Ceramics



In-situ scanning transmission electron microscopy study of Al-amorphous SiO₂ layer-SiC interface

Esmaeil Adabifiroozjaei^{1,7,*} , Ebad Rastkerdar², Yoshihiro Nemoto³, Yoshiko Nakayama³, Yuki Nishimiya³, Marco Fronzi⁴, Yin Yao⁵, Minh Triet Nguyen⁶, Leopoldo Molina-Luna¹, and Tohru S. Suzuki⁷

¹ Advanced Electron Microscopy (AEM) Division, Institute of Materials Science, Technische Universität Darmstadt, 64287 Darmstadt, Germany

² Faculty of Mechanical Engineering, Department of Materials Engineering, University of Tabriz, Tabriz 5166616471, Iran

³ Electron Microscopy Analysis Station, Nanostructural Characterization Group, National Institute for Materials Science (NIMS), Tsukuba 305-0047, Japan

⁴ IGP, SIT Laboratory, College of Engineering, Shibaura Institute of Technology, Tokyo 135-8548, Japan

⁵ Electron Microscopy Unit (EMU), UNSW Sydney, Mark Wainwright Analytical Centre, Sydney, NSW 2052, Australia

⁶ARC Center of Excellence in Exiton Science, School of Physics, UNSW Sydney, Sydney, NSW 2052, Australia

⁷ Research Center for Functional Materials (RCFM), National Institute for Materials Science (NIMS), Tsukuba 305-0047, Japan

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ABSTRACT

Here, we present a comprehensive study on atomic-scale in-situ biasing/heating scanning transmission electron microscopy ((S)TEM) of Al-amorphous SiO₂–SiC interface. The investigation includes electrical, chemical, and structural analysis of the interface at different temperatures (25–600 °C). The results show that at ~ 500 °C the electrical (three-orders of magnitude resistivity drop), chemical (dissolution of SiO₂ amorphous layer), and microstructural features (*e.g.* formation of Al₂O₃, Si and Al₄C₃) of the interface start to change. According to the results, amorphous SiO₂ dissolves in Al, leading to formation of α -Al₂O₃ and Si within the Al. In contrast, elemental interdiffusion (Al³⁺ \rightleftharpoons Si⁴⁺) between Al and SiC occurs resulting in formation of Al₄C₃. From the results, we can infer that reaction mechanism between Al and crystalline SiC is different with that between Al and SiO₂ amorphous phase. It is believed that structural similarities between SiC and Al₄C₃ play an important role in paving the way for elemental interdiffusion.

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Address correspondence to E-mail: e.adabifiroozjaei@aem.tu-darmstadt.de

Introduction

The development of materials based on novel hybrid structures, particularly those containing both metals and ceramics are of great importance in today's rapidly evolving microelectronic and manufacturing industries [1, 2]. This is because by combining the different features of the metals and the ceramics (e.g. ductility v.s. brittleness, conductivity v.s. insulating (or semiconductor) [3]), the resulting composite material could have remarkably-improved and wellbalanced properties [4-7]. Additionally, when the device is made of non-oxides (carbides or nitrides), there is an amorphous oxide layer (hereafter called AOL) between the metal and the ceramic that can potentially alter the device properties [8, 9]. Examples are, but not limited to, metal-SiC Schottky diodes [10], metal-oxide semiconductor (MOS) devices [11, 12], and metal matrix composites reinforced with non-oxides (e.g. SiC, TiC) [13]. One representative system that can be applied in all these applications is Al-SiC, in which AOL (few nanometers thin of amorphous SiO₂) always exist between Al and SiC [10, 11, 14–16]. In semiconductor devices, an annealing process at intermediate temperature is prescribed in order to make a closer contact between the metal and the ceramic component [14, 17], so as to adjust the electrical characteristics of the device [18-20]. Similar processes can be applied to Al-SiC composites, in which the annealing process enhances the composite mechanical properties by preventing direct contact between Al and SiC, which in turn stops the formation of brittle and undesired aluminum carbide phase (Al_4C_3) [15, 16, 21].

In spite of the central influence of the AOL on the metal-ceramic device properties, the mechanism of interaction of AOL, or the crystalline ceramic (SiC) with the reactive metal (Al) under the heat-treatment process is still not well-understood. Currently, there are two theories: (1) First theory suggests that amorphous and crystalline ceramics, regardless of their crystallinity, react with the metals through a similar mechanism, being ceramic dissolution into the metal (solid or liquid) and consequent crystallization of reaction product [20, 22, 23]. This is based on very limited dissolution of the reactive metal in the ceramics, which itself is according to equilibrium phase diagram of the relevant bulk system (*e.g.* Al–Si–C ternary system [24]). However, it is well-known

that for interfaces in multicomponent systems, due to the significant role of interfacial energies, a new equilibrium system different than that of existing in the bulk systems can be observed (formation of metastable complexions in various materials [25–27]). Additionally, the reactive metal-ceramic systems are very far from the chemical equilibrium, and accordingly their behavior can deviate considerably from the systems at equilibrium [28, 29]. Also, it has to be considered that decomposition of the covalent crystalline ceramics such as SiC requires substantial amount of energy and only occurs at high temperatures (at least 1000 °C) [30, 31], which are not comparable with the heat treatment temperatures of the Al-SiC composites (~ 500-650 °C) [16, 32]. In contrast to first theory, the second theory is based on interdiffusion of elements across the interface of the metal and the ceramic. This theory was applied in the previous works on Al-Si₃N₄ [33], Al-CaAl₂Si₂O₈ [34, 35], Al-BaAl₂Si₂O₈ [36, 37], and Al-MgAl₂O₄ [38] systems, in which elemental interdiffusion (e.g. $Al^{3+} \rightleftharpoons Ca^{2+}, Al^{3+} \rightleftharpoons Si^{4+}, Al^{3+} \rightleftharpoons Mg^{2+}$) across the metal-ceramic interface was proposed as the interfacial phase evolution mechanism. Furthermore, the $Al^{3+} \rightleftharpoons Si^{4+}$ interdiffusion was also considered in the past as the mechanism of interfacial phase evolution in the Al-SiC system, but due to the resolution limit (10 nm) of the microscopes, this mechanism was not confirmed [32]. Furthermore, recent studies on metalceramic interfaces showed that rate of elemental interdiffusion at the interface can be a few orders of magnitude higher than that observed in the bulk ceramics [1, 39]. The major issue is that the studies conducted so far, regardless of the mechanism proposed in them, were ex-situ and expectedly not being capable of resolving the atomic-scale nanostructural and chemical changes occurring at the interfaces during the heat-treatment process. Hence, there is still ambiguity in understanding of how reactive metal-ceramic interfaces evolve when exposed to high temperature.

Here, by the application of atomic resolution, insitu (S)TEM techniques (using Cs corrected microscopes) we reveal the evolution mechanism of the Al– AOL–SiC system under biasing/heating conditions. Our I–V curves and high resolution TEM (HRTEM) images acquired from in-situ biasing/heating test at different temperatures indicate that the resistivity of the Al–AOL–SiC device decreased three orders of magnitudes at 500 °C with no apparent change in the nanostructure. Separate in-situ heating experiment with acquisition of the STEM-HADDF (high-angle annular dark field) images and interfacial chemical profile (using EELS (energy electron loss spectroscopy)) of the elements show that at 550 °C the AOL width was reduced, which was due to AOL dissolution into the Al. The structural analysis of the interface at 600 °C confirms formation of Al₂O₃ and Si in the Al, but Al₄C₃ within the SiC with no clear boundary. Structural similarities of Al₄C₃ and SiC as well as the lack of observation of SiC dissolution into the metal lead us to conclude that elemental interdiffusion (Al³⁺ \leftrightarrows Si⁴⁺) between Al and SiC results in topotactic formation of Al₄C₃ from SiC as a precursor.

Experimental

4H n-type SiC wafer with thickness of $\sim 350 \ \mu m$ was purchased from Electronics and Materials Corporation Limited (Hyogo, Japan)). The growth direction of SiC wafer was [0001]. The main impurity in SiC was nitrogen with calculated content of 1×10^{19} atom/ cm³. The wafer was ultrasonically cleaned in acetone for few mins and then was dipped into 10 wt% HF solution for 5 min to remove the oxide layer present on SiC. Immediately after removal of the oxide layer, the SiC wafer was put in desiccator for few days in order to allow the regrowth of the oxide layer. Then, an Al layer with thickness of $\sim 1 \,\mu m$ was sputtered on the wafer. In order to decrease heating caused from sputtering process, very low sputtering speed $(\sim 1.85 \text{ Å/s})$ was used. The sputtering was applied using an i-miller stutterer (CFS-4EP-LL, Shibaura Corporation, Yokohama, Japan). Mechatronics Focused ion beam (JIB-4000, JEOL Ltd., Tokyo, Japan and JEM-9310FIB, JEOL Ltd., Tokyo, Japan) milling was used to prepare the lamellae. Similar lamellae were prepared, some of which was used for in-situ biasing/heating experiment and the other ones for insitu heating. DENSsolutions lightning nano-chip was used for in-situ biasing/heating experiment (Fig. 1a). The prepared lamella was loaded on the chip using micromanipulator. The low- and high-magnification scanning electron microscopy (SEM) images of the chip and the loaded lamella are shown in Fig. 1b, c. Lamella was glued to chip using epoxy resin. Then, two Au lamellae were prepared by FIB and connected to Al-AOL-SiC lamella and chip. This was to ensure electrical current passes through Al-AOL-SiC lamella. No glue was used for connection of Au lamellae and Al–AOL–SiC lamella. For in-situ heating experiment DENSsolutions nano-chip was used (Fig. 1d). The low- and high-magnification optical microscopy (OM) images of the chip and the loaded lamella are shown in Fig. 1e, f. Here, only epoxy was used to ensure that the lamellae is tightly bonded to the chip.

For the in-situ biasing/heating experiment, a DENSsolutions Lightning holder (DENSsolutions B.V., Delft, The Netherlands) was used. To regulate the heating and biasing, both DENSsolutions Lightning heating and Protochips Fusion electric biasing systems (Protochips Inc., Morrisville, NC, USA) were used. The prepared lamella was loaded on a DENSsolutions Lightning chip, and a compliance current of 3 nA was applied. Then the voltage required to reach such a current was recorded at each temperature. The temperature was increased from room temperature to 600 °C with an interval of 100 °C and holding time of 30 min at each temperature. Between 500 and 600 °C the interval was set to 50 °C. The I-V curves were measured at each temperature over the holding time and any changes or variations were recorded. After finishing the characterization at 600 °C, the sample was cooled down to room temperature. The change in the microstructure of the interface was recorded in TEM mode by imaging and capturing movies. For imaging, $1\overline{1}00$ zone axis was chosen for SiC single crystal. Since sputtered Al is formed as polycrystalline, closest zone axis of a grain of Al to $1\overline{100}$ zone axis of SiC was found and all analysis were done accordingly.

In-situ heating test was done using the same holder, but on a DENS solutions Wildfire chip. Heating procedure was same as biasing/heating test. Microstructural analysis was done in the STEM mode. EELS was conducted to measure the chemical profile of the different elements across the interface. The resolution of the EELS line analysis was 4 Å. K-edges of Al, Si, O, and C were used in order to acquire the chemical profiles. Same edges were used for obtaining elemental maps, however, elemental mapping seemed to damage/change the lamella. Therefore, the chemical changes occurring at the interface were only characterized using the line chemical profiles acquired from EELS. At each temperature, the line profile measurements were recorded. In order to record the change in the microstructure, HAADF (High-Angle Annular Dark Field) imaging was done at each temperature. The imaging was done when holding time was over. EDS mapping measurements was also done to characterize the AOL layer before doing the tests. The thickness of lamellae was measured using EELS. The insitu tests were done using JEM-ARM200F (Cold FEG and 2 Cs correctors (CL and OL)) machine (JEOL Ltd. Tokyo, Japan).

Results

Before starting the in-situ tests, the microstructure and the thickness of the lamellae were studied, as they are important factors in obtaining high quality in-situ TEM data. Figure 2a shows a low-mag bright field TEM image of a prepared lamella. The middle part of lamella was further thinned compared to the sides, as this would be the area of interest. No bending contours are observed in the "analyzed area", indicating a high-quality lamella. Figure 2b shows a STEM image of a small part of the analyzed area, showing the Al–AOL–SiC interface. The graphic plot shows the variation of thickness of the lamella across the interface. The thickness of the SiC part of the lamella is ~ 100 nm, while that on Al side is ~ 80 nm.

The chemical composition of the phases across the Al–AOL–SiC interface was also studied. EDS mapping of the interface is shown as Fig. 3a, while high resolution EELS elemental mapping of the interface is given as Fig. 3b. In Fig. 3a, b, the presence of a narrow layer of oxide layer is visible. The thickness of the layer is in the range of 3–5 nm and it is consistently present everywhere along the interface. As seen from the EELS chemical profile, the layer does not have a sharp profile, meaning that the layer is not pure SiO₂.

The electrical characteristics of the lamella was studied using the in-situ biasing/heating TEM test. The acquired I–V curves for room temperature, 500° and 600° C after 30 min of application of the field are presented in Fig. 4a–c, respectively. The curves for 100° and 400° C are presented as Fig. S1. The applied compliance current was set to 3 nA (vertical axis) and accordingly the voltage (horizontal axis) required to reach to such current was recorded at each temperature. As seen, the voltage required to reach the set current is same for temperatures lower than 500° C,

while at this temperature it decreases drastically (three orders of magnitude) and stays the same at 600 °C. Since the current is set, the decrease in voltage implies that the resistivity of the device is decreased in same orders of magnitude as the decrease in the voltage. The resistivity reduction possibly implies to closer contact of the Al and SiC, meaning that AOL width was reduced or alternatively the AOL layer was locally removed through the interfacial reaction with the metal. Such situation will result in change of chemical bonding of the phases involved at the interface [14, 17, 18]. To evaluate the nanostructure of the Al-AOL-SiC interface, the HRTEM images of investigated area of the interface are given as Fig. 4 d-f for room temperature, 500 ° and 600 °C, respectively. The FFT of the HRTEM images is also presented as insets in these figures (see low-magnification images in Fig. S2). Low- and high-magnification TEM images of the device at 100 ° and 400 °C are also shown as Fig. S3. The HRTEM images and related FFTs do not indicate significant changes in the interface nanostructure, particularly the hallow pattern of the amorphous layer stays the same over the heat-treatment process. Since the length of the interface in the lamella is $\sim 15 \,\mu\text{m}$, there is a high chance that the expected structural changes occurred at other points of the interface and therefore were missed in our observation. To explore the possibility, two movies (Movie S1: low-magnification, and Movie S2: highmagnification) were captured along the interface at 600 °C. But, no significant changes were observed in the structure of the AOL. Another reason for missing the structural changes could be that the experiment was done in TEM mode, which is a phase contrast imaging mode and obviously being focus-dependent. Moreover, since the experiment was done in TEM mode, we could not do accurate in-situ chemical measurements.

Therefore, the chemical changes occurring at the interface during the heating process were investigated on another lamella (see Fig. 1e, f) through doing in-situ heating test with no bias application. HAADF-STEM images + EELS chemical profiles (see Fig. S4 for position of STEM and EELS investigation) were acquired and the results are shown as Fig. 5. As seen, the chemical profiles are basically same for the nanostructures at room temperature and 500 °C indicating that no considerable chemical variation occurred. However, at 550 °C the oxygen (O) peak of





Figure 1 a DENSsolutions lightning nano-chip for in-situ biasing/ heating experiment, **b** and **c** low- and high-magnification scanning electron microscopy (SEM) images of loaded lamella on chip,

AOL layer starts to flatten. At 600 °C oxygen seems to be uniformly spread in the AOL and Al phases, showing that O diffused in Al from AOL. Simultaneously the AOL width is reduced. Reduction of AOL width can be directly related to the decrease of the resistivity observed in the system (see I-V curves in Fig. 1). Recent nanoscale scanning spreading resistance microscopy analysis of SiO₂ amorphous layer/4H-SiC interface indicated that the carrier concentration in SiO₂ amorphous layer (10^{16} cm⁻³) is three orders of magnitudes lower than 4H-SiC $(10^{19} \text{ cm}^{-3})$ [40]. This is in same scale as the order of magnitude of resistivity drop observed in our experiment. It is well-known that O dissolution in Al is greatly limited at temperatures ~ 660 °C (melting point of Al). Data collected by Wriedt [41] shows that only 2.9×10^{-8} at% of O can be dissolved in Al at its

respectively. **d** DENSsolutions nano-chip for in-situ heating experiment, **e** and **f** low- and high-magnification optical microscopy (OM) images of loaded lamella, respectively.

liquid state (~ 660 °C). The value for our system at 600 °C and at solid state will be slightly lower. Accordingly, it is expected that in Al side and at points close to the interface, alumina (Al₂O₃) forms and simultaneously Si is inserted in the Al [42]. Our line chemical profile with point resolution of 4 Å indicate significant change neither in the profile of Si nor Al in both sides of the device. Since the thickness of analyzed area is very thin (4 Å), there is a high possibility that such Si or Al₂O₃ formation occurred at other points near the interface.

Hence, the possibility of new phase formation was explored through analyzing the structural changes at the interface nanostructure. This was done using the BF (bright field)-STEM images (Fig. 6) of the corresponding HAADF-STEM images given in Fig. 5. The Fast Fourier Transformed (FFT) images of the **Analyzed Area**

(a)





Figure 2 a Low-magnification bright field TEM image of prepared Al–AOL–SiC lamella, b High-magnification STEM image of Al–AOL–SiC interface. Inset in b shows thickness of lamella in Al and SiC areas. Lamella thickness was measured using EELS.



Figure 3 a EDS elemental mapping of Al–AOL–SiC interface, showing presence of AOL, b STEM-HAADF image of Al–AOL–SiC interface and its EELS map profile. Width and length of mapped area are 1.8 and 32 nm, respectively.

interface nanostructures are also presented in the Fig. 6. According to Figs. 6a, b and their FFTs, no additional phases were formed due to heating from room temperature to 500 °C. At 550 °C (Fig. 6c) the AOL thickness becomes smaller (~ 2 nm) and therefore Al and SiC grains will expand to occupy the AOL layer. Considering the initial thickness of Al (~ 1 μ m) and SiC (~ 3.5 μ m) layers and their thermal expansion coefficients, being 24 × 10⁻⁶ and 2.77 × 10⁻⁶ m/m °C [28], their expansions will be ~ 132 and 152 nm, respectively. At 600 °C (Fig. 6d) new reflections appear in the nanostructure. This is further investigated through inversing

individual reflexes of each phase in the FFT pattern of Fig. 6d, and the results are shown as Fig. 7. In the IFFT images, the location of each phase can be found out through locating the brighter contrast. As seen, apart from the original phases (Al and SiC), there are now three new set of reflexes that belongs to Si, α -Al₂O₃ and Al₄C₃ phases. Si and α -Al₂O₃ are formed adjacent to one another in the Al side, while Al₄C₃ is formed adjacent to the interface in the SiC side. The fact that α -Al₂O₃ and Si are crystallized within the Al implies that AOL dissociates into its elemental form (Si and O), as is expected according to previous studies [43, 44]. After reaching to saturation level O





Figure 4 a, b, and c I–V curves of Al–AOL–SiC interface measured at room temperature (25°), 500° and 600 °C, respectively. d, e, and f high-magnification images of Al–AOL–SiC interface from a small area of low-magnification images

reacts with Al to form α -Al₂O₃, while Si will precipitate as Si nanocrystallite. In contrast to α -Al₂O₃ and Si, Al₄C₃ is formed within SiC with orientation relationship of (0004)_{SiC} || (0006)_{Al4C3}. The d-spacing of (0006)_{Al4C3} was found to be ~ 4.00 Å, while according to Al₄C₃ structure it has to be 4.18 Å [45], indicating that Al₄C₃ nanocrystallite is possibly defective.

Discussions

As discussed before, the reaction of ceramics with metals can proceed through two different paths; (1) dissolution of the ceramic into the metal, and (2) elemental interdiffusion between the elements at the ceramic–metal interface. In the former, the elements from the ceramic dissolve into the metal and when the elements reach their saturation level the formation of new products occurs in the metal. In this study, since we observed the disappearance of AOL

(yellow squares in Fig. S2). FFT image of nanostructures shown in d, e, and f are presented as insets in same figures. Stacking of phases in all figures are similar (bottom: SiC, middle: AOL, top: Al). Scale bar in d applies also to e and f.

with increase in the temperature, and additionally Si and α -Al₂O₃ are formed in the Al, we infer that AOL, which is an amorphous phase, follows the first path. Such path for pure amorphous SiO₂ and consequent formation of Al₂O₃ and Si can be described as follows:

Step 1: Bond breakage $SiO_2 \text{ (amorphous)} \rightleftharpoons Si^{4+} + 2O^{2-}$ Step 2: Dissolution $Si^{4+} + 2O^{2-} \rightleftharpoons Si_{\text{dissolved in Al}} + 2O_{\text{dissolved in Al}}$ Step 3: Reaction $2Al + 3O_{\text{dissolved in Al}} \rightleftarrows Al_2O_3$

On the other hand, Al_4C_3 was formed within the SiC phase with a certain orientation relationship $((0004)_{SiC} | | (0006)_{Al4C3})$. In the previous research on a similar system (ex-situ TEM investigation on Al-

Figure 5 a, b, c and d show changes in chemistry (line profiles of Al (Aqua), Si (Violet), C (Lime), and O (Yellow)) of Al-AOL-SiC interface at room temperature (25°), 550°, 500° and 600 °C, respectively. White area in the AOL are Ga contamination due to FIB milling. Scale bar in a applies also to **b**, **c**, and **d**.



Si₃N₄ [33]), Adabifiroozjaei observed similar orientation relationship ((0001)_{AIN} \mid | (0001)_{Si3N4})) between the reaction product (AlN) and the ceramic reactant (Si_3N_4) . Therefore, it was inferred that the reaction product is formed from the reactant through an elemental interdiffusion $(Al^{3+} \rightleftharpoons Si^{4+})$ between the metal and the reactant ceramic. In fact, the ceramic reactant acted as a precursor for the reaction product, meaning that after interdiffusion the reactant transforms topotaxially to the reaction product, as this is observed in many ceramic systems with structural similarities [46]. In this study, the in-situ observation of the formation of Al₄C₃ within the SiC without destruction of SiC structure enabled us to conclude that in Al-SiC system interdiffusion of Al and Si at the interface is required to proceed the interfacial reaction. The interdiffusion path for reaction between Al and SiC involves three steps, as described below:

Step 1: Activation

Al + SiC ≈ Al_{with activated atoms} + SiC with activated atoms Step 2: Interdiffusion (I) 4Al with activated atoms + $4SiC_{with activated atoms} \rightleftharpoons Al_4C_3$ with SiC structure + 4Si dissolved in Al + C dissolved in Al Step 3: Phase transformation Al_4C_3 with SiC structure $\rightleftharpoons Al_4C_3$ with Al4C3 structure



Figure 6 a, b, c, and **d** HRTEM and their corresponding FFT images of Al–AOL–SiC interface at room temperature (25°), 550°, 500° and 600 °C, respectively. Reflections of each phase are color-

The observed difference between the *d*-spacing of Al₄C₃ crystallite characterized in the present study relative to perfect Al₄C₃ structure is due to the fact that there are some C vacancies $(V_{\text{CinSiC}}^{\prime\prime\prime\prime})$ in the Al_4C_3 crystallite as suggested by the above defect equilibria. This implies that the Step 3 (phase transformation) is not yet finished in the present study (Fig. 6d). It is expected that when Step 3 is finished, due to density difference of Al₄C₃ (2.93 g/cm³) and SiC (3.16 g/ cm³), the former gets separated from the latter as a nanocrystallite with distinct boundaries. At the end, when heat-treatment process is continued for considerable amount of time, these nanocrystallites will join and form larger grains that might or might not have orientation relationship with the reactant ceramic [25, 28].

coded. MF in FFT of c stands for Moiré fringes that appears due to overlay of two Al grains at grain boundary area. Scale bar in a applies also to \mathbf{b} , \mathbf{c} , and \mathbf{d} .

Our results clearly show that SiO₂ amorphous phase has different reaction mechanism with Al than the crystalline SiC. As mentioned before, the current theories suggest that reaction between metals and follow dissolution ceramics can either the [22, 23, 28, 47] or the interdiffusion path [33–38]. The reason behind the different reaction mechanism for SiO₂ amorphous phase and SiC can be explained using the structural similarities of reaction products and the reactants for the crystalline ceramics. This was hypothesized in the previous study on crystalline oxides (CaAl₂Si₂O₈-Al system [35]) and subsequently was applied to the Al-Si₃N₄ system [33]. In Ref. [35], it is suggested that because of close structural similarity between the reactant ceramic $(CaAl_2Si_2O_8)$ and the reaction product $(CaAl_4O_7)$, the



Figure 7 Phase configuration observed in Fig. 6d, deconvoluted using FFT and inverse FFT images.

space group of the latter (C2/c) being subgroup of the space group of the former $(P\overline{1})$, then CaAl₄O₇ is merely formed through an elemental interdiffusion $(Al^{3+} \rightleftharpoons Ca^{2+} \text{ and } Al^{3+} \rightleftharpoons Si^{4+})$ between $CaAl_2Si_2O_8$ and Al. This is particularly relevant when the cations in the metal and ceramics are not very different in their sizes (e.g. Si crystal radius: 0.4 Å and Al crystal radius: 0.53 Å), as they create nearly same surrounding environment with common anion (e.g. C, N, or O). Regarding Al-SiC system, Fig. 8 presents similarities of the atomic arrangement of SiC (reactant) and Al_4C_3 (reaction product). The arrangement of the cations (Al and Si) in both structures is very alike. Further, the lattice parameters of SiC (a = b = 3.079 $\dot{A}_{,c} = 10.082 \ \dot{A}_{,c}$ and Al_4C_3 ($a = b = 3.354 \ \dot{A}_{,c}$ c = 25.116 Å), and space groups (SiC: P6₃mc, Al₄C₃: R3m) are very close. c in Al₄C₃ is ~ 2.5 larger than c in SiC. Therefore, the similarity of the structures paves the way for reaction to proceed through elemental interdiffusion. On the other hand, the dissociation occurs for AOL since there does not exist such structural similarities between α -Al₂O₃ and AOL (amorphous SiO₂).

Conclusion

Through careful device preparation of a representative reactive metal-ceramic system (Al-AOL-SiC) and consequent presentation of a comprehensive ultrahigh-resolution electrical, chemical and structural data aqcuired by in-situ TEM and STEM techniques we elaborate that reaction mechanisms between Al and SiO₂ amorphous layer is different from that between Al and SiC. The reaction between SiC and Al proceed through elemental interdiffusions, while that between SiO₂ and Al follows the dissolution mechanism. Additionally, we hypothesize that the elemental diffusions are encouraged due to similarities of atomic arrangements in the reactant (SiC) and reaction product (Al_4C_3) structures. Our findings might be applicable to other reactive metalscrystalline ceramics systems that are currently used in manufacturing and electronic industries.





Figure 8 a and b SiC structures in [0001] and [1000] directions, respectively, and c and d Al_4C_3 structures in [0001] and [1000] directions, respectively. SiC structure is $2 \times 2 \times 2.5$ supercell, while that of Al_4C_3 is a $2 \times 2 \times 1$ supercell. Al (Aqua), Si (Violet), C (Lime). Hexagons are superimposed on structures to show similarities of atomic arrangements. Structures are visualized using VESTA visualization program.

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Data availability

The data used in this study are available from the corresponding author (e.adabifiroozjaei@aem.tu-darmstadt.de) upon reasonable request.

Declarations

Competing interests The authors declare no competing interests.

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