

25 **Closure to “Enhancing Rail Track Performance Using Recycled Rubber Energy Absorbing**
26 **Grids: Laboratory and Field Evidence”**

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35 **Authors’ Response:**

36 The authors would like to express their appreciation for the feedback provided by the Discusser, and
37 for raising some relevant discussion points. While the Authors are generally in agreement with the
38 Discusser’s comments, some points warrant further clarification as highlighted and elaborated below:

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40 ***Measured Lateral and Vertical Deformation of Ballast***

41 The discussor makes a valid observation, which the Authors fully acknowledge. A woven geotextile
42 was indeed placed at the ballast–capping interface in the large-scale cyclic loading test program. This
43 fabric was used consistently in all tests, both with and without the REAG, to ensure comparable
44 boundary conditions. The woven fabric served primarily to prevent ballast particles from penetrating
45 into the capping layer and to minimize the upward migration of fine particles from the capping layer
46 into the ballast. The Discusser is also correct in noting that if nonwoven geotextiles had been used
47 instead of woven ones, there would have been a higher likelihood of puncture by the ballast particles,
48 since woven geotextiles typically exhibit greater tensile strength and puncture resistance than
49 nonwoven alternatives (Koerner, 2012). As detailed in Hettiyahandi et al. (2025), the REAG effectively
50 reduced both lateral displacement and settlement of the ballast across all applied load magnitudes and
51 loading frequencies, outperforming conventional polymer geogrids and under-ballast mats in terms of
52 deformation control and energy dissipation.

53

54 ***Ballast Breakage***

55 The Discusser’s observations regarding ballast breakage are consistent with the findings presented in
56 Fig. 7. The Ballast Breakage Index (BBI) decreased across all ballast layers when the REAG was
57 introduced, with the greatest reduction observed in the bottom layer directly above the grid. This

58 reduction results from the REAG's ability to attenuate dynamic stresses and absorb impact energy,
59 thereby limiting particle degradation (Siddiqui et al. 2023). Consequently, the measured reductions in
60 BBI correlate well with the corresponding decreases in settlement and lateral displacement, reaffirming
61 the effectiveness of the REAG in improving ballast stability and durability under cyclic loading.

62

63 ***Field Testing***

64 A drainage layer and a subsurface drainpipe were incorporated in the field test section to address the
65 heavy rainfall and periodic saturation of the subgrade encountered during the construction process,
66 which were conditions that were not present in the controlled laboratory environment. In the field,
67 nonwoven geotextiles were placed both on top of the subgrade and over the capping layer. The
68 geotextile placed above the subgrade served to prevent upward migration of fine particles into the
69 overlying layers, while the one above the capping layer minimized contamination of the ballast by
70 underlying fines and restricted ballast intrusion into the capping material (Indraratna et al. 2025). The
71 Discusser is also correct in observing that nonwoven geotextiles were used in field trials, whereas
72 woven geotextiles were adopted in laboratory tests. Although woven fabrics are generally stronger, the
73 use of nonwoven geotextiles in the field was recommended by the technical team at the Chullora Rail
74 Precinct to ensure adequate drainage through the layers under wet site conditions, since woven
75 geotextiles could have impeded vertical water flow. The authors wish to clarify the maximum dry
76 densities of the ballast and capping layers are 1.6 and 2.2 tonne/m³, respectively, and these values are
77 presented in Table 1.

78

79 ***Energy Dissipation and Damping Ratio of the Track***

80 The Authors acknowledge the Discusser's further elaboration on the comparison of energy dissipation
81 between the REAG and the conventional under-ballast mat (UBM). As noted, the UBM, being a solid
82 rubber sheet without apertures, possesses a larger rubber volume than the REAG, which inherently
83 allows greater energy absorption per cycle of loading (Navaratnarajah et al. 2018). However, it should
84 be emphasized that the REAG, despite its smaller rubber volume, also enhances internal confinement
85 and reduces particle displacement, leading to improved long-term performance, particularly in
86 maintaining track geometry stability under repeated train loading (Qi et al. 2024).

87 The Discusser is correct in noting that the woven geotextile layer placed beneath the REAG could have
88 a minor effect on the measured energy dissipation. Nevertheless, this contribution is considered
89 negligible compared to that of the REAG itself. The woven geotextile is not viscoelastic in nature and
90 therefore does not undergo significant resilient deformation under cyclic loading. Furthermore, no
91 visible deformation or damage was observed in the geotextile layer after the testing, confirming that

92 its influence on the overall track performance was minimal. The primary mechanism of energy
93 dissipation arises from the viscoelastic deformation of the REAG (i.e, damping property) and frictional
94 interactions at the ballast–grid interface, as discussed in Hettiyahandi et al. (2025).

95

96 **Concluding Remarks**

97 The authors thank the Discusser for their constructive comments and valuable insights regarding the
98 cost implications associated with producing REAG and UBMs, as well as the availability of source
99 materials for their manufacture. It was observed that the REAG outperforms the UBMs in reducing
100 ballast breakage because of the additional confinement and interlocking restraint it provides to the
101 ballast particles. This enhanced confinement minimizes particle displacement, leading to improved
102 deformation control and prolonged track stability. In Australia, large quantities of discarded rubber
103 conveyor belts are generated annually from the mining sector, particularly in Western Australia, making
104 them a readily available and sustainable resource for manufacturing REAG. Nevertheless, the authors
105 acknowledge that the availability of discarded conveyor belts for REAG production may be constrained
106 in regions lacking a substantial mining industry. The fabrication of REAG employed water jet cutting
107 technology, which could entail marginally higher production costs compared to the direct reuse of
108 recycled conveyor belts for UBMs. However, such additional costs are expected to diminish with large-
109 scale commercialization and the establishment of an open market.

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