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# catena-Poly[[copper(I)-µ-2,6-bis[4-(pvridin-2-vl)thiazol-2-vl]pvridine] hexafluoridophosphate acetonitrile monosolvate] from single-crystal synchrotron data

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Key indicators: single-crystal synchrotron study; T = 100 K; mean  $\sigma(C-C) = 0.004$  Å; disorder in solvent or counterion; R factor = 0.031; wR factor = 0.078; data-toparameter ratio = 10.0.

The title complex,  $\{[Cu(C_{21}H_{13}N_5S_2)]PF_6 \cdot CH_3CN\}_n$ , was formed immediately on adding together a methanol solution containing copper(I) ions and a methanol solution of 2,6-bis[4-(pyridin-2-yl)thiazol-2-yl]pyridine. Crystallographic studies of the complex reveal a coordination polymer with the ligand acting as a bis(bidentate) ligand with the pyridine N atom not coordinating a metal centre. The Cu<sup>I</sup> atom is four-coordinate with approximately tetrahedral stereochemistry: the N<sub>4</sub> donor set is provided by bipyridine-like moieties of the two heterocyclic ligands. Parallel chains of the coordination polymer run along the *b*-axis direction with the disordered (0.50:0.50 occupancy ratio)  $PF_6^-$  anions and acetonitrile solvent molecules located between the chains.

#### **Related literature**

For a related complex, see: Baker & Matthews (1999).



#### **Experimental**

Crystal data

| $[Cu(C_{21}H_{13}N_5S_2)]PF_6 \cdot C_2H_3N$<br>$M_r = 649.05$ | $V = 2532.4 (9) \text{ Å}^3$<br>Z = 4                         |
|--|---|
| Monoclinic, $P2_1/c$   | Synchrotron radiation $0.71072$                               |
| a = 12.525 (3)  A<br>b = 13.950 (3)  Å                         | $\lambda = 0.71073 \text{ A}$<br>$\mu = 1.16 \text{ mm}^{-1}$ |
| c = 14.626 (3) Å   | T = 100  K  |
| $\beta = 97.72 \ (3)^{\circ}$                                  | $0.03 \times 0.02 \times 0.01 \mbox{ mm}$                     |
| Data collection  |   |
| 3-BM1 Australian Synchrotron                                   | 3641 reflections with $I > 2\sigma(I)$                        |
| diffractometer   | $R_{\rm int} = 0.024$   |
| 28022 measured reflections                                     | $\theta_{\rm max} = 23.8^{\circ}$                             |
| 3890 independent reflections                                   | hinx  |

#### Refinement

| $R[F^2 > 2\sigma(F^2)] = 0.031$ | 389 parameters   |
|---------------------------------|--|
| $wR(F^2) = 0.078$               | H-atom parameters constrained                              |
| S = 1.08                        | $\Delta \rho_{\rm max} = 0.30 \text{ e } \text{\AA}^{-3}$  |
| 3890 reflections                | $\Delta \rho_{\rm min} = -0.57 \ {\rm e} \ {\rm \AA}^{-3}$ |

Data collection: BLU-ICE (McPhillips et al., 2002); cell refinement: XDS (Kabsch, 1993); data reduction: XDS; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: Mercury (Macrae et al., 2008); software used to prepare material for publication: publCIF (Westrip, 2010).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: VM2190).

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# supplementary materials

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# *catena*-Poly[[copper(I)-µ-2,6-bis[4-(pyridin-2-yl)thiazol-2-yl]pyridine] hexafluoridophosphate acetonitrile monosolvate] from single-crystal synchrotron data

### Linda Xiao, Mohan Bhadbhade and Anthony T. Baker

#### Comment

We have prepared and studied many analogues of 2,2'-bipyridine and 2,2':6',2"-terpyridine (Baker and Matthews, 1999 and references therein) and have extended this work to the preparation of ligands analogous to quinquepyridine. For metal complexes of these quinquepyridine analogues, a number of features have been observed. The interpolation of a five-membered heterocycle appears to reduce the capacity of the ligands to employ all five donor atoms and we have seen several examples where the ligands act in a bis(bidentate) mode [2 + 2]. In such cases the ligands bridge between metal centres in binuclear complexes. Herein we report a coordination polymer shown in Scheme 1, again where the ligand binds in [2 + 2] mode. A thermal ellipsoid plot is shown in Fig. 1. Each copper centre has approximately tetrahedral stereochemistry as shown in Fig. 1. The principal cause of distortion being the bite angles of the bidentate ligand N2B—Cu1—N1B (82.47 (8)°) and N2A<sup>i</sup>—Cu1—N1A<sup>i</sup> (82.95 (8)°) (symmetry code: (i) -*x* + 1, *y* + 1/2, -*z* + 1/2) are considerably less than the ideal tetrahedral angle. Two 'thiazolylpyridine' moieties coordinate each copper(I) centre with the relevant bond lengths being Cu—N1A<sup>i</sup> 2.098 (2) Å, Cu—N1B 2.050 (2) Å, Cu—N2A 1.992 (2) Å and Cu—N2B 2.024 (2) Å. The Cu—N bond lengths are similar but the Cu—N<sub>pyridiny1</sub> bonds are slightly shorter than the Cu—N<sub>thiazoly1</sub> bonds. This indicates a slightly stronger interaction of the metal atom with the pyridinyl moiety, in line with base strength. A single chain of the coordination polymer, thus created, is depicted in Fig. 2 and packing of these chains that include PF<sub>6</sub><sup>-</sup> anions and solvent molecules of acetonitriles are shown in Fig. 3.

#### Experimental

The quinquedentate ligand 2,6-bis(4-(pyridin-2-yl)thiazol-2-yl)pyridine was prepared by adding a solution of 2-(bromoacetyl)pyridinium hydrobromide (5.6 g, 20 mmol) in hot ethanol (50 ml) to a solution of 2,6-di(thioamido)pyridine (2.0 g, 10 mmol) in hot ethanol (50 ml). The solution was heated for 5 min, a yellow precipitate of 2,6-bis(4-(pyridin-2yl)thiazol-2-yl)pyridinium hydrobromide separated soon. The mixture was allowed to stand for 30 min s and the yellow precipitate was filtered and washed with sodium bicarbonate (5%) until effervescence ceased. Yield: 75%. The complex was prepared as follows: Tetrakis(acetonitrile)copper(I) hexafluorophosphate (200 mg, 0.54 mmol) in hot methanol (20 ml) was added to a solution of the ligand (214 mg, 0.54 mmol) in hot methanol (20 ml). The reaction mixture was heated on the water bath for 1 h. An orange solid formed during this time and once cooled the solid was collected, washed with cooled methanol and stored over silica gel (yield 164 mg, 50%). Crystals were grown by vapour diffusion of diethyl ether into a concentrated acetonitrile solution of the complex.

#### Refinement

All the H-atoms were fixed stereochemically and included in the refinement using riding model option in *SHELXL97*. The PF6 anion was found to exhibit orientational disorder, which was modelled over two positions.

H atoms were positioned geometrically with C—H = 0.93 - 0.96 Å.  $U_{iso}(H)$  values were set at  $1.2U_{eq}$  (aromatic) or  $1.5U_{eq}$  of the parent atom (methyl group).

#### **Computing details**

Data collection: BLU-ICE (McPhillips *et al.*, 2002); cell refinement: XDS (Kabsch, 1993); data reduction: XDS (Kabsch, 1993); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: Mercury (Macrae *et al.*, 2008); software used to prepare material for publication: *publCIF* (Westrip, 2010).



#### Figure 1

Thermal ellipsoids plot (40% probability) of the part of the coordination polymer showing the geometry around Cu(I) ion. Hydrogen atoms, the PF<sub>6</sub> anion and the solvent acetonitrile molecule are omitted for clarity. Symmetry code: (i) -x + 1, y + 1/2, -z + 1/2.



## Figure 2

A single chain showing the construction of the coordination polymer formed with the ligand.



## Figure 3

Packing of coordination polymers viewed down *c* axis that includes PF6 anions (disorder omitted for clarity) and solvent molecules (acetonitrile).

# *catena*-Poly[[copper(I)-µ-2,6-bis[4-(pyridin-2-yl)thiazol-2-yl]pyridine] hexafluoridophosphate acetonitrile monosolvate]

| Crystal data   |  |
|--|--|
| $[Cu(C_{21}H_{13}N_5S_2)]PF_6 \cdot C_2H_3N$<br>$M_r = 649.05$<br>Monoclinic, $P2_1/c$<br>Hall symbol: -P 2ybc<br>a = 12.525 (3) Å<br>b = 13.950 (3) Å<br>c = 14.626 (3) Å<br>$\beta = 97.72$ (3)°<br>V = 2532.4 (9) Å <sup>3</sup><br>Z = 4 | F(000) = 1304<br>$D_x = 1.702 \text{ Mg m}^{-3}$<br>Synchrotron radiation, $\lambda = 0.71073 \text{ Å}$<br>Cell parameters from 9980 reflections<br>$\theta = 2.5-22.5^{\circ}$<br>$\mu = 1.16 \text{ mm}^{-1}$<br>T = 100  K<br>Thin plates, blue<br>$0.03 \times 0.02 \times 0.01 \text{ mm}$ |
| Data collection  |  |
| 3-BM1 Australian Synchrotron<br>diffractometer<br>Radiation source: Synchrotron BM<br>Si<111> monochromator<br>$\varphi$ scans<br>28022 measured reflections<br>3890 independent reflections   | 3641 reflections with $I > 2\sigma(I)$<br>$R_{\text{int}} = 0.024$<br>$\theta_{\text{max}} = 23.8^\circ, \ \theta_{\text{min}} = 1.6^\circ$<br>$h = -14 \rightarrow 14$<br>$k = -15 \rightarrow 15$<br>$l = -16 \rightarrow 16$  |

Refinement

| Secondary atom site location: difference Fourier                 |
|--|
| map  |
| Hydrogen site location: inferred from                            |
| neighbouring sites   |
| H-atom parameters constrained                                    |
| $w = 1/[\sigma^2(F_o^2) + (0.0359P)^2 + 3.8973P], P = (F_o^2)^2$ |
| $+2F_{c}^{2})/3$   |
| $(\Delta/\sigma)_{\rm max} = 0.001$                              |
| $\Delta \rho_{\rm max} = 0.30 \text{ e } \text{\AA}^{-3}$        |
| $\Delta \rho_{\rm min} = -0.57 \text{ e } \text{\AA}^{-3}$       |
|  |

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(A^2)$ 

|     | x            | у            | Ζ            | $U_{ m iso}$ */ $U_{ m eq}$ | Occ. (<1) |
|-----|--------------|--------------|--------------|-----------------------------|-----------|
| Cu1 | 0.70815 (2)  | 1.19154 (2)  | 0.36895 (2)  | 0.01965 (11)                |           |
| N1  | 0.40269 (16) | 0.95445 (14) | 0.35587 (13) | 0.0159 (4)                  |           |
| C1  | 0.5696 (2)   | 0.89759 (19) | 0.25992 (17) | 0.0211 (6)                  |           |
| H1  | 0.6257       | 0.8784       | 0.2285       | 0.025*                      |           |
| C2  | 0.4814 (2)   | 0.83892 (18) | 0.26281 (17) | 0.0197 (5)                  |           |
| H2  | 0.4773       | 0.7794       | 0.2339       | 0.024*                      |           |
| C3  | 0.3990 (2)   | 0.87086 (17) | 0.30999 (16) | 0.0165 (5)                  |           |
| C4  | 0.48924 (19) | 1.00992 (17) | 0.35293 (16) | 0.0162 (5)                  |           |
| C5  | 0.5735 (2)   | 0.98545 (18) | 0.30444 (17) | 0.0197 (5)                  |           |
| Н5  | 0.6311       | 1.0270       | 0.3020       | 0.024*                      |           |
| S1A | 0.21354 (5)  | 0.84000 (5)  | 0.39190 (4)  | 0.02002 (16)                |           |
| N1A | 0.27744 (16) | 0.73513 (14) | 0.26615 (14) | 0.0163 (4)                  |           |
| N2A | 0.17898 (16) | 0.59744 (15) | 0.15433 (14) | 0.0180 (4)                  |           |
| C1A | 0.3024 (2)   | 0.81261 (17) | 0.31486 (16) | 0.0160 (5)                  |           |
| C2A | 0.18499 (19) | 0.69316 (17) | 0.28980 (17) | 0.0173 (5)                  |           |
| C3A | 0.1400 (2)   | 0.74016 (19) | 0.35688 (17) | 0.0207 (5)                  |           |
| H3A | 0.0781       | 0.7207       | 0.3803       | 0.025*                      |           |
| C4A | 0.14469 (19) | 0.60735 (18) | 0.23785 (17) | 0.0173 (5)                  |           |
| C5A | 0.0784 (2)   | 0.5404 (2)   | 0.27187 (18) | 0.0239 (6)                  |           |
| H5A | 0.0574       | 0.5484       | 0.3300       | 0.029*                      |           |
| C6A | 0.0438 (2)   | 0.4617 (2)   | 0.21859 (19) | 0.0276 (6)                  |           |
| H6A | -0.0001      | 0.4157       | 0.2405       | 0.033*                      |           |
| C7A | 0.0757 (2)   | 0.4527 (2)   | 0.13181 (19) | 0.0275 (6)                  |           |
| H7A | 0.0520       | 0.4015       | 0.0937       | 0.033*                      |           |
| C8A | 0.1432 (2)   | 0.52119 (18) | 0.10326 (18) | 0.0232 (6)                  |           |
| H8A | 0.1652       | 0.5142       | 0.0454       | 0.028*                      |           |

| S1B  | 0.37811 (5)  | 1.12599 (5)  | 0.46088 (4)  | 0.02089 (16) |      |
|------|--------------|--------------|--------------|--------------|------|
| N1B  | 0.56301 (16) | 1.16578 (14) | 0.41446 (13) | 0.0154 (4)   |      |
| N2B  | 0.69867 (17) | 1.31538 (14) | 0.43946 (14) | 0.0193 (5)   |      |
| C1B  | 0.48752 (19) | 1.09985 (18) | 0.40534 (16) | 0.0165 (5)   |      |
| C2B  | 0.5353 (2)   | 1.24125 (18) | 0.46810 (16) | 0.0173 (5)   |      |
| C3B  | 0.4376 (2)   | 1.23154 (18) | 0.49859 (17) | 0.0207 (5)   |      |
| H4B  | 0.4076       | 1.2762       | 0.5349       | 0.025*       |      |
| C4B  | 0.6105 (2)   | 1.32303 (18) | 0.48297 (17) | 0.0190 (5)   |      |
| C5B  | 0.5930 (2)   | 1.40191 (19) | 0.53706 (18) | 0.0248 (6)   |      |
| H5B  | 0.5330       | 1.4047       | 0.5682       | 0.030*       |      |
| C6B  | 0.6670 (2)   | 1.47623 (19) | 0.54353 (19) | 0.0290 (6)   |      |
| H6B  | 0.6566       | 1.5303       | 0.5785       | 0.035*       |      |
| C7B  | 0.7559 (2)   | 1.46972 (19) | 0.49804 (18) | 0.0263 (6)   |      |
| H7B  | 0.8059       | 1.5193       | 0.5013       | 0.032*       |      |
| C8B  | 0.7696 (2)   | 1.38795 (19) | 0.44740 (18) | 0.0239 (6)   |      |
| H8B  | 0.8305       | 1.3831       | 0.4176       | 0.029*       |      |
| P1   | 0.91781 (5)  | 0.77051 (5)  | 0.06197 (5)  | 0.02250 (17) |      |
| F1   | 1.02028 (15) | 0.72763 (13) | 0.02232 (14) | 0.0467 (5)   |      |
| F2   | 0.9637 (5)   | 0.7561 (5)   | 0.1692 (5)   | 0.0320 (13)  | 0.50 |
| F3   | 0.8706 (11)  | 0.6650 (9)   | 0.0595 (7)   | 0.034 (2)    | 0.50 |
| F4   | 0.8738 (5)   | 0.7876 (5)   | -0.0432 (4)  | 0.0503 (15)  | 0.50 |
| F5   | 0.9640 (8)   | 0.8778 (6)   | 0.0694 (4)   | 0.0348 (15)  | 0.50 |
| F2′  | 1.0012 (6)   | 0.7796 (6)   | 0.1511 (5)   | 0.064 (2)    | 0.50 |
| F3′  | 0.8878 (13)  | 0.6654 (11)  | 0.0896 (8)   | 0.063 (4)    | 0.50 |
| F4′  | 0.8345 (5)   | 0.7575 (6)   | -0.0299 (5)  | 0.063 (2)    | 0.50 |
| F5′  | 0.9533 (8)   | 0.8721 (7)   | 0.0272 (6)   | 0.080 (3)    | 0.50 |
| F6   | 0.81523 (16) | 0.81302 (15) | 0.10063 (17) | 0.0572 (6)   |      |
| C1AN | 0.1934 (3)   | 0.1022 (3)   | 0.2238 (2)   | 0.0507 (9)   |      |
| H1A1 | 0.1468       | 0.0772       | 0.1718       | 0.076*       |      |
| H1A2 | 0.1637       | 0.1606       | 0.2442       | 0.076*       |      |
| H1A3 | 0.2001       | 0.0562       | 0.2730       | 0.076*       |      |
| C2AN | 0.2998 (3)   | 0.1214 (2)   | 0.19694 (19) | 0.0297 (7)   |      |
| N1AN | 0.3824 (2)   | 0.13309 (19) | 0.17597 (18) | 0.0368 (6)   |      |
|      |              |              |              |              |      |

Atomic displacement parameters  $(Å^2)$ 

|     | $U^{11}$     | $U^{22}$     | $U^{33}$     | $U^{12}$     | $U^{13}$     | $U^{23}$      |
|-----|--------------|--------------|--------------|--------------|--------------|---------------|
| Cul | 0.02253 (19) | 0.01556 (18) | 0.02245 (18) | 0.00197 (12) | 0.00884 (13) | -0.00093 (12) |
| N1  | 0.0184 (11)  | 0.0143 (10)  | 0.0151 (10)  | 0.0000 (8)   | 0.0026 (8)   | 0.0017 (8)    |
| C1  | 0.0218 (13)  | 0.0219 (14)  | 0.0209 (13)  | 0.0003 (11)  | 0.0083 (10)  | -0.0021 (11)  |
| C2  | 0.0243 (14)  | 0.0154 (13)  | 0.0195 (13)  | -0.0016 (10) | 0.0031 (10)  | -0.0016 (10)  |
| C3  | 0.0198 (13)  | 0.0146 (12)  | 0.0146 (12)  | 0.0000 (10)  | 0.0012 (10)  | 0.0032 (10)   |
| C4  | 0.0214 (13)  | 0.0130 (12)  | 0.0137 (12)  | -0.0013 (10) | 0.0000 (10)  | 0.0016 (10)   |
| C5  | 0.0195 (13)  | 0.0194 (13)  | 0.0210 (13)  | -0.0038 (10) | 0.0058 (10)  | 0.0006 (10)   |
| S1A | 0.0198 (3)   | 0.0213 (3)   | 0.0196 (3)   | 0.0006 (3)   | 0.0054 (2)   | -0.0028 (3)   |
| N1A | 0.0173 (10)  | 0.0145 (11)  | 0.0172 (10)  | 0.0002 (8)   | 0.0024 (8)   | 0.0026 (9)    |
| N2A | 0.0174 (10)  | 0.0165 (11)  | 0.0199 (11)  | 0.0017 (9)   | 0.0022 (8)   | 0.0025 (9)    |
| C1A | 0.0179 (12)  | 0.0151 (13)  | 0.0150 (12)  | 0.0023 (10)  | 0.0025 (10)  | 0.0023 (10)   |
| C2A | 0.0157 (12)  | 0.0173 (13)  | 0.0188 (12)  | 0.0003 (10)  | 0.0016 (10)  | 0.0047 (10)   |
| C3A | 0.0173 (13)  | 0.0243 (14)  | 0.0211 (13)  | -0.0019 (11) | 0.0046 (10)  | 0.0023 (11)   |

| C4A  | 0.0148 (12) | 0.0160 (13) | 0.0207 (13) | 0.0019 (10)  | 0.0009 (10)  | 0.0041 (10)  |
|------|-------------|-------------|-------------|--------------|--------------|--------------|
| C5A  | 0.0221 (14) | 0.0262 (14) | 0.0233 (13) | -0.0032 (11) | 0.0029 (11)  | 0.0052 (11)  |
| C6A  | 0.0258 (14) | 0.0227 (14) | 0.0337 (15) | -0.0093 (11) | 0.0023 (12)  | 0.0069 (12)  |
| C7A  | 0.0317 (15) | 0.0188 (14) | 0.0310 (15) | -0.0073 (12) | 0.0004 (12)  | -0.0022 (12) |
| C8A  | 0.0272 (14) | 0.0199 (14) | 0.0226 (13) | -0.0005 (11) | 0.0036 (11)  | -0.0002 (11) |
| S1B  | 0.0197 (3)  | 0.0201 (3)  | 0.0244 (3)  | -0.0023 (3)  | 0.0085 (3)   | -0.0034 (3)  |
| N1B  | 0.0189 (11) | 0.0132 (10) | 0.0146 (10) | 0.0000 (8)   | 0.0038 (8)   | 0.0009 (8)   |
| N2B  | 0.0225 (11) | 0.0152 (11) | 0.0197 (11) | 0.0005 (9)   | 0.0010 (9)   | 0.0010 (9)   |
| C1B  | 0.0181 (12) | 0.0178 (13) | 0.0141 (12) | 0.0018 (10)  | 0.0039 (10)  | 0.0021 (10)  |
| C2B  | 0.0230 (13) | 0.0148 (12) | 0.0142 (12) | 0.0020 (10)  | 0.0025 (10)  | 0.0001 (10)  |
| C3B  | 0.0231 (14) | 0.0186 (13) | 0.0212 (13) | 0.0005 (11)  | 0.0059 (10)  | -0.0051 (11) |
| C4B  | 0.0229 (13) | 0.0166 (13) | 0.0172 (12) | 0.0019 (10)  | 0.0013 (10)  | 0.0019 (10)  |
| C5B  | 0.0294 (15) | 0.0196 (14) | 0.0253 (14) | 0.0035 (11)  | 0.0037 (11)  | -0.0033 (11) |
| C6B  | 0.0404 (17) | 0.0173 (14) | 0.0288 (15) | 0.0022 (12)  | 0.0022 (13)  | -0.0060 (11) |
| C7B  | 0.0336 (16) | 0.0153 (13) | 0.0283 (15) | -0.0057 (11) | -0.0021 (12) | -0.0008 (11) |
| C8B  | 0.0236 (14) | 0.0212 (14) | 0.0269 (14) | -0.0031 (11) | 0.0030 (11)  | 0.0038 (11)  |
| P1   | 0.0214 (4)  | 0.0218 (4)  | 0.0244 (4)  | 0.0027 (3)   | 0.0035 (3)   | 0.0035 (3)   |
| F1   | 0.0402 (11) | 0.0389 (11) | 0.0688 (13) | 0.0088 (8)   | 0.0354 (10)  | 0.0116 (9)   |
| F2   | 0.046 (4)   | 0.029 (2)   | 0.021 (2)   | 0.009 (2)    | 0.003 (2)    | 0.0040 (16)  |
| F3   | 0.033 (4)   | 0.020 (4)   | 0.051 (5)   | -0.010 (3)   | 0.016 (3)    | -0.016 (4)   |
| F4   | 0.064 (5)   | 0.061 (4)   | 0.023 (2)   | 0.018 (3)    | -0.008 (3)   | 0.011 (2)    |
| F5   | 0.046 (3)   | 0.017 (2)   | 0.046 (3)   | -0.001 (2)   | 0.024 (3)    | -0.002 (3)   |
| F2′  | 0.053 (5)   | 0.092 (6)   | 0.039 (4)   | 0.035 (4)    | -0.018 (3)   | -0.038 (4)   |
| F3′  | 0.051 (6)   | 0.043 (5)   | 0.103 (10)  | 0.004 (4)    | 0.037 (6)    | 0.032 (6)    |
| F4′  | 0.031 (3)   | 0.113 (6)   | 0.041 (3)   | 0.001 (3)    | -0.010 (2)   | 0.001 (3)    |
| F5′  | 0.038 (3)   | 0.030 (4)   | 0.176 (9)   | 0.006 (3)    | 0.027 (6)    | 0.054 (6)    |
| F6   | 0.0392 (11) | 0.0510 (13) | 0.0864 (16) | 0.0157 (9)   | 0.0267 (11)  | -0.0079 (11) |
| C1AN | 0.0362 (19) | 0.077 (3)   | 0.0421 (19) | -0.0020 (18) | 0.0159 (15)  | 0.0064 (19)  |
| C2AN | 0.0368 (18) | 0.0305 (16) | 0.0215 (14) | 0.0006 (13)  | 0.0026 (13)  | 0.0061 (12)  |
| N1AN | 0.0347 (16) | 0.0418 (16) | 0.0340 (14) | -0.0042 (12) | 0.0049 (12)  | 0.0149 (12)  |

Geometric parameters (Å, °)

| Cu1—N2A <sup>i</sup> | 1.992 (2) | C8A—H8A | 0.9300    |
|----------------------|-----------|---------|-----------|
| Cu1—N2B              | 2.024 (2) | S1B—C3B | 1.708 (3) |
| Cu1—N1B              | 2.050 (2) | S1B—C1B | 1.723 (2) |
| Cu1—N1A <sup>i</sup> | 2.098 (2) | N1B—C1B | 1.313 (3) |
| N1—C4                | 1.337 (3) | N1B—C2B | 1.385 (3) |
| N1—C3                | 1.343 (3) | N2B—C8B | 1.342 (3) |
| C1—C2                | 1.380 (4) | N2B—C4B | 1.351 (3) |
| C1—C5                | 1.386 (4) | C2B—C3B | 1.364 (4) |
| C1—H1                | 0.9300    | C2B—C4B | 1.476 (4) |
| С2—С3                | 1.390 (4) | C3B—H4B | 0.9300    |
| С2—Н2                | 0.9300    | C4B—C5B | 1.390 (4) |
| C3—C1A               | 1.467 (3) | C5B—C6B | 1.385 (4) |
| C4—C5                | 1.391 (4) | C5B—H5B | 0.9300    |
| C4—C1B               | 1.472 (3) | C6B—C7B | 1.375 (4) |
| С5—Н5                | 0.9300    | C6B—H6B | 0.9300    |
| S1A—C3A              | 1.710 (3) | C7B—C8B | 1.383 (4) |
| S1A—C1A              | 1.730 (2) | С7В—Н7В | 0.9300    |
|                      |           |         |           |

| N1A—C1A                          | 1.309 (3)               | C8B—H8B  | 0.9300               |
|----------------------------------|-------------------------|--|----------------------|
| N1A—C2A                          | 1.382 (3)               | P1—F2'   | 1.562 (7)            |
| N1A—Cu1 <sup>ii</sup>            | 2.098 (2)               | P1—F3′   | 1.580 (16)           |
| N2A—C8A                          | 1.342 (3)               | P1—F4  | 1.581 (6)            |
| N2A—C4A                          | 1.355 (3)               | P1—F3  | 1.585 (13)           |
| N2A—Cu1 <sup>ii</sup>            | 1.992 (2)               | P1—F6  | 1.587 (2)            |
| C2A—C3A                          | 1.363 (4)               | P1—F5'   | 1.589 (9)            |
| C2A—C4A                          | 1.470 (4)               | P1—F1  | 1.5941 (18)          |
| СЗА—НЗА                          | 0.9300                  | P1—F4′   | 1.597 (7)            |
| C4A—C5A                          | 1.385 (4)               | P1—F5  | 1.603 (9)            |
| C5A—C6A                          | 1.382 (4)               | P1—F2  | 1.609 (7)            |
| C5A—H5A                          | 0.9300                  | C1AN—C2AN  | 1.464 (4)            |
| C6A—C7A                          | 1.387 (4)               | C1AN—H1A1  | 0.9600               |
| C6A—H6A                          | 0.9300                  | CIAN—HIA2  | 0.9600               |
| C7A—C8A                          | 1 377 (4)               | CIAN—HIA3  | 0.9600               |
| C7A—H7A                          | 0.9300                  | C2AN—N1AN  | 1 130 (4)            |
|                                  | 0.9500                  |  | 1.150 (1)            |
| N2A <sup>i</sup> —Cu1—N2B        | 137 85 (9)              | S1B-C3B-H4B  | 124 7                |
| $N2A^{i}$ —Cu1—N1B               | 128 37 (8)              | N2B-C4B-C5B  | 122.1(2)             |
| N2B—Cu1—N1B                      | 82 47 (8)               | N2B - C4B - C2B  | 1145(2)              |
| $N2A^{i}$ —Cu1—N1 $A^{i}$        | 82.95 (8)               | C5B-C4B-C2B  | 1233(2)              |
| $N2B-Cu1-N1A^{i}$                | 10453(8)                | C6B-C5B-C4B  | 123.5(2)<br>118 5(3) |
| $N1B-Cu1-N1A^{i}$                | 123 28 (8)              | C6B-C5B-H5B  | 120.8                |
| C4-N1-C3                         | 1174(2)                 | C4B-C5B-H5B  | 120.8                |
| $C_{2}-C_{1}-C_{5}$              | 119 2 (2)               | C7B-C6B-C5B  | 120.0<br>119.7(3)    |
| C2                               | 120.4                   | C7B-C6B-H6B  | 120.1                |
| C5-C1-H1                         | 120.1                   | C5B-C6B-H6B  | 120.1                |
| C1 - C2 - C3                     | 1184(2)                 | C6B-C7B-C8B  | 120.1<br>118.7(3)    |
| C1 - C2 - H2                     | 120.8                   | C6B - C7B - H7B  | 120.7                |
| $C_{3}$ $C_{2}$ $H_{2}$          | 120.8                   | $C^{8}B-C^{7}B-H^{7}B$   | 120.7                |
| N1 - C3 - C2                     | 123.3(2)                | N2B_C8B_C7B  | 120.7<br>122.7(3)    |
| N1 - C3 - C1A                    | 125.5(2)<br>115.5(2)    | N2B_C8B_H8B  | 122.7 (5)            |
| $C_2 = C_3 = C_1 \Delta$         | 113.3(2)<br>121.3(2)    | C7B C8B H8B  | 118.6                |
| $C_2 = C_3 = C_1 A$              | 121.3(2)<br>123.3(2)    | $E'_{D}$ $E'_{C}$ $E'_{D}$ $E'_{C}$ $E$ | 910(5)               |
| N1 = C4 = C3                     | 123.3(2)<br>114.1(2)    | $F_2 - F_1 - F_3$<br>F2' P1 F4   | 91.0(3)              |
| $C_{1} = C_{1} = C_{1}$          | 114.1(2)<br>122.7(2)    | $F_2 - F_1 - F_4$<br>$F_3' - P_1 - F_4$  | 133.0(4)             |
| $C_1 = C_5 = C_4$                | 122.7(2)<br>118.4(2)    | $F_{2}^{-1} = F_{1}^{-1} = F_{2}^{-1}$   | 107.0(5)             |
| C1 = C5 = H5                     | 110.4 (2)               | $F_2 - F_1 - F_3$<br>$F_2' - D_1 - F_2$  | 16.8 (6)             |
| $C_1 = C_2 = H_2$                | 120.8                   | $\Gamma_{3} - \Gamma_{1} - \Gamma_{3}$   | 10.8(0)              |
| $C_{4}$                          | 120.8<br>80.57 (12)     | $F_{4} = F_{1} = F_{5}$<br>$F_{2}' = D_{1} = F_{6}$  | 92.2(3)              |
| $C_{1A} = N_{1A} = C_{1A}$       | 39.37(12)               | $F_2 = 1 = 10$<br>$F_3' = D_1 = F_6$   | 90.9(3)              |
| $C1A = N1A = C1^{\parallel}$     | 111.1(2)<br>135.01(17)  | $F_{4} = F_{1} = F_{4}$  | 91.4(0)              |
| $C_{1A} = N_{1A} = C_{11}^{ii}$  | 107.09(15)              | $F_{4} = F_{1} = F_{0}$  | 93.0(3)              |
| $C_{2A} = N_{1A} = C_{4A}$       | 107.09(13)<br>117.4(2)  | $F_{2}' = P_{1} = F_{2}'$  | 92.2(5)              |
| C8A N2A Cu <sup>1ii</sup>        | 117.7(2)<br>128.23(18)  | $F_2 = 11 = 15$<br>$F_3' = D_1 = 5'$   | 90.0(3)              |
| CAA = N2A = Cu1                  | 120.23 (10)             | $F_{4} = F_{1} = F_{5}$  | 1/4.7(/)<br>68 3 (1) |
| $V_{TA} = IN_{2A} = Cul$         | 113.07 (10)             | $F_{} F_{} F_{} F_{} F_{} F_{} F_{} F_{} F_{$  | 160 2 (5)            |
| $N1\Delta$ $C1\Delta$ $S1\Delta$ | 127.7(2)<br>114 16 (18) | $F_{6}$ $P_{1}$ $F_{5}'$   | 03.2(3)              |
| $C_{3} = C_{1A} = S_{1A}$        | 121 00 (18)             | 10 - 11 - 10<br>F2' = D1 = F1  | 93.2(3)              |
| UJ-UIA-BIA                       | 121.07 (10)             | 12 - 11 - 11   | 01.0(3)              |

| C3A—C2A—N1A                   | 114.7 (2)   | F3′—P1—F1                     | 88.6 (6)     |
|-------------------------------|-------------|-------------------------------|--------------|
| C3A—C2A—C4A                   | 128.1 (2)   | F4—P1—F1                      | 84.0 (3)     |
| N1A—C2A—C4A                   | 117.2 (2)   | F3—P1—F1                      | 87.7 (5)     |
| C2A-C3A-S1A                   | 110.47 (19) | F6—P1—F1                      | 179.52 (13)  |
| C2A - C3A - H3A               | 124.8       | F5′—P1—F1                     | 86.8 (3)     |
| SIA-C3A-H3A                   | 124.8       | F2'                           | 177 9 (4)    |
| N2A—C4A—C5A                   | 122.2 (2)   | F3'                           | 87.6 (5)     |
| N2A—C4A—C2A                   | 114.9 (2)   | F4—P1—F4'                     | 25.2 (2)     |
| C5A-C4A-C2A                   | 122.9 (2)   | F3—P1—F4'                     | 71.1 (5)     |
| C6A—C5A—C4A                   | 119.4 (2)   | F6—P1—F4'                     | 82.8 (3)     |
| C6A—C5A—H5A                   | 120.3       | F5'—P1—F4'                    | 90.7 (4)     |
| C4A—C5A—H5A                   | 120.3       | F1—P1—F4'                     | 96.8 (3)     |
| C5A—C6A—C7A                   | 118.8 (2)   | F2′—P1—F5                     | 70.9 (4)     |
| С5А—С6А—Н6А                   | 120.6       | F3'-P1-F5                     | 161.0 (4)    |
| C7A-C6A-H6A                   | 120.6       | F4—P1—F5                      | 90.0 (3)     |
| C8A - C7A - C6A               | 118.6 (3)   | F3—P1—F5                      | 177.2(5)     |
| C8A - C7A - H7A               | 120.7       | F6—P1—F5                      | 86.0.(3)     |
| C6A - C7A - H7A               | 120.7       | F5′—P1—F5                     | 22.4 (4)     |
| N2A—C8A—C7A                   | 123.6 (2)   | F1—P1—F5                      | 94.2 (3)     |
| N2A—C8A—H8A                   | 118.2       | F4′—P1—F5                     | 110.7 (4)    |
| C7A—C8A—H8A                   | 118.2       | F2′—P1—F2                     | 23.9 (3)     |
| C3B - S1B - C1B               | 89.68 (12)  | F3'                           | 72.6 (4)     |
| C1B—N1B—C2B                   | 111.0 (2)   | F4—P1—F2                      | 178.4 (3)    |
| C1B—N1B—Cu1                   | 138.40 (17) | F3—P1—F2                      | 89.4 (4)     |
| C2B—N1B—Cu1                   | 110.56 (16) | F6—P1—F2                      | 84.2 (2)     |
| C8B—N2B—C4B                   | 118.3 (2)   | F5'—P1—F2                     | 110.2 (4)    |
| C8B—N2B—Cu1                   | 127.22 (18) | F1—P1—F2                      | 96.2 (2)     |
| C4B—N2B—Cu1                   | 114.53 (17) | F4′—P1—F2                     | 156.0 (3)    |
| N1B—C1B—C4                    | 126.1 (2)   | F5—P1—F2                      | 88.4 (3)     |
| N1B—C1B—S1B                   | 114.28 (18) | C2AN—C1AN—H1A1                | 109.5        |
| C4—C1B—S1B                    | 119.61 (18) | C2AN—C1AN—H1A2                | 109.5        |
| C3B—C2B—N1B                   | 114.4 (2)   | H1A1—C1AN—H1A2                | 109.5        |
| C3B—C2B—C4B                   | 127.6 (2)   | C2AN—C1AN—H1A3                | 109.5        |
| N1B—C2B—C4B                   | 117.9 (2)   | H1A1—C1AN—H1A3                | 109.5        |
| C2B—C3B—S1B                   | 110.60 (19) | H1A2—C1AN—H1A3                | 109.5        |
| C2B—C3B—H4B                   | 124.7       | N1AN—C2AN—C1AN                | 177.8 (4)    |
|                               |             |                               |              |
| C5—C1—C2—C3                   | 0.5 (4)     | N2B—Cu1—N1B—C1B               | 176.7 (3)    |
| C4—N1—C3—C2                   | 2.0 (3)     | N1A <sup>i</sup> —Cu1—N1B—C1B | 74.2 (3)     |
| C4—N1—C3—C1A                  | -179.8 (2)  | N2A <sup>i</sup> —Cu1—N1B—C2B | 147.28 (15)  |
| C1—C2—C3—N1                   | -2.6 (4)    | N2B—Cu1—N1B—C2B               | -0.84 (16)   |
| C1—C2—C3—C1A                  | 179.3 (2)   | N1A <sup>i</sup> —Cu1—N1B—C2B | -103.31 (16) |
| C3—N1—C4—C5                   | 0.6 (3)     | N2A <sup>i</sup> —Cu1—N2B—C8B | 39.4 (3)     |
| C3—N1—C4—C1B                  | -179.6 (2)  | N1B—Cu1—N2B—C8B               | -178.7 (2)   |
| C2-C1-C5-C4                   | 1.9 (4)     | N1A <sup>i</sup> —Cu1—N2B—C8B | -56.2 (2)    |
| N1—C4—C5—C1                   | -2.6 (4)    | N2A <sup>i</sup> —Cu1—N2B—C4B | -140.17 (17) |
| C1B—C4—C5—C1                  | 177.7 (2)   | N1B—Cu1—N2B—C4B               | 1.73 (17)    |
| C2A—N1A—C1A—C3                | 176.6 (2)   | N1A <sup>i</sup> —Cu1—N2B—C4B | 124.25 (17)  |
| Cu1 <sup>ii</sup> —N1A—C1A—C3 | -37.1 (4)   | C2B—N1B—C1B—C4                | 179.8 (2)    |

| C2A—N1A—C1A—S1A                | -0.7 (3)     | Cu1—N1B—C1B—C4  | 2.3 (4)      |  |
|--------------------------------|--------------|-----------------|--------------|--|
| Cu1 <sup>ii</sup> —N1A—C1A—S1A | 145.62 (16)  | C2B—N1B—C1B—S1B | 0.3 (3)      |  |
| N1—C3—C1A—N1A                  | 171.2 (2)    | Cu1—N1B—C1B—S1B | -177.16 (14) |  |
| C2—C3—C1A—N1A                  | -10.5 (4)    | N1—C4—C1B—N1B   | 179.0 (2)    |  |
| N1—C3—C1A—S1A                  | -11.7 (3)    | C5—C4—C1B—N1B   | -1.2 (4)     |  |
| C2—C3—C1A—S1A                  | 166.63 (19)  | N1—C4—C1B—S1B   | -1.5 (3)     |  |
| C3A—S1A—C1A—N1A                | 0.76 (19)    | C5—C4—C1B—S1B   | 178.24 (19)  |  |
| C3A—S1A—C1A—C3                 | -176.6 (2)   | C3B—S1B—C1B—N1B | -0.1 (2)     |  |
| C1A—N1A—C2A—C3A                | 0.2 (3)      | C3B—S1B—C1B—C4  | -179.6 (2)   |  |
| Cu1 <sup>ii</sup> —N1A—C2A—C3A | -155.55 (18) | C1B—N1B—C2B—C3B | -0.5 (3)     |  |
| C1A—N1A—C2A—C4A                | 177.6 (2)    | Cu1—N1B—C2B—C3B | 177.75 (17)  |  |
| Cu1 <sup>ii</sup> —N1A—C2A—C4A | 21.8 (2)     | C1B—N1B—C2B—C4B | -178.3 (2)   |  |
| N1A—C2A—C3A—S1A                | 0.3 (3)      | Cu1—N1B—C2B—C4B | -0.1 (3)     |  |
| C4A—C2A—C3A—S1A                | -176.7 (2)   | N1B-C2B-C3B-S1B | 0.4 (3)      |  |
| C1A—S1A—C3A—C2A                | -0.6 (2)     | C4B—C2B—C3B—S1B | 178.0 (2)    |  |
| C8A—N2A—C4A—C5A                | 2.3 (3)      | C1B—S1B—C3B—C2B | -0.2 (2)     |  |
| Cu1 <sup>ii</sup> —N2A—C4A—C5A | -170.47 (19) | C8B—N2B—C4B—C5B | -1.8 (4)     |  |
| C8A—N2A—C4A—C2A                | -178.9 (2)   | Cu1—N2B—C4B—C5B | 177.81 (19)  |  |
| Cu1 <sup>ii</sup> —N2A—C4A—C2A | 8.3 (3)      | C8B—N2B—C4B—C2B | 178.2 (2)    |  |
| C3A—C2A—C4A—N2A                | 155.6 (2)    | Cu1—N2B—C4B—C2B | -2.2 (3)     |  |
| N1A—C2A—C4A—N2A                | -21.4 (3)    | C3B—C2B—C4B—N2B | -176.0 (2)   |  |
| C3A—C2A—C4A—C5A                | -25.6 (4)    | N1B—C2B—C4B—N2B | 1.5 (3)      |  |
| N1A—C2A—C4A—C5A                | 157.4 (2)    | C3B—C2B—C4B—C5B | 4.0 (4)      |  |
| N2A—C4A—C5A—C6A                | -1.4 (4)     | N1B—C2B—C4B—C5B | -178.5 (2)   |  |
| C2A—C4A—C5A—C6A                | 179.9 (2)    | N2B-C4B-C5B-C6B | 2.3 (4)      |  |
| C4A—C5A—C6A—C7A                | -0.7 (4)     | C2B—C4B—C5B—C6B | -177.7 (2)   |  |
| C5A—C6A—C7A—C8A                | 1.8 (4)      | C4B—C5B—C6B—C7B | -1.0 (4)     |  |
| C4A—N2A—C8A—C7A                | -1.1 (4)     | C5B—C6B—C7B—C8B | -0.6 (4)     |  |
| Cu1 <sup>ii</sup> —N2A—C8A—C7A | 170.5 (2)    | C4B—N2B—C8B—C7B | 0.0 (4)      |  |
| C6A—C7A—C8A—N2A                | -1.0 (4)     | Cu1—N2B—C8B—C7B | -179.53 (19) |  |
| N2A <sup>i</sup> —Cu1—N1B—C1B  | -35.2 (3)    | C6B—C7B—C8B—N2B | 1.2 (4)      |  |

Symmetry codes: (i) -*x*+1, *y*+1/2, -*z*+1/2; (ii) -*x*+1, *y*-1/2, -*z*+1/2.