefore distinctly have a ¹⁹⁸ phase difference. For two RX antennas, the AoA of a reflected signal (*θx*) can be expressed ¹⁹⁹ as equation [\(10\)](#page-5-2). In an architecture where multiple RX antenna pairs are presented. The $_{200}$ final AoA can be derived by determining the average AoA result from all RX antenna pairs. $_{201}$

$$
\theta_x = \sin^{-1}\left(\frac{\lambda \omega_x}{2\pi d}\right) \tag{10}
$$

where d is the distance between the two RX antennas. 202

The ultimate outcome of this stage in an mmWave tracking system is to obtain the $_{203}$ necessary information to construct a 2 dimensional plot that illustrates the reflection points $_{204}$ in the environment. Estimating the range, angle and velocity of each reflection point is $_{205}$ sufficient enough to construct a plot of this nature. The most common way to illustrate this $_{206}$ information is to plot it in a point cloud graph. 207

2.3. Association and Tracking 208

The association and tracking component of a mmWave tracking system should funda- ²⁰⁹ mentally consume the information that illustrates reflection points, deduced in section [2.2](#page-4-7) 210 of this paper. Using this information, usually in point cloud format, the process illustrated $_{211}$ in figure [5](#page-6-0) highlights the typical stages involved in achieving a set of continuously tracked $_{212}$ objects from the obtained point cloud data. ²¹³

The first processing stage illustrated in figure 5 , static noise removal, refers to a process $_{214}$ whereby any points in the point cloud data that are present in both frame N_x and N_{x-1} 215 are deemed as static noise and removed from frame N_x . This noise removal technique is $_{216}$ typical in current mmWave multi-object tracking systems. One key assumption that is 217 made in this noise removal attempt is that targets of interest must always be moving to $_{218}$ be tracked. Therefore, any targets that are mostly stationary, such as a person sitting at an 219

Figure 5. Generalized stages of association and tracking in a mmWave tracking architecture system.

office desk, cannot reliably maintain a track under this assumption. This paper explores ₂₂₀ advanced strategies in section [3](#page-7-0) that attempt to overcome this assumption when tracking $_{221}$ multiple-objects. 222

Proceeding to the second stage in figure [5,](#page-6-0) although the static noise has been removed, ₂₂₃ the data points present may not be noise free. Due to the multi-path theory, there will $_{224}$ likely be a number of data points present that are ghosts of the actual reflected objects, 225 otherwise known as false positives. As a result, an appropriate correlation and clustering ²²⁶ algorithm is usually employed to alleviate this challenge and gate relevant data objects. The 227 most successful clustering algorithm that is used in point cloud data is the density-based ₂₂₈ spatial clustering of applications with noise (DBSCAN) algorithm, originally presented in $_{229}$ [\[9\]](#page-19-0). MmWave radar tracking systems predominately either use the DBSCAN algorithm for ²³⁰ clustering and association of data points or implement an alternate clustering algorithm ²³¹ that is typically a variation of the original DBSCAN algorithm. The variant DBSCAN algo-
232 rithms presented usually outperform the original DBSCAN algorithm [\[10](#page-19-1)[–13\]](#page-19-2). However, 233 before blindly adopting a variation of the DBSCAN algorithm for a claim of superiority, ²³⁴ an acknowledgment should be made of the differences between the dataset used to bench- ²³⁵ mark the variant DBSCAN algorithm and the intended dataset that the variant DBSCAN 236 algorithm will be applied to. An assessment of the differences should be made to determine $\frac{237}{2}$ if the particular variations of the DBSCAN algorithm are impacted by the differences in $_{238}$ the datasets. Once the point cloud data points have been correlated and clustered together 239 to form a set of groups, a common strategy to decide the position of a holistic object is to $_{240}$ logically take the centroid of the respective cluster. 241

After guaranteeing reliable point cloud associations and clustering has been made to $_{242}$ collate the points associated with the various objects in scene, the next step is to persist $_{243}$ a track for each of these objects across a continuous set of frames. In the vast majority of $_{244}$ mmWave multi-object tracking systems, the tracking aspect in its simplest form is primarily 245 achieved through the use of a Kalman filter. Kalman filtering is a widely adopted approach ²⁴⁶ to efficiently provide tracking and estimations [\[14\]](#page-19-3). Many variations of Kalman filters have $_{247}$ been presented in the literature to ultimately optimize the performance and outcome of ²⁴⁸ tracking an object via mmWave radar. The research conducted by $[15]$ demonstrates an $\frac{249}{2}$ example where Kalman filtering was applied to successfully track multiple objects with $_{250}$ respect to a mmWave radar. For each object detected by the radar, an individual Kalman ₂₅₁ filter is applied for tracking and estimation of the specific object. Each Kalman filter is then run independently [\[15\]](#page-19-4). The authors of [15] highlight that the success of implementing a $_{253}$ Kalman filter to track and estimate the position of an object is highly dependent on the $_{254}$ clustering and data association techniques that have been employed for object detection. ²⁵⁵

2.4. Sensing and Identification ²⁵⁶

The final component of a mmWave tracking system is any sensing and identification ₂₅₇ strategies that might be employed in addition to the core tracking architecture. The desired 258 outcome of this component of the system is to ultimately perform a particular sensing ²⁵⁹ or identification task and associate the outcomes with the tracked objects. It should be $_{260}$ noted that this stage is not required in a system where the sole objective is to simply $_{261}$ perform multi-object tracking. Nevertheless, this stage has been included for discussion ²⁶² in this paper as it serves an important role in the idealized unified tracking and sensing 263

Figure 6. Areas explored and discussed in section [3](#page-7-0) in contrast to the typical multi-object mmWave tracking architecture block diagram presented in figure [2.](#page-2-0)

framework, ultimately achieving more elaborate tracking profiles. Currently, there is no ²⁶⁴ typical/generalized way this component of a mmWave tracking system is achieved. 265

Sensing and identification components of mmWave tracking can be loosely coupled ²⁶⁶ with the ability to discontinuously track a particular object. Specific examples of this are $_{267}$ explored in section [3](#page-7-0) of this paper.

3. Advanced Technologies and Methodologies ²⁶⁹

In the previous section of this paper, a typical mmWave radar multi-object tracking 270 system and its components were explored and discussed. This section of the paper aims ₂₇₁ to describe the state-of-the-art advancements in mmWave multi-object tracking and how 272 it contributes to the generalized multi-object mmWave tracking architecture explored $_{273}$ in section [2.](#page-2-1) Figure [6](#page-7-1) highlights the areas that are being explored in this section of the $_{274}$ paper in contrast to the typical system architecture presented in figure [2.](#page-2-0) The system ²⁷⁵ architecture stages; radar data collection, position and velocity estimation, and gating are 276 all mature in the context of multi-object tracking. The areas which require most attention 277 for developing advanced methodologies is object detection, sensing and identification. ₂₇₈ These areas specifically are receiving the most focus primarily due to the limitations that 279 are faced in the current typical multi-object tracking architectures.

For each of the below sub-sections, the methodologies presented will be compared and ₂₈₁ contrasted with respect to the below criteria. The relevant advantages and disadvantages ₂₈₂ for the methodologies discussed will be outlined for each criterion (Crit.). The following 283 details the criteria that will be used to assess the methodologies: 284

- Adaptability (Adap.): The ability to apply the methodology in a generalized form so 285 that it can contribute to advancing the system architecture presented in figure [2.](#page-2-0) 286
- **Performance (Perf.):** The overall performance of the methodology with respect to it's ₂₈₇ suitability for real-time applications. 288
- Accuracy (Accu.): A consideration regarding the accuracy metric of the techniques ₂₈₉ presented in the specific methodology. ²⁹⁰
- **Specificity (Spec.):** The sensitivity of the methodology in regard to the particular ₂₉₁ event/action being measured or characterized. This criterion provides an opportunity ₂₉₂ to consider any event overlap that the methodology might have, such as false positives. 293

3.1. Object Detection Enhancements ²⁹⁴

One of the fundamental flaws in a typical mmWave tracking system is the reliance on ₂₉₅ static noise filtering. In the context of radar imaging, as opposed to tracking, there have $_{296}$

been advancements towards adaptive background filtering. Recent adaptive background ₂₉₇ filtering research in the mmWave domain can be seen presented by [\[16\]](#page-19-5). The authors $_{298}$ of [\[16\]](#page-19-5) present a novel approach toward adaptive background noise suppression, that ²⁹⁹ remains computationally cost effective. The approach presented by $[16]$ ultimately relies $\frac{300}{200}$ on the ability to observe the operating background environment without any targets in $_301$ the field of view. This allows for the construction of a background image which in turn is 302 used to derive a background power map. The work presented by $[16]$ demonstrates an 303 adaptive background filtering approach that can be used when imaging a single target with 304 mmWave. Although not practically tested, the principles that the authors of $[16]$ rely on for $\frac{305}{205}$ adaptive background subtraction are also present in the context of multi-object tracking $\frac{306}{200}$ with mmWave. Therefore, this serves as an interesting approach towards reducing the $\frac{307}{200}$ reliance on static noise filtering in the mmWave tracking domain. $\frac{308}{308}$

The reliance on static noise filtering ultimately spawns challenges related to the reliable 309 tracking of a stationary object. As a result, a large focus on methodologies and strategies to $\frac{310}{2}$ alleviate these challenges can be seen in the literature. The two overarching themes that $\frac{311}{311}$ encompass the research direction for addressing these challenges are sensor fusion and ³¹² micro-Doppler feature analysis. $\frac{313}{2}$

Sensor fusion, in the context of this paper, refers to the combination of data from $\frac{314}{2}$ additional sensors in addition to a mmWave sensor. A common approach to this in the 315 literature is to fuse camera data with the data obtained from the mmWave sensor to ³¹⁶ achieve a more coherent and comprehensive object detection algorithm, whilst alleviating 317 challenges associated with illumination in the vision domain. One of the primary challenges $\frac{318}{2}$ with fusing camera and mmWave radar detections is that they are a heterogeneous pair of $\frac{319}{2}$ sensors [\[17\]](#page-19-6). The plane in which the radar detections are aligned with is different to that 320 of the camera detection. Therefore, this can make associating the detections between the $\frac{321}{221}$ two sensors quite difficult [\[17\]](#page-19-6). Research presented by [17] demonstrate a novel approach 322 to solving the association challenge. In the methodology presented in $[17]$, the authors 323 define the concept of error bounds to assist with the data association and gating within a 324 fusion extended Kalman filter. The concept of error bounds provide a criteria to define the $\frac{325}{2}$ behavior of the individual sensors before and after the sensor fusion $[17]$.

In the fusion-extended Kalman filter presented in $[17]$, the radar point cloud clusters 327 are formed using an approach similar to the typical architecture discussed in section [2](#page-2-1) of ³²⁸ this paper, with DBSCAN. Similarly, the bounding boxes on the image plane are initially 329 formed in isolation to the radar and then sent to the fusion-extended Kalman filter to 330 be associated and tracked with the radar clusters. The plane of the camera data points ³³¹ is transformed from an image plane to a world plane using a homography estimation $\frac{332}{2}$ method $[17]$. A warped bird eye view of the camera data points can then be estimated $\frac{333}{2}$ using the world coordinates. The estimated warped birds eye view can then be compared 334 and associated with the radar point cloud data points $[17]$. In the fusion-extended Kalman 335 filter presented by $[17]$, the error bounds are updated using data points from both of $\frac{336}{2}$ the sensors (as opposed to independently) and the warped birds eye view of the image 337 plane is calculated for each sample point. As a result, the authors of $[17]$ demonstrate $\frac{338}{2}$ that although this yields a higher association accuracy a time synchronization challenge is $\frac{339}{2}$ faced between the sensors. This challenge is resolved in the research by ensuring timeline $\frac{340}{2}$ alignment between the sensors and a synchronization strategy is employed by comparing ³⁴¹ certain regions of the fusion-extended Kalman filter output with the error bounds $[17]$. The $\frac{342}{2}$ experimental results presented by [\[17\]](#page-19-6) appear to demonstrate a higher reliability in real-time 343 target detection and persisted tracks, compared to a radar alone. Another approach seen in ³⁴⁴ literature towards mmWave sensor fusion, is a track-to-track based association method. The 345 authors of [\[18\]](#page-19-7) demonstrate an implementation of track-to-track based association between ³⁴⁶ a mmWave radar and a thermal camera. In the research presented by [\[18\]](#page-19-7), it is assumed the $\frac{347}{2}$ independent sensors are co-located, whereby the two sensors are orientated and located $\frac{348}{2}$ is the same position. Under this operating condition, the targets in the field of view are ³⁴⁹ tracked independently by the mmWave sensor and thermal camera. The independent ³⁵⁰ tracks are then ultimately associated by solving a combinatorial cost minimization problem. 351 In the research presented by $[18]$, the components involved in this problem are identified 352 \overline{a} s: \overline{a} s:

- **Estimated distance** 354
- Projected horizontal component 355
- **Frack length** 356

Exploiting micro-Doppler in mmWave radar systems is actively being sought as ³⁵⁷ another angle to devise methodologies that resolve the challenge of static object detection $\frac{358}{2}$ and localization. Specifically in the context of human detection, bio-metric information, $\frac{359}{2}$ such as heartbeat and breathing are being explored as potential features that are measurable 360 through micro-Doppler. A study performed by [\[19\]](#page-19-8) demonstrates an algorithm designed $_{361}$ to localize multiple static humans using their individual breathing pattern. The research ₃₆₂ performed by [\[19\]](#page-19-8) highlight that the time of flight of a signal is minimally impacted by the $\frac{363}{100}$ small movements of a breathing chest cavity. As a result, the sub-millimeter movements 364 are lost when performing static background removal between two consecutive frames, 12.5 365 milliseconds apart in the case of the experiment performed by [\[19\]](#page-19-8). To counter this loss of 366 information, the authors in $[19]$ suggest subtracting the static background from a frame 367 that is a few seconds apart, 2.5 seconds in the case of the research performed by [\[19\]](#page-19-8). In $\frac{368}{10}$ doing this, the sub-millimeter movements are ultimately exaggerated in comparison to a ³⁶⁹ truly stationary object and therefore are left intact when preforming a removal of static data 370 points. The state of the st

The authors of $[19]$ make note that removing static background points from a frame 372 that is a few seconds apart does not work in for a non-stationary object, such as a person 373 walking. This is due to the principle that the movements appear exaggerated when 374 comparing to a frame a few seconds apart, so [\[19\]](#page-19-8) notes that walking appears 'smeared' in $\frac{375}{2}$ this regard. Based on this differing outcome with static and dynamic objects, the algorithm 376 presented in [\[19\]](#page-19-8) employs independent different background removal strategies; one for $\frac{377}{2}$ static object using a long window and one for dynamic objects using a short window. The $\frac{378}{278}$ experimental results presented in [\[19\]](#page-19-8) demonstrate a high accuracy of 95%. It should be $\frac{379}{2}$ noted that the experiments performed by [\[19\]](#page-19-8) does not appear to quantify the success of 380 both moving individuals and static individuals simultaneously within the scene. The radar 381 architecture used in the research presented by $[19]$ is slightly different to the mmWave 382 tracking system that has been discussed in this paper. However, the research performed $\frac{383}{383}$ by [\[19\]](#page-19-8) illustrates the potential to use vital signs as a means of detecting a static object. ₃₈₄ It would be of interest to assess the range potential of implementing a static localization $\frac{385}{100}$ algorithm of this nature using a mmWave tracking system architecture. $\frac{386}{366}$

The literature explored in this paper regarding vision sensor fusion and bio-metric ³⁸⁷ micro-Doppler feature analysis are viable approaches to enhance traditional object detection ³⁸⁸ techniques to track objects interchanging from a dynamic and static movement state. Table ³⁸⁹ [1](#page-10-0) outlines the advantages and disadvantages of the two methodologies with respect to the ³⁹⁰ comparison criteria. Although individually both methodologies prove viable, it would $_{391}$ be interesting to consider a combination of both methodologies to compliment each other. ₃₉₂ Specifically, incorporating a micro-Doppler feature analysis component to the vision system 393 could in turn remove the need of utilizing the universal background subtraction algorithm ³⁹⁴ [\[20\]](#page-19-9) for identifying moving objects in the image. This could potentially be considered as $\frac{395}{2}$ a three component sensor fusion approach, where camera data points, static radar data 396 points and dynamic radar points are fused. $\frac{397}{2}$

3.2. Sensing Methodologies 398

Sensing is not typically considered a usual aspect that is present in an object tracking $\frac{399}{2}$ system. However, it is a stream of research that has been investigated independently $_{400}$ and has the potential when integrated with a tracking system to enhance the tracking $_{401}$ systems sensitivity and reliability. An enhancement to the tracking system through sensing 402 could ultimately spawn through the additional extracted features that the sensing solution 403

Crit.	mmWave and Vision Sensor	Micro-Doppler Feature Analysis			
	Fusion				
Adap.	Low architecture assump- \checkmark tions. Unified sensor point cloud \checkmark	Decoupled from architecture ✓ dependencies. Specialized noise treatment. \times			
	data. Unified plane projection \times overhead.				
Perf.	Suitability demonstrated in \checkmark the literature. Potential time synchroniza- \times tion drift.	No impact to typical multi- ✓ object detection. Immature understanding on X technique overhead.			
Accu.	Azimuth angle accuracy ✓ improved. Multi-object track persis- \checkmark tence improved. Immature system under- \times standing regarding the compromise of a single sen- sor (i.e. dark room).	High for multiple dynamic ✓ objects. Uncompromised fixed multi- ✓ object tracking. Immature understanding re- X garding accuracy and range relationship.			
Spec.	All moving objects have a \checkmark presence in radar and vision that can be correlated. Fixed objects of interest are \times not typically distinguish- able.	Technique not constrained to ✓ breathing. Immature understanding × of simultaneous static and fixed multi-object tracking.			

Table 1. A comparison of methodologies explored for the enhancement of object detection in a mmWave tracking architecture.

provides, granting more data points that can be incorporated into the tracking estimation 404 and prediction. The advanced sensing methodologies that are explored in this paper can be 405 classified as either general activity recognition or specialized estimation methodologies. 406

General activity recognition can be considered as a class of sensing methodologies 407 that have an underlying objective of classifying a broad set of movements or activities that $\frac{408}{408}$ a given object in the field of view might exhibit. One stream of research that dominates this 409 class of sensing methodologies is human activity recognition (HAR). Traditionally, a radar ⁴¹⁰ based HAR system relied on machine learning techniques such as random forest classifiers 411 [\[21\]](#page-19-10), dynamic time warping [\[22\]](#page-19-11) and support vector machines (SVM) [\[23\]](#page-19-12). In comparison to ⁴¹² a deep learning based approach, these techniques are usually computationally less taxing 413 due to their lower complexity. However, relying solely on conventional machine learning ⁴¹⁴ techniques for HAR contrastingly presents several limitations. A survey conducted by ⁴¹⁵ the authors of [\[24\]](#page-19-13) provides a thorough critical analysis over the evolution of radar-based ⁴¹⁶ HAR. In $[24]$, a conventional machine learning approach to HAR is considered to make 417 optimization and generalization of the HAR solution difficult. The authors of $[24]$ highlight 418 three fundamental limitations of machine learning techniques with respect to a HAR system. 419 The first acknowledges the approach in which feature extraction takes place, specifically a 420 manual procedure based on heuristics and domain knowledge which is ultimately subject 421 to the human's experience $[24]$. The second limitation identified relates to the fact that 422 manually selected features tend to also be accompanied by specific statistical algorithms 423 that are dependent on the trained dataset. As a result, when applying the trained model to $_{424}$ a new dataset the performance is typically not as good as the dataset that was used to train 425 the model. Lastly, the authors of $[24]$ highlighted that the conventional machine learning 426 approaches used in a radar based HAR system primarily learn on discrete static data. This 427

Figure 7. Walking classification system designs explored in [\[25\]](#page-19-14); **a)** Principal component analysis combined with support vector machine classification; **b)** Principal component analysis combined with k-nearest neighbor classification; **c)** t-distributed stochastic neighbor embedding combined with support vector machine classification; **d)** t-distributed stochastic neighbor embedding combined with k-nearest neighbor classification.

poses a difference between the data that is used to train a model and the data that the model 428 is subject to during real-time testing. The real-time data is principally continuous and 429 dynamic in nature. The survey conducted by [\[24\]](#page-19-13) explores the potential for deep learning 430 to assist in alleviating these limitations in machine learning radar-based HAR systems. $\frac{431}{431}$

Although there are some limitations with using conventional machine learning approaches, it should also be acknowledged that there has been successful applications of $\frac{433}{433}$ radar-based HAR using these techniques. The research presented in [\[25\]](#page-19-14) identifies recent ⁴³⁴ work that attempts to classify three different walking/movement patterns:

- Slow walk \bullet
- Fast walk ⁴³⁷
- Slow walk with hands in pockets $\frac{438}{438}$

The authors of $[25]$ attempt to classify these walking patterns comparing the performance 439 between an approach using k-Nearest Neighbor (k-NN) and SVMs. The four system designs 440 explored in the work presented by $[25]$ can be seen illustrated in [7.](#page-11-0) In $[25]$, both the range-Doppler and Doppler-time data is incorporated into feature extraction. In the research 442 presented by [\[25\]](#page-19-14), the impact each of the walking patterns has in the range-Doppler and ⁴⁴³ Doppler-time maps is illustrated in the form of a heat-map. It can be seen in this illustration, $\frac{444}{4}$ that the change in walking speed (the difference between slow and fast walking) results in 445 a dramatic change in the range-Doppler and Doppler-time maps. Whereas, maintaining a 446 consistent walking speed and with hands in the pocket has less of a notable difference. $\frac{447}{400}$

In regard to extracting the features, the authors of $[25]$ explore and compare two $\frac{448}{4}$ potential approaches, using either Principle Component Analysis or t-distributed Stochastic ⁴⁴⁹ Neighbor Embedding. Both of which are non-supervised transform algorithms. The two 450 feature extraction methods are compared against each other whilst equally being applied ⁴⁵¹ with the two aforementioned classification methods. The permutations of feature extraction 452 methods with classification algorithms explored are shown in figure $\frac{7}{10}$. The results obtained $\frac{453}{153}$ from [\[25\]](#page-19-14) for each of the explored system designs in figure [7](#page-11-0) demonstrate the capability of $_{454}$ classifying fast and slow walking with high accuracy. Using the feature extraction methods 455 and classification algorithms explored in [\[25\]](#page-19-14), the authors note a 72% accuracy in classifying 456 slow walking with hand in the pocket.

Another piece of leading research in radar-base HAR is RadHAR presented in $[26]$. In 458 [\[26\]](#page-19-15), the authors explore a range of classification approaches, including both conventional 459 machine learning algorithms and deep learning based algorithms. The primary objective $\frac{460}{460}$ of the RadHAR system is to classify five human movement activities; walking, jumping, $_{461}$ jumping jacks, squats and boxing. $\frac{462}{462}$

Unlike the research presented in [\[25\]](#page-19-14), in [\[26\]](#page-19-15) the data that is used for classification $\frac{463}{100}$ originates from point cloud. The point cloud data is first voxelized to to ensure a uniform ⁴⁶⁴ frame size, despite the number of points, before feeding to the classification algorithm. ⁴⁶⁵ Using the voxelized point cloud data, an SVM, multi-layered perceptron (MLP), Long $_{466}$ Short-term Memory (LSTM) and convolution neural network (CNN) combined with LSTM 467 were trained and compared against each other. 468

The results of the research conducted in $[26]$ demonstrate that the classification algorithm with the highest accuracy, 90.47% , is that of a combined time-distributed CNN $_{470}$ and bi-directional LSTM. The authors of [\[26\]](#page-19-15) hypothesis that the high accuracy of this approach can be attributed towards the fact that the time-distributed CNN learns the spatial ⁴⁷² features of the point cloud data, whilst the bi-directional LSTM learns the time dependent 473 component of the activities being performed. ⁴⁷⁴

Another more recent piece of research, presented in [\[27\]](#page-19-16), demonstrates a mmWave 475 sensing framework that is capable of recognizing gestures fundamentally using micro-Doppler and AoA (both elevation and azimuth) data to form a set of feature maps. Features 477 are then ultimately extracted using an empirical feature extraction method and used to train 478 a MLP to classify gestures [\[27\]](#page-19-16). An important aspect to consider regarding the research 479 presented by the authors of $[27]$, is that the approach presented is for a field of view where only a single human performing gestures is present (i.e. not multi-object). This same ⁴⁸¹ limitation can also be seen in a similar piece of research presented in [\[28\]](#page-19-17). The authors 482 of [\[28\]](#page-19-17) demonstrate a mmWave system capable of performing 3D finger joint tracking ⁴⁸³ using the vibrations and distortions evident on the forearm as a consequence to finger 484 movements. However, as previously mentioned, this specialized estimation is also subject $\frac{485}{485}$ to the challenge of operating in a multi-person environment. Despite this, the authors of 486 $[27]$ have made their approach so that underlying encoded assumptions about the number 487 of people in the field of view has been abstracted from the core methodology to performing 488 gesture recognition. Instead, the field of view constraint has been isolated to being a data 489 formation challenge. The authors of $[27]$ acknowledge that the range data has not been 490 taken into account in their presented approach, but would yield beneficial in extending $_{491}$ their design to handle multiple people simultaneously performing their own sequence of 492 gestures. Putting the specific classification task aside, the abstracted methodology presented 493 by the authors of $[27]$ could serve as a framework to incorporating generalized activity 494 recognition into a mmWave multi-object tracking system, ultimately uplifting the tracking 495 profile maintained for an individual. As the authors of $[27]$ did not have multi-object within 496 scope, extending the methodology to operate on each range bin, for satisfying multi-object 497 support, raises concerns around whether real-time processing is still feasible.

Specialized estimation, as opposed to general activity recognition, is a class of sensing 499 that ultimately has a primary focus on a single objective that can be measured. Measurement $\frac{500}{200}$ of this nature of course should be considered as an estimation. This class of sensing has $_{501}$ overlap with features that can be used as a criteria for identifying a specific object. More $_{502}$ details on features with the potential to be used as an identification strategy are addressed $\frac{503}{200}$ in section [3.3](#page-13-0) of this paper. The primary driver behind research in radar-based specialized $_{504}$ estimation methodologies originates from a human health perspective. The ability to $_{505}$ determine human vital signs passively is an area in which mmWave radar is being explored ₅₀₆ as a viable solution. A study performed in [\[29\]](#page-19-18) demonstrates a solution named 'mBeats' 507 which aims to implement a moving mmWave radar system that is capable of measuring $\frac{508}{100}$ the heart beat of an individual. The proposed 'mBeats' system implements a three module $\frac{509}{200}$ architecture. The first modules is a user tracking module, which the authors of $[29]$ state $\frac{100}{2}$ that the system utilizes a standard point cloud based tracking system, as illustrated in $_{511}$ section [2](#page-2-1) of this paper. The purpose of this module is to ultimately find the target in the $\frac{512}{2}$ room. It should be noted that in [\[29\]](#page-19-18) an assumption is made that there will only be one $\frac{513}{2}$ target in the field of view. The second module is termed proposed in $[29]$ is termed as the 514 'mmWave Servoing' module. The purpose of this module is to optimize the angle in which 515 target is situated from the mmWave radar to give the best heart beat measurement. To $_{516}$ achieve this, the authors of $[29]$ specify the ultimate goal of this module as obtaining peak 517 signal reflections for the targets lower limbs, since the mmWave radar is situated on a robot $\frac{1}{518}$ at ground level. Using the Peak To Average value as a determinant for the reflected signal $\frac{519}{2}$ strength, the authors define an observation variable which is incorporated by a feedback $_{520}$ Proportional-Derivative controller to ultimately orientate the radar in the direction that ₅₂₁ yields the highest signal strength. 522

The last module is the heart rate estimation module, responsible for ultimately determining the targets heart rate from a set of different poses. The poses consist of various sitting and lying down positions. The authors of [\[29\]](#page-19-18) acknowledge that heartbeats lie in the frequency band of 0.8 4Hz, and therefore implement a biquad cascade infinite impulse response (IIR) filter to eliminate unwanted frequencies and extract the heartbeat waveform. A CNN is selected in [\[29\]](#page-19-18) as the predictor due to the heartbeat detection problem being considered as a regression problem. The authors state that a key challenge with using a CNN for this problem is estimating the uncertainty of the result. Uncertainty in this problem is ultimate caused by measurement inaccuracies, sensor biases and noise, environment changes, multipath and inadequate reflections [\[29\]](#page-19-18). To overcome this, the authors of [\[29\]](#page-19-18) cast the problem into a Bayesian model, defining the likelihood between the prediction and ground truth (**y**) as a probability following a Gaussian distribution. This ultimately results in a loss function as illustrated in equation [\(7\)](#page-13-1).

$$
loss(x) = \frac{\|\mathbf{y} - \hat{\mathbf{y}}\|_2}{2\mathbf{\alpha}^2} + \frac{1}{2}\log \mathbf{\alpha}^2
$$
 (7)

where the CNN predicts a mean \hat{y} and variance α^2 . Using this approach the authors s23 of [\[29\]](#page-19-18) compare the outcome of their model with three other common signal processing 524 approaches (FFT, Peak Count (PK) and Auto-correlation (XCORR)) with accuracy as the $\frac{525}{225}$ metric that is compared. $\frac{526}{26}$

In the results presented in [\[29\]](#page-19-18), it can be seen that the other approaches fail to maintain 527 an accuracy above 90% in all poses, whereas the CNN presented in [\[29\]](#page-19-18) does maintain a $\frac{528}{2}$ high accuracy for the selected poses. The authors acknowledge that in the current system $\frac{529}{2}$ the target must maintain static whilst performing the heartbeat measurement and that 530 future work will be focused on measuring a moving object. It would also be interesting to $\frac{531}{531}$ assess the viability and challenges of this approach in a multi-person scene. $\frac{532}{2}$

The underlying theme of the sensing methodologies explored in this paper is that $\frac{533}{133}$ independently they are successful in the goal they aim to achieve. However, there is a lack $_{534}$ of acknowledgment in the literature regarding the suitability of these methodologies in a combined holistic tracking and sensing architecture. It would not only be interesting to $\frac{536}{120}$ assess their suitability in such a system, but also how they may contribute to enhance the $\frac{537}{2}$ sophistication and reliability of such a tracking system. Table [2](#page-14-0) outlines the advantages 538 and disadvantages of the explored sensing methodologies, with respect to the comparison 539 criteria. It can be seen in this table that both methodologies explored fail to address the ⁵⁴⁰ challenges of operating in a multi-object environment. In order to achieve a tracking system $_{541}$ that completes a target profile with sensing characteristics, the challenge of sensing multiple 542 objects and associating the acquired information to a detected target must be solved. $\frac{543}{543}$

3.3. Identification Strategies 544

The development of identification methodologies is a natural direction of the evolution 545 for mmWave tracking systems. It can be considered a more unique type of specialized $_{546}$ estimation sensing but with the key focus on being able to reliably and uniquely correlate $\frac{547}{2}$ the sensed information to a tracked object. There are a number of challenges that need $_{548}$ to be considered and overcome in identification approaches, such as the feasible range, ⁵⁴⁹ separation of multiple objects/people and generalization of the approach. This sections $\frac{550}{2}$ aims to explore the leading identification methodologies of radar-based tracking systems. ⁵⁵¹

Gait identification approaches rely on the different gait characteristics between individuals. Gait based identification strategies are the most common passive based approach to 553

Crit.	Generalized Activity Recogni-	Specialized Estimation		
	tion			
Adap.	Decoupled architecture im- √ pact.	Trusted point cloud process- ✓ ing techniques.		
	Uncertain tracking enhance- \times ment reliability.	Uncertain feedback enhance- \times ment reliability.		
Perf.	Algorithm real-time perfor- ✓	Real-time suitability has \checkmark been proven viable.		
	mance proven. Uncertain system suitability. \times	Optimization overhead to \times		
		accommodate.		
Accu.	High pre-defined activity ✓	High due to the narrow		
	accuracy.	focus.		
	Dependent on training envi- \times ronment.	Highly coupled to the train- \times ing data.		
Spec.	Pre-defined actions reliably ✓	Optimized for estimating a ✓		
	classified.	single action.		
	Uncertainty of multi-object \times suitability.	One target is considered for X estimation.		
	Simultaneous classification \times challenging.	Immature literature in \times mmWave field.		

Table 2. A comparison of sensing methodologies explored for the enhancement of tracking reliability in a mmWave tracking architecture.

identifying people in a radar or WiFi based tracking system. They fundamentally leverage $_{554}$ that each person typically has a unique pattern in the way they walk, this pattern is most 555 often identified through a deep learning based technique. Gait recognition can pose it's 556 own challenges, such as inconsistencies and unpredictable upper limb movements that 557 influence the lower limb signal reflections. This interference can ultimately reduce the $\frac{558}{558}$ reliability of obtaining a consistent lower limb gait pattern for a given individual. A recent 559 study performed in [\[30\]](#page-19-19) attempts to overcome the challenges associated with upper limb movement interference by narrowing the vertical field of view and focusing attention on $_{561}$ the finer grain movements of the lower limbs. The research presented in [\[30\]](#page-19-19) proposes a $_{562}$ system that comprises of three phases: $\frac{563}{200}$

- 1. Signal processing and feature extraction 564
- 2. Multi-user identification 565
- 3. CNN-based gait model training 566

In the first phase the authors of [\[30\]](#page-19-19) construct a range-Doppler map following the traditional methodology described in section [2](#page-2-1) of this paper. The stationary interference in the range-Doppler map is then removed following a technique similar to the described approach in section [2.3](#page-5-3) of this paper. The stationary reflections are subtracted from each frame of the range-Doppler frequency responses. The authors of [\[30\]](#page-19-19) observe that a cumulative deviation of the range-Doppler data occurs due to the dynamic background noises, which are not eliminated when subtracting the static interference. To overcome this, a threshold-based high-pass filter is implemented with a threshold *τ* of 10*dBFS*. This filter is described in equation [\(11\)](#page-13-2).

$$
R_{(i,j,k)} = \begin{cases} R_{(i,j,k)}, & R_{(i,j,k)} \ge \tau, \\ 0, & R_{(i,j,k)} < \tau, \end{cases}
$$
 (11)

where $R_{(i,j,k)}$ is the range-Doppler domain frequency response at the k_{th} frame with range i s67 and velocity *j*.

The authors of [\[30\]](#page-19-19) identify that the dominant velocity \hat{V}_i can be used to describe the targets lower limb velocity in each frame. In [\[30\]](#page-19-19), this is expressed as equation [\(12\)](#page-15-0).

$$
\hat{V}_i = \frac{\sum_{j=1}^{N_D} (\hat{R}_{(i,j,k)} V_j)}{N_D}, i \in [1, N_R], j \in [1, N_D].
$$
\n(12)

where $\hat{R}_{(i,j,k)}$ is the normalized frequency response, V_j is the velocity corresponding to the 569 frequency response $R_{(i,j,k)}$, N_R and N_D represent the number of range-FFT and Doppler-FFT $\;$ 570 points respectively. $\frac{571}{200}$

The authors of $[30]$ illustrate the composition of these gait characteristics as a heat-map 572 corresponding to the actual gait captured with a camera. Using these extracted gait features, 573 the author of $[30]$ identifies that multiple targets can be differentiated firstly by range and 574 secondly (if the range is the same) by leveraging distinct spatial positions. This is ultimately 575 done by projecting the point $R_{(i,j,k)}$ in the $k_t h$ frame to a point $\hat{R}_{(i,j,k)}$ in the two-dimensional $\frac{1}{576}$ spatial Cartesian coordinate system. To differentiate the data points in the spatial Cartesian 577 coordinate system, [\[30\]](#page-19-19) implements a K-means clustering algorithm. Each individual gait 578 feature can be generated as a range-Doppler map by negating the frequency responses that ⁵⁷⁹ were not correlated in the K-means clustering [\[30\]](#page-19-19). After differentiating the gait features, $\frac{580}{2}$ the authors of [\[30\]](#page-19-19) then identify a challenge regarding the segmentation of the actual step. $\frac{581}{100}$ In [\[30\]](#page-19-19), this is ultimately overcome by using an unsupervised learning technique to detect $\frac{582}{2}$ the silhouette of the steps. $\frac{583}{200}$

Finally, a CNN-based classifier in the image recognition domain is used to identify the $\frac{584}{584}$ patterns associated with the gait feature maps. The classifier is assessed with multiple users $\frac{585}{585}$ and varying steps to determine the overall accuracy of the system. Overall, the system $\frac{586}{20}$ demonstrates a high accuracy that marginally decreases in accuracy as the number of users increases but is ultimately corrected as the number of steps increases. $\frac{588}{588}$

Another overarching class of identification strategies being explored are tagging based ₅₈₉ approaches. This is not a passive approach unlike the others mentioned in this paper $\frac{590}{2}$ and involves incorporating a tag on the object so that it can be uniquely identified. There $\frac{591}{591}$ are two directions in which the literature focuses on in regards to identification of this ₅₉₂ nature. The first is radio frequency identification (RFID). In a chipless based RFID system, ₅₉₃ data must be encoded in the signal either by altering the time-domain, frequency-domain, ⁵⁹⁴ spatial-domain or a combination of two or more of the domains. An example of RFID 595 implemented as an identification strategy in mmWave can be seen in the 'FerroTag' research 596 presented in [\[31\]](#page-19-20). The 'FerroTag' system presented in [31] is a paper-based RFID system. ₅₉₇ Although the usage of the FerroTag research is intended for inventory management, it $\frac{598}{2}$ could potentially be adopted to as a tagging strategy for a tracking based system. FerroTag $\frac{599}{2}$ is ultimately based on ferrofluidic ink, which is colloidal liquids that fundamentally contain $\frac{600}{200}$ magnetic nanoparticles. The ferrofluidic ink can be printed onto surfaces which in turn 601 will embed frequency characteristics in the response of a signal. The shape, arrangement 602 and size of the printed ferrofluidic ink will ultimately influence the frequency tones that $\frac{603}{603}$ are applied to the response signal. In order to identify and differentiate the different $\frac{604}{604}$ signal characteristics caused by the chipless RFID surface, the solution presented by $[31]$ ⁶⁰⁵ utilizes a random forest as a classifier to identify the corresponding tags present in the \sim $\frac{606}{25}$ field of view. The second approach to tagging as a means of identification is through 607 re-configurable reflective surfaces (RIS). To the best of our knowledge no system has been 608 presented in the literature that demonstrates a practical RIS solution for identification 609 purposes in a mmWave tracking system. Research regarding RIS with respect to mmWave 610 is predominantly in the communication domain. The challenges and opportunity to design 611 an RIS based identification system for a mmWave tracking system are yet to be detailed. 612

Shape profiling has been seen implemented in previous mmWave research to identify 613 an object by the properties of the objects shape. For example, if the object being tracked 614 is a human, the height and curvature of the human body can influence the way in which $\frac{615}{615}$ the mmWave signal is reflected [\[32\]](#page-19-21). The authors of [32] demonstrate how a human being $\frac{616}{2}$ tracked and represented in point cloud form can be identified based on the shape profile of 617 their body. Using a fixed-size tracking window, the related points to the particular human 618 are voxelized to form an occupancy grid $[32]$. This is then ultimately sequenced through a 619 Long-short Term Memory network to classify the particular human $[32]$. This particular $\frac{620}{20}$ identification method is abstracted from the tracking aspect of the process, therefore making 621 it suitable regardless if there are multiple objects being tracked. suitable for identifying 622 objects in an environment where multiple object tracking is taking place. $\frac{623}{623}$

The research presented in [\[33\]](#page-19-22) differs to that presented in [\[32\]](#page-19-21) in the regard that the 624 tracking data is not used during the identification stage. Instead, the authors in [\[33\]](#page-19-22) propose $\frac{625}{625}$ a strategy where once the human has been tracked, the radar adjusts its transmit and receive $\frac{626}{626}$ beams towards the tracked human. By doing so the granularity of the feature set available $\frac{627}{627}$ from the human body is increased. In other words, more specific profiling can be performed $\frac{628}{628}$ on the individual. The research presented in [\[33\]](#page-19-22) demonstrates the ability to characterize $\frac{629}{629}$ the human body by its outline, surface boundary and vital signs. Having this granular $\frac{630}{100}$ feature set, and tailored profiling, provides a stronger ground to positively identify an ⁶³¹ individual. However, this particular method does come at the cost of directing the beam 632 just for identification purposes. Additionally, the existing research presented in $[33]$ does $\frac{633}{2}$ not make any remarks regarding the suitability for this method in real-time applications. $\frac{634}{6}$

The various identification strategies explored in this section of the paper each have 635 their own complexities involved in fundamentally incorporating into a tracking system. $\frac{636}{120}$ Table [3](#page-17-0) aims to assist in comparing the various identification methodologies, to ultimately $\frac{637}{637}$ understand their suitability and limitations around implementing them in a tracking 638 $\mathsf{system.}$. The system is a set of $\mathsf{S39}$ and $\mathsf{S$

4. Future Research Directions ⁶⁴⁰

Despite many advancements underway in achieving a unified mmWave tracking and 641 sensing architecture, there are still many challenges and limitations to be resolved. The 642 following are suggestions for some of the key areas in which future research should be $\frac{643}{643}$ directed to assist in the development of the limitations associated with such a unified $\frac{644}{644}$ system: ⁶⁴⁵

- **Concurrent Tracking Enhancements:** The number of people that can reliably be ⁶⁴⁶ concurrently tracked continues to be a challenge for a tracking system. It would be 647 of interest to explore potential areas that could provide a scalable approach to this ⁶⁴⁸ problem. Integrating sensing outcomes into the tracking estimation and prediction 649 filter could be an area that is worth exploring to assist with overcoming tracking $\frac{650}{650}$ concurrency challenges. $\frac{651}{651}$
- **Coverage Area:** The maximum range in which a solution is functional until can ⁶⁵² impact the practicality of the solution. This is specifically true for systems that are 653 dependent of high signal resolution, therefore sacrificing range. The default approach 654 to this problem is to simply increase the transmitter power. However, in situations 655 where this might not be possible it would be beneficial to research novel approaches 656 that overcome signal range without increasing the transmitter power and minimally 657 impacting the resolution. It could prove beneficial to investigate the techniques being 658 employed using RIS in the communications domain for signal propagation and beam 659 steering as a potential to be smarter with obtaining a larger coverage area. $\frac{660}{660}$
- **Integrating Tracking and Sensing Systems:** There are currently not many integrated 661 sensing and tracking mmWave systems present in the literature. The challenges and 662 limitations that come with doing so deserve more focus. Integrating systems of this $\frac{663}{663}$ nature could prove fruitful in designing an enhanced tracking system capable of 664 discontinuous tracking and more robust predictions.
- **Real-time Performance:** As the techniques for advanced tracking systems evolve and 666 become more complex, their feasibility for real-time applications requires assessment. 667 This especially becomes true when incorporating sensing solutions reliant on deep 668 learning based algorithms.

Crit.	Gait			Tagging		Shape Profile
Adap.	\checkmark \times \times	Low architec- ture impact. Ability to corre- late to multiple tracks un- known. Specific hard- ware position- ing.	✓ \times \times \times	Loosley coupled to tracking ar- chitecture. Different data domain. Additional hard- ware. Multi-object correlation chal- lenge.	✓ \times	Potential to extend on point cloud. Sampling con- cerns with simultaneous beam directing and tracking.
Perf.	✓ \times	Proven real- time viability. Compute over- head.	✓ ✓ \times	Very minimal impact. Pre-encoded data absorbs impact. Untested multi- object setting.	✓ \times	Minimal over- head. Suitability un- proven.
Accu.	\checkmark \times	High multi- object accuracy. Scalability chal- lenges.	✓ \times	Very accurate. Immature un- derstanding on range.	\checkmark \times	No impact due to multi-object. External depen- dencies.
Spec.	✓ \times	Focused move- ment considera- tions. Challenges with wider field of view.	✓ \times	Low risk of false positives. Undefined challenges with multi-object.	✓ \times	Multi-objects independently profiled. Immature un- derstanding on environmental impacts.

Table 3. A comparison of identification methodologies explored for the enhancement of tracking objects discontinuously in a mmWave tracking architecture.

- **Stationary Object Tracking:** Lastly, in a pure tracking system a large fundamental σ ₀₇₀ floor is the method in which static noise is removed from the signal response. The 671 traditional approach of subtracting signal responses that do not change between 672 frames immediately scarifies stationary objects that should not be considered as noise, $\frac{673}{673}$ such as a person sitting. This challenge could be researched by either exploring more 674 sophisticated static noise removal techniques or by attempting to recover stationary 675 objects of interest after the removal of static signal responses. ⁶⁷⁶
- **RNN Suitability** In the literature there is an underlying theme of CNN models being 677 utilized and demonstrating the best performance. This is in contrary to the theoretical σ ₆₇₈ better suitability of recurrent neural network (RNN) models for temporal based data. 679 A likely reason for their lack of use could be attributed toward the difficulty of training $\frac{680}{100}$ the shared parameters across the layers. It would be interesting to look at introducing 681 an algorithm unfolding technique to address this potential issue by embedding domain 682 knowledge into the network itself. The same state of the state of the state of

5. Conclusion 684

This paper aimed to provide an overview and analysis into traditional, state-of-the- ⁶⁸⁵ art, and future methodologies for mmWave multi-object tracking. In the review of the 686 advanced methodologies it should be noted that many of the approaches explored have 687 only been implemented in an isolated setting. They demonstrate their potential and success 688 in achieving the particular purpose they were intended for. However, the challenges and $\frac{689}{689}$

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