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**Efficient Extraction of Silica from Openly Burned Rice Husk Ash as**

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## **Abstract:**

 Rice is the staple food in many countries including Bangladesh. In Bangladesh, >80% of the total irrigated area is planted with rice. This leads to generate a huge amount of rice husk (RH) as a solid waste which requires proper management. This study, therefore, aimed to extract amorphous silica from openly burned rice husk ash (RHA) using a low-cost energy-saving method by avoiding calcination or combustion processes. The extracted silica was then applied for the removal of environmental contaminants i.e., methylene blue dye from an aqueous solution. It was found that the yield of silica produced from sulfuric acid-pretreated RHA was 72.4%. The FTIR absorption 35 peaks in 1057 and 783 cm<sup>-1</sup> indicate the presence of a highly condensed silica-containing asymmetric and symmetric siloxane (Si-O-Si) network mixture. The broad maximum bond peak 37 intensity at  $2\theta = 22^{\circ}$  by x-ray diffraction analysis also indicates that the produced silica was amorphous with a mesoporous structure. The sulfuric acid treated RHA-based silica surface area 39 was 182 m<sup>2</sup>/g. This silica resulted in a maximum adsorption capacity of 107 mg/g of methylene blue at pH 8 with a faster equilibrium of 60 minutes. The mechanistic study indicated that Langmuir's and Freundlich both adsorption isotherms were fitted well which indicated homogeneous adsorbent surfaces involving monolayer and multilayer adsorption processes.

**Keywords:** Rice husk ash; Acid-pretreatment; Mesoporous silica; Methylene blue; Adsorption

**1. Introduction**

 Bangladesh is an agricultural country, and approximately 80% of the total irrigated lands are used for rice production (BRRI, 2021). Consequently, the rice processing industries produce large amounts of rice husk waste. The milling of paddy rice generates about 70% yield of rice as the principal product together with unconsumed portions of rice husk (RH, 20%)[,](https://www.omicsonline.org/searchresult.php?keyword=rice-bran) [rice bran](https://www.omicsonline.org/searchresult.php?keyword=rice-bran) **(**8%), and rice germ (2%) (Me and Bee Ling, 2016; Van Hoed et al., 2006). As significant amounts of RH are produced during the milling of paddy rice, RH has been utilized for different purposes including activated carbon production (He et al., 2021; Wazir et al., 2020), electricity generation (Ejiofor et al., 2020; Silva et al., 2021), nitrates, and heavy metal removal from wastewater (Ag et al., 2018; Sadeghi Afjeh et al., 2020). However, most RH in Bangladesh is being utilized for energy production. Hence, a significant amount of rice husk ash (RHA) is generated by those small-scale industries enriched with a high portion of silica content (Zareihassangheshlaghi et al., 2020). The silica content in RHA depends on various factors including climate, soil types, harvesting season, the amounts of fertilizers used during cultivation, and geographical and environmental aspects (Beidaghy Dizaji et al., 2019; Singh et al., 2022). This RHA is often dumped on land leading to pollution of the soil environment. Therefore, recycling of such RHA into valuable products or use as adsorbent (Silvalingam and Sen, 2020; Costa and Paranhos, 2019; Mor et al., 2016; Lakshmi et al., 2009; Mane et al., 2007) has great demand as RHA contains more than 90% silica with small fractions of other inorganic oxides such as sodium, potassium, iron, and magnesium (Alam et al., 2020). Among these constituents, silica is the crucial element forming the inorganic compound 65 silicon dioxide  $(SiO<sub>2</sub>)$ . Although silica is found in nature, mainly as sand or sand quartz, RHA represents another potential source. Silica is industrially used for many purposes e.g., as an additive for catalyst, insulation, toothpaste, coating solutions, and cosmetics (Park et al., 2021).

 Furthermore, rice husk-derived silica is used as an adsorbent for organic dye removal (Niculescu and Raboaca, 2021), for the removal of phosphates and heavy metals (Dutta Gupta et al., 2021; Suzaimi et al., 2020), filler in plastics and rubber compounding (Karthigairajan et al., 2020), wastewater treatment (Mohamed and Alfalous, 2020), gas purification (Bakdash et al., 2020), ceramics processing (Sobrosa et al., 2017), thermal insulators (Hossain et al., 2017; Sembiring et al., 2016), concrete (Zareei et al., 2017), steel, and refractory bricks (Shen, 2017).

 Recently, several studies suggested that pure silica can be effectively extracted from RHA through a combination of extraction and purification methods such as alkali leaching (Ma et al., 2012), acid leaching (Sankar et al., 2016; Schliermann et al., 2018) and thermal treatment (Bakar et al., 2016; Beidaghy Dizaji et al. 2022a; Beidaghy Dizaji et al., 2022b). Singh et al., (2022) reported that if rice husk is calcined below 900℃, then amorphous silica is produced; whereas if calcination temperature rises above 900℃, crystalline silica is produced. Chun et al.*,* (2020) burned RHA at 900℃ for 12 h after sulfuric acid pretreatment to produce ordered mesoporous nano-silica particles with 5.0 M NaOH. Azat et al., (2019) produced 98.7% pure silica with 625  $\text{m}^2/\text{g}$  surface area from RHA by leaching with 2.0 M NaOH at 90°C for 2 h. 89% silica yield was found with two-stage continuous processes and 79% with a single-stage when RHA was treated with 0.2 M NaOH at 80℃ for 3 h (Park et al., 2021). After extraction, the precipitate was calcined 85 at 900 °C for 6 h to produce 98.5% pure silica with a surface area of 1.973  $\text{m}^2/\text{g}$ . Another study reported a 91% yield with 93% purity of silica obtained from RHA with 1.0 M NaOH for 1 h (Kalapathy et al., 2000). They used 660℃ temperatures for 8 h to convert rice husk to ash. Similarly, Ma et al., (2012) prepared silica powder when RHA collected from a power plant was 89 heated at 120 °C with 4.0 M NH<sub>4</sub>F for 3 h with a conversion yield of 94.6%. Therefore, all processes used pre-calcination or post-calcination techniques to extract and purify silica from RHA.

 Literature shows that controlled burning or calcination processes were carried out by changing the temperature (post calcination) as well as the use of alkali before or after extraction. Therefore, this study aims to extract silica from RHA via a non-post calcination or carbonization method by collecting the RHA from a local rice processing mill. This process leads to the low-cost and less energy-intensive and sustainable production of pure silica from RHA. In addition, the extracted silica was then applied as a natural adsorbent to remove organic pollutants such as methylene blue dye from the aqueous solution.

## **2. Materials and Methods**

### **2.1. Materials**

 Rice husk ash (RHA) was collected from the Tungipara Rice Processing Mill, Gopalganj, Bangladesh. All the reagents used in this study were of analytical grade. Sulfuric acid (98%) and sodium hydroxide pellets were purchased from Merck Specialties Private Limited, India.

**2.2. Pretreatment of RHA**

 Incompletely burned RHA is separated using a 45-mesh sieve, and there present no visible slag in the collected sample. After sieving, half of the total ash was washed using water, and another half was washed with 0.5N H2SO<sup>4</sup> acid with constant stirring at 40℃. A magnetic stirrer hotplate (Scilogex Magnetic Stirrer with hot plate, model MS7-H550-Pro, USA) was used for heating and stirring. After acid washing, RHA samples were neutralized to pH 7 by washing them with distilled water. Washed samples were dried at 80℃ for 12 h, and stored in zip-lock bags at room temperature (**Figure 1**). Silica produced from water-washed RHA was denoted as WW\_RHA, and silica produced from acid-washed RHA was denoted as AW\_RHA.

### **2.3. Silica preparation from RHA**

114 Pretreated RHA was leached at a constant temperature (105<sup>o</sup>C) and varying the time from 0.5 h to 3.0 h in the presence of 3.0 M NaOH. To do so, 5 g ash was weighed and placed in a flat- bottomed flask with 100 ml 3 M NaOH. At the end of the experiments, the sodium silicate and leachate solution were separated from insoluble residue using Whatman filter paper 125 mm 118 Grade-1. Then the separated solution was neutralized to pH 7 with 3 M  $H_2SO_4$  solution with continuous stirring, and allowed to stand overnight to precipitate silicic acid (**Figure 1**). The precipitated product was collected and washed thoroughly with distilled water to remove any unwanted water-soluble salt and clouds of dust. After washing, the final product was dried at 80°C for 24 h for converting silicic acid to pure silica; and stored in an airtight sample holder for further use.

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## **"Figure 1"**

## **2.4. Characterizations of silica**

 The surface morphology of produced silica was observed by employing field emission scanning electron microscopy (FESEM, JSM-7610F, JEOL, Japan). Energy dispersive spectroscopy (EDS; 7610F, JEOL, Japan) coupled with FESEM was used to identify the presence of corresponding elements in silica samples. SEM-EDS analysis was performed under a low- pressure vacuum with a processing time of 3.25 s, beam accelerating voltage of 15 kV at beam aperture of 6 mm, with a working distance of 7.6 mm, magnification of 2000, probe current of 1.0 134 nA, and EDX count rate at  $1400 \pm 200$  cps. X-ray fluorescence (XRF) was done using SHIMADZU ED-XRF (EDX-8000, Japan) to determine the chemical compositions of the initial RHA and

 Rigaku WD-XRF (ZSX Primus IV, Japan) to determine the chemical compositions of the produced silica. XRF was done taking a 0.2 g sample, pressing pressure of 10 lb, and 3 minutes of palletization time. X-ray diffraction (XRD) patterns of silica from WW\_RHA and silica from AW\_RHA were recorded using Rigaku AC 2021 (Japan) X-Ray diffractometer using Kβ filter 1D for Cu and HyPix-400 (horizontal) detector operated at 50 mA and 40 kV at a scan rate of 20 °/min 141 in the 2 $\theta$  range of 5-30°. FTIR spectra identified the functional groups present in SiO<sub>2</sub> precipitate. An IR Prestige 21 FTIR (SHIMADZU, Japan) spectrometer was used with the ATR technique at 143 a spectral range from 700 to  $1400 \text{ cm}^{-1}$  for 30 scans at a speed of 4 cms<sup>-1</sup>. The Brunauer-Emmett-144 Teller (BET) surface area of silica was determined from  $N_2$  adsorption measurements using BET-145 201-A Sorptometer (PMI, USA). N<sub>2</sub> adsorption/desorption isotherms were recorded in the range 146 of relative pressures,  $P/P_0$ , from 0.0 to 0.977. To remove any moisture or adsorbed contaminants, 147 samples were outgassed to 20 microns vacuum overnight at 120 °C before measurements.

## **2.5. Adsorption of organic dye using extracted silica**

 The stock solution of methylene blue (MB) was prepared with distilled water. Firstly, we studied the effect of pH on dye adsorption. To do so, the pH was adjusted from 2 to 12, using 0.1 M HCl and 0.1 M NaOH solutions at room temperature before adsorption experiments were carried out for 6 h to determine sorption capacity at equilibrium. HI-2211 Bench-type pH meter was used for measuring the pH of the solution. Before measuring the pH of the solution, the pH meter was calibrated using buffer solutions of pH 4 and 7 (BDH). The effect of pH on adsorption was studied for both acid-washed and water-washed silica. The absorbance of each test solution was measured before and after performing the adsorption at 660 nm using T 92+ Double Beam UV-Vis Spectrophotometer (PG Instrument, UK). Then we carried out the kinetics experiment to determine the equilibrium time of adsorption for both acid-washed and water-washed silica. The

 kinetics studies were carried out for up to 240 minutes. For each type of silica, the initial concentration of MB was 1000 mg/L, and the adsorbent amount was 0.25 g. Starting from 5 minutes, the sample was taken at regular intervals, and absorbance was measured to determine the equilibrium concentration and amount adsorbed at equilibrium. The adsorption process reached an equilibrium around 60 minutes. The pseudo-first-order (PFO) kinetic model (equation 1) and the pseudo-second-order (PSO) (equation 2) were fitted to the experimental data.

165 
$$
PFO: Q_1 = Q_e (1 - e^{-K_1 t}) \dots \dots \dots \dots (1)
$$

166 
$$
PSO: Q_2 = \frac{K_2 Q_e^2 t}{1 + K_2 Q_e^2 t} \dots \dots \dots \dots (2)
$$

167 where  $Q_e$  (mg/g) is the adsorption amount at equilibrium, and  $K_1$  (min<sup>-1</sup>) and  $K_2$  (mg<sup>-1</sup>min<sup>-1</sup>) 168 are PFO and PSO kinetic rate constant, respectively. These parameters were estimated by nonlinear 169 regression weighted by the dependent variables.

 Then adsorption isotherm experiments were conducted by adding 0.25 g of silica to 100 ml of MB solution in a conical flask. The initial concentrations of MB were kept within 100 to 500 mg/L. The mixtures were kept at room temperature with constant stirring for 60 minutes at pH 8 (as higher adsorption capacity was found at this pH). Two standard sorption models called Langmuir and Freundlich isotherm models were used to fit the experimental data.

175 The apparent sorption distribution coefficient  $(K_d, L/kg)$  is defined as the ratio of adsorbate 176 sorbed per unit sorbent mass  $(Q_e, mg/g)$  to adsorbate concentration in solution  $(C_e, mg/L)$  at 177 equilibrium and was calculated using Eq. (3):

178 
$$
K_d = 1000 \frac{Q_e}{C_e} = 1000 \frac{V}{M} \left( \frac{C_0 - C_e}{C_e} \right) \dots \dots \dots \dots \dots (3)
$$

179 where V is the solution volume (L),  $C_0$  is the initial adsorbate concentration in water (mg/L), and M (g) is the sorbent mass. The Langmuir and Freundlich isotherm models can be represented as follows:

182 **Freundlich model:** 
$$
Q_e = K_F C_e^{1/n}
$$
 .... ... .... ... (4)

183 Language. 
$$
\text{Langmuir model: } Q_e = \frac{Q_{\text{max}} K_L C_e}{1 + K_L C_e} \dots \dots \dots \dots \dots (5)
$$

184 where  $Q_{\text{max}}$  is the maximum adsorption capacity (mg/gm),  $K_F$  is the Freundlich capacity-185 affinity coefficient (mg<sup>1-n</sup>L<sup>n</sup>g<sup>-1</sup>), 1/n is a dimensionless number related to surface heterogeneity, and K<sub>L</sub> is the Langmuir fitting parameter ( $\text{Lmg}^{-1}$ ). Parameters were estimated using the above equations and fitting in Origin pro software by nonlinear regression weighted by the dependent variable.

## **3. Results and discussion**

## **3.1. Mechanism of silica extraction from RHA**

 The silica production process from RHA involves two steps (Chun and Lee, 2020). Firstly, the leaching of silica from RHA to the solution, and secondly, silica precipitation. Previous studies indicate that amorphous silica is soluble in an alkaline medium when pH was increased above pH 9 (Alexander et al., 1954). As the average process temperature for the production of RHA in the rice processing mill is below 650℃, therefore according to the literature it contained mainly amorphous silica. When RHA is treated with NaOH solution, silica from RHA dissolves by 198 forming  $Na<sub>2</sub>SiO<sub>3</sub> according to the following chemical reaction 6:$ 

$$
2NaOH + SiO2(ash) \rightarrow Na2SiO3 + H2O ... ... ... ... (6)
$$

 The solubility of silica increases with the increase in pH; therefore, lowering the pH or neutralizing the alkaline silicate solution is the essential requirement for precipitating silica from the solution. Sulfuric acid is a standard method for neutralizing the sodium silicate solution for silica precipitation (Soltani et al., 2015). Following reaction-7 involves this process:

# Na<sub>2</sub>SiO<sub>3</sub> + H<sub>2</sub>SO<sub>4</sub>  $\rightarrow$  SiO<sub>2</sub>  $\downarrow$  + Na<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O … … … … (7)

**3.2. Chemical composition of initial RHA**

 The chemical composition of the initial RHA and extracted silica was examined by Energy Dispersive X-ray Fluorescence (ED-XRF) spectroscopic measurement. The RHA used in this 208 study contains: SiO<sub>2</sub> (90.990%), Al<sub>2</sub>O<sub>3</sub> (3.982%), K<sub>2</sub>O (1.864%), CaO (1.811%), Fe<sub>2</sub>O<sub>3</sub> (0.496%), SO<sup>3</sup> (0.307%), Cl (0.302%), MgO (0.140%), and ZnO (0.029%); and it undergoes 3.103% weight 210 loss on ignition. The results from ED-XRF analysis (**Table 1**) show that  $SiO<sub>2</sub>$  was the main component of the siliceous precipitate, and the contents of various metal oxide impurities were low. In our case, the purity of silica produced from RHA by avoiding calcination was 96.3% and 94.0% for silica from WW\_RHA and silica from AW\_RHA, respectively. The obtained silica masses were 94-96.3% for silica extracted via acid and water washed. It is noticeable that although pre-carbonization or post-carbonization was not used, our results showed a higher amount of silica present in the final composition. Whereas, many studies of silica extraction from RHA were 217 carried out using pre- or post-calcination methods involving high temperature (above  $600^{\circ}$ C), with a slightly better percentage of silica content in the final products (i.e., 93-98%) (Azat et al., 2019; Bakar et al., 2016; Chun et al., 2020). For example, Park et al., (2021) obtained 98.5% silica from RHA, but they calcined their samples after the extraction process to obtain the final product. More comparison is listed in **Table 1**. In contrast, we used RHA produced from burning rice husk in an open environment to heat the boiler in local rice processing mills and avoid further calcination



 increase in dissolution time up to 2 h for both water-washed and sulfuric acid-washed RHA. Over 2 h of reaction time, the percentage yield does not increase significantly. The yield percentage of silica produced from water-washed and acid-washed RHA was 71.71% and 72.44%, respectively for 2 h reaction time and without further calcination. Therefore, the optimum time of silica extraction from RHA was 2 h at 105℃ by using 3.0 M NaOH solution and constant stirring. On the other hand, Park et al., (2021) reported 79.9% silica yield by using 0.5 M NaOH for 3 h reaction time in 80℃, but they calcined the precipitated silica at 900℃ for 6 h for the final product. Similarly, Azat et al., (2019) extracted silica from RHA after 2 h of reaction time with 2 M NaOH at 90℃, but they calcined the sample at 600℃ before alkali extraction. Therefore, our method of silica extraction from RHA involves lower energy consumption than other methods.

**3.5. FTIR analysis of produced silica**

257 **Figure 3(b)** presents the FTIR-ATR spectra to identify functional groups of produced SiO<sub>2</sub> 258 from RHA data between 700 to  $1400 \text{ cm}^{-1}$  for silica from WW\_RHA and silica from AW\_RHA. 259 The literature shows that the absorption band for  $SiO<sub>2</sub>$  is known to be within the wavenumber 260 range of  $1000-1100 \text{ cm}^{-1}$  (Post et al., 2018). The IR spectra at the ranges 778-799 and 1035-1125 261 cm<sup>-1</sup> could be attributed to stretching, and asymmetrical stretching vibration of Si-O-Si (Prempeh et al., 2021). For example, Melendez et al., (2014) reported Si-O-Si stretching and bending 263 vibration peaks at  $1058 \text{ cm}^{-1}$  and  $800 \text{ cm}^{-1}$ . RHA-derived amorphous silica shows absorption 264 stretching vibration peaks at  $1055 \text{ cm}^{-1}$  (Azat et al., 2019); and  $1051 \text{ cm}^{-1}$  (Umeda and Kondoh, 2010)*.* Widjonarko and Kartini (2014)*,* found the presence of both asymmetric siloxane (Si-O-Si) and symmetric siloxane (Si-O-Si) in pure silica gel, confirmed by FTIR absorption peaks at 1087 cm<sup>-1</sup> and 802 cm<sup>-1</sup>, respectively. Singh et al., (2022) found the symmetric and asymmetric 268 stretching vibration of the Si-O-Si bond at 794  $cm^{-1}$  and 1109  $cm^{-1}$  for amorphous silica

269 nanoparticles. **Figure 3(b)** shows the absorption peaks in this study are found at  $1057 \text{ cm}^{-1}$  and  $783 \text{ cm}^{-1}$  for silica from WW\_RHA; and 1053 cm<sup>-1</sup> and 802 cm<sup>-1</sup> for silica from AW\_RHA, respectively. These peaks indicate a highly condensed silica network containing mainly asymmetric siloxane (Si-O-Si) together with some symmetric siloxane (Si-O-Si) in the produced silica from RHA without calcination. Due to removing acid-soluble impurities, silica from AW\_RHA possesses much higher absorbance than silica from WW\_RHA in the asymmetric siloxane region, where both possess approximately the same absorbance in the symmetric siloxane region. Therefore, it is clear that acid pretreatment affects mainly the asymmetric siloxane network in silica.

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## **"Figure 3"**

## **3.6. XRD analysis of produced silica**

282 The crystallinity of produced silica from WW\_RHA and silica from AW\_RHA was investigated using XRD spectra, and corresponding data were plotted in **Figure 3(c)**. Beidaghy Dizaji et al. (2019) summarized that the crystallization temperature shifts to higher values from 600℃ to about 1000℃ when RHA is pretreated with different chemicals. The removal of alkali metal content in pre-treatment is the reason for this shift. Azat et al., (2019) found a broad diffused 287 peak in XRD with a maximum intensity at  $2\theta = 22^{\circ}$  with the corresponding d-spacing value of 0.36 288 nm which confirmed the amorphous nature of produced silica from RHA when calcined at 600 °C. 289 Park et al., (2021) found broad diffraction at  $2\theta=20^\circ$  for RH-derived silica while calcined at 900°C. In this study, without any calcination, we found broad diffused peaks with a maximum intensity 291 at  $2\theta = 21.7^\circ$  for silica from WW\_RHA, and at  $2\theta = 22^\circ$  for silica from AW\_RHA, respectively.

 These broad peaks indicate the amorphous nature of the produced silica and confirm the absence of any crystalline silica. However, the peak for WA\_RHA is slightly sharper than the peak for silica from WW\_RHA. This was due to sulfuric acid pretreatment before leaching with NaOH which removed organic compounds from the RHA. Therefore, without post calcination, our extracted silica gives similar peaks as reported in other studies.

## **3.7. Nitrogen adsorption isotherms and BET surface areas**

 The nitrogen adsorption-desorption isotherms for silica from WW\_RHA and AW\_RHA are shown in **Figures 3(d) and 3(e)**. The isotherms of silica produced from untreated and acid pretreated RHA are closer to type III isotherms, similar to the isotherms derived by Azat et al. (2019). The results were almost similar to the findings of Beidaghy Dizaji et al., (2022) and Singh et al., (2022). They found that the porosity of silica-rich ashes diminishes, once the crystallinity 303 fraction is higher than 10 wt.%. The results show that  $N_2$  adsorption on silica from AW\_RHA is higher than on silica from WW\_RHA; which is supported by the BET surface area and pore volume data. The weak hysteresis loop and curvature in low pressures indicate a mixture of mesoporous-macroporous materials. It indicates the formation of monolayers, bilayers, trilayers, and so on at the same time, resulting in an almost exponential increase in the amount of adsorption. 308 The Brunauer-Emmett-Teller (BET) specific surface area of silica was determined from  $N_2$  adsorption-desorption measurements and pore volume and pore diameter (pore size distribution) were calculated using Pierce and Barret-Joyner-Halenda (BJH) desorption methods. The specific surface area, pore volume, and average pore diameter of the produced silica from RHA are shown 312 in **Table 2** and **Figure 3f**. The  $R^2$  of BET transfer plots are 0.9998 and 0.9997, and the BET C values are 154.45 and 142.91 for AW\_RHA silica and WW\_RHA silica respectively. The BET 314 surface area (182 m<sup>2</sup>/g) found in this study was lower than that found by Bakar et al., (2016), but



 between the adsorbent and the dye molecules. To determine the effect of pH on the K*<sup>d</sup>* values for MB removal from aqueous solution by rice husk-derived silica, we studied the effect of pH ranging from 2 to 12 by taking 100 mg/L initial MB concentration at room temperature with 0.25 g adsorbent loading, and the results are depicted in **Figure 4(a)**.

**"Figure 4"** 

 The figure shows that the increase in pH from 2 to 8 caused a substantial increase in the K*<sup>d</sup>* values for MB removal for both water-washed and acid-washed silica. The adsorbent surface became negative, which enhanced the adsorption of positively charged MB dye by electrostatic attraction force, which might cause these increased K*<sup>d</sup>* values with increasing initial pH. But, after pH 8, the K*<sup>d</sup>* values decreased with an increase in pH. Because above pH 8, the adsorbent surface 345 will hold the more partial negative charge as O<sup>-</sup> in **Figure 5.** So, a repulsive force arises between the adsorbent surface and the presence of a partial negative charge of chloride ions on MB. Therefore, pH 8 is chosen as the optimum pH for further study. Literature shows that with the modification of silica adsorbent surface, the optimum pH can be between 6.8 to 11 (Adam et al., 2013; Alver et al., 2020; Hongo et al., 2021; Sharma et al., 2010). **"Figure 5"**  Adsorption of MB on silica surfaces can occur in three cases (**Figure 5**). In cases 1 and 2, electrostatic attraction between partially charged nitrogen-oxygen and partially charged sulfur- oxygen. Case 3 represents hydrogen bonding. In lower pH values, the adsorption occurs mainly by hydrogen bonding. These hydrogen bonds would be expected to occur between amino groups in the dye molecule and the silica surface hydroxyl groups. The surface becomes more ionic on

reacts with the -OH group, eliminating HCl and increasing the adsorption capacity. This

the increasing pH value to neutral pH. Deprotonation starts when the cationic methylene blue

mechanism is also supported by previous studies on pH-dependent data (Adam et al., 2013;

Chandrasekhar and

Pramada, 2006; Hongo et al., 2021).

## **3.9. Adsorption kinetics for MB removal by RHA-derived silica**

 The contact time is an essential parameter for the dye adsorption process. The effect of time on MB removal by RHA-derived silica and corresponding PFO and PSO kinetics model fitting are shown in **Figure 4(b)**. It can be seen from the figure that the maximum uptake of MB reached maximum approximately in equilibrium time of 60 minutes for both water-washed and acid- washed RHA silica which is consistent with previous studies (Azevedo et al., 2017; Chen et al., 2012). Modifying RHA with alginate increased the equilibration time to 90 minutes (Alver et al., 2020). Singh et al., (2022) used UV-C irradiation with silica nanoparticles for the degradation of methylene blue dye, and they found ~100% of degradation within the initial 30 minutes of the adsorption onto silica-nanoparticles.

 The nature of the adsorption process can be identified from the adsorption kinetics models. pseudo-first-order (PFO) and pseudo-second-order (PSO) models were used in this study to determine the adsorption process, and the calculated data were given in **Table 3**. The PFO and PSO kinetic models are well-fitted for both silica. Therefore, water-washed silica and acid-washed silica both followed PSO and PFO models indicating the role of the physisorption and the chemisorption processes (Agbovi and Wilson, 2021).

## **"Table 3"**

#### **3.10. Sorption isotherm for MB removal by RHA-derived silica**

 The Langmuir and Freundlich isotherms models were fitted for MB adsorption by RHA- derived silica. The sorption data were plotted in **Figure 4(c)** to find the best-fitted model, and 385 corresponding data were given in **Table 4**. Figure and the corresponding  $\mathbb{R}^2$  values from table 4 indicate that sorption data were well fitted with both the Langmuir isotherm model and the Freundlich isotherm model. Fitting to the Langmuir isotherm means that RHA-derived silica has homogeneous adsorbent surfaces involving monolayer adsorption processes with similar adsorption sites whereas fitting to Freundlich isotherms indicated surfaces were multilayer 390 coverings. Anyway, the  $Q_m$  values were in little agreement with the  $Q_e$  values (**Tables 3 and 4**). Previous studies of MB adsorption by RHA have found similar characteristics (Chen et al., 2012; Hongo et al., 2021), but if RHA is modified with alginate, it is better fitted with Freundlich isotherm (Alver et al., 2020).

- **"Table 4"**
- 

 We further then calculated the sorption distribution coefficient K*<sup>d</sup>* values. The K*<sup>d</sup>* values decreased with the increase in MB concentration and were plotted with the equilibrium MB 399 concentration in **Figure 4(d).** The observed values of  $Q_m$  and  $K_f$  for MB for both cases were higher than the values reported by Chen et al., (2012), Moeinian and Mehdinia (2019), and Hongo et al., (2021). Q*<sup>m</sup>* and K*<sup>f</sup>* values were lower than reported by Peres et al., (2018) and Chandrasekhar and Pramada (2006), who both used RHA directly without separating the silica. Therefore, there may also be many carbon-containing compounds that adsorb MB molecules.

### **4. Conclusions**

 This study reported a low-cost method for extracting silica from RHA, with > 94% pure mesoporous amorphous silica and a high yield conversion of > 72.3% without further calcination. 408 XRF and FTIR results show that  $SiO<sub>2</sub>$  is the major component of the siliceous precipitate with a 409 highly condensed siloxane (Si-O-Si) network structure with a surface area ranging from 165 m<sup>2</sup>/g 410 to 183 m<sup>2</sup>/g. Adsorption studies showed that 107 mg of methylene blue can be adsorbed by 1.0 g of silica produced from acid-washed RHA at pH 8 within 60 minutes. Therefore, the results demonstrate the feasibility of environment-friendly extraction of silica from RHA with a high adsorption capacity for methylene blue. This research has proved the conversion of a waste material (i.e. RHA) to a valuable product (i.e. silica) as a natural element and effective adsorbent of contaminants. As a result, this method can prevent the dumping of RHA on land and subsequent environmental pollution.

#### **Conflict of interest:**

The authors declare no conflict of interest for this study.

## **Acknowledgments**

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# **Total 5 Figures Figure 1:**



Figure 1: Schematic representation of silica production process.





**Figure 2:** SEM images and EDX analysis of the produced silica with their chemical composition.



Figure 3: (a) Effect of time on the extraction of silica from RHA. (b) FTIR spectra of produced silica. (c) X-ray diffraction spectra of produced silica. (d) Adsorption-desorption isotherm for silica from water-washed RHA. (e) Adsorption-desorption isotherm for silica from acid-washed

RHA. (f) BJH desorption pore size distribution by volume. In the figure, WW\_RHA= Water washed Rice Husk Ash; and AW\_RHA= Acid washed Rice Husk Ash.



## **Figure 4:**

**Figure 4:** (a) Effect of pH on the distribution coefficient  $(K_d)$  for methylene blue removal. (b) Sorption kinetics data with PFO and PSO kinetics model fitting. (c) Sorption isotherm plots and model fitting. (d) Change of K*<sup>d</sup>* values against equilibrium concentrations from isotherm studies.





**Figure 5:** Schematic representation of the proposed mechanism of adsorption of MB on the silica surface.

# **All Tables**

# **Total 4 Tables**

# **Table 1:**

Chemical compositions of silica from different rice husk and rice husk ash samples.





# **Table 2:**



BET specific surface area of silica produced from RHA.



# **Table 3:**



PFO and PSO kinetics data for MB adsorption on RHA.





# **Energy Efficient Extraction of Silica from Rice Husk Ash as Adsorbent for Dye Removal**

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The authors declare no conflict of interest.