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Performance Analysis of Energy Regeneration System of Electric Vehicle with Two Wheels under the Mode of Constant Braking Torque

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Abstract- A comprehensive performance analysis is crucial for advance a system to a practical level. This paper presents the performance analysis of energy regeneration system (ERS) of electric vehicle (EV) with two wheels under the mode of constant braking torque (CBT). For this, a boost equivalent circuit for main power case (MPC) of ERS is obtained firstly, and then a large signal time domain average model of MPC, which constitutes the complete model of ERS along with the other three parts: system dynamics model, permanent dc motor driving system model and system performance calculation model, is given here. During modeling ERS, a new method based on state forecast viewer is proposed to identify the state (CCM or DCM) of the MPC. As a nonlinear system, the large signal time domain model of ERS can't be transferred to frequency domain model and implemented in MATLAB/Simulink directly, a method of dividing the system into a slow variable system and a fast variable system is introduced. By running this simulation model, several important performances of ERS are obtained efficiently.

I. INTRODUCTION

In order to protect the nature surrounding and decrease the danger of using rock oil as a main single energy resource, electric vehicle (EV) has been becoming the main research point in almost developed countries since the decade of 80 in last century^[1]. As a main vehicle of short distance, the EV with two wheels has also acquired much attention in many countries, especially in China and Japan. Although the product of EV with two wheels has entered into the practical market, for being limited by the current technique of storage battery, there are many problems left to be solved till now^[2]. According to the distributed characteristic of power consumed in EV, the technique of ERS, which can prolong the rated distance by over 20% in the surrounding of city road, becomes one of important research points at present.

In EV with two wheels, there are two main kinds of motor: permanent dc motor and brushless dc motor (BLDC). Both of them often have hubcap structures, which will decrease the assembling difficulty and the power consume of dynamics transferring system. For EV with two wheels, the BLDC motor

has not advantages than permanent dc motor in totally^[3]. Many permanent dc motor driving systems have been used, and this situation will continue^[3]. For being the main mode of four ERS modes, the mode of ERS: constant braking torque (CBT) has higher practical value than those others^[4]. Considering all the above factors, studying ERS of EV with two wheels and dc motor driving system under the mode of CBT is valuable for its application practically. Among many topics, obtaining the effect of ERS on the performance of EV is one of the most important works; it is the base for the application of ERS.

Several papers have done some analysis for EV, however, a systemic performance analysis for EV is not found till now. For that, a boost equivalent circuit for main power case (MPC) of ERS is obtained, and then the signal average time domain model of the converters is given. Along with the system dynamics model, dc motor driving system and system performance calculation model, the complete average model of ERS is given. A new method based on state forecast viewer is proposed to identify the state of MPC. As the nonlinear time domain model can't be transferred to the frequency domain model and implemented in MATLAB/Simulink directly, a method of dividing the system into a fast and slow system is adopted. By running this model, several important performances of ERS are calculated efficiently.

II. DYNAMICS MODEL OF EV WITH TWO WHEELS

According to the theory of mechanical kinematics, the dynamics model of EV with two wheels running in a straight course is shown as follows:

$$\begin{cases} F_w = \frac{1}{2} C_d A \rho (v + v_w)^2 \\ F_f = mgf \cos a \\ F_i = mg \sin a \\ F_a = \delta m \frac{dv}{dt} \end{cases} \quad (1)$$

$$\delta = 1 + \frac{J}{mr^2} \quad (2)$$

$$F_g = F_w + F_f + F_i + F_a \quad (3)$$

where v is the speed of EV, v_w is the windward speed, J is the

rotational inertia of two wheels, C_d is the wind baffle coefficient, A is the windward area, ρ is the air mass density, r is the radius of the wheel, m is the sum of EV mass and burden, g is the gravitation coefficient, f is the roll hinder coefficient, δ is the equivalent inertia coefficient, α is the gradient angular of road, F_g is the propulsive force of motor, and all the left symbols are in accordance with their conventional customs.

III. MODELING ENERGY REGENERATION SYSTEM

A. MPC Equivalent Circuit of ERS

The typical MPC circuit of permanent dc motor driving system with the function of energy regeneration in EV with two wheels is shown in Fig.1 (a). It is comprised of two controllable switches T_1 and T_2 (s.g., MOSFET), two diodes D_1 and D_2 , a filter capacitor C , a permanent dc motor M_D , and a current sensor I_{sensor} . The switch is turned on and off at the switching frequency $f_s = 1/T$ with the ON duty ratio $d_f = t_{on}/T$, where t_{on} is the interval when the switch is ON. If EV is working in the state of driving, the T_2 is working in the PWM state, and the T_1 is turned off all the time. If EV is working the state of energy regeneration, the T_1 is working the PWM state, and the T_2 is turned off all the time. There are two sub-state of energy regeneration: the state of storing the kinetic energy of EV into the inductance of dc motor, and the state of releasing the energy stored in the inductance of dc motor to battery, which are shown in Fig.1 (b) and Fig.1 (c), correspondingly.

When the EV is working in the state of ERS, the block comprised of T_2 and D_2 in Fig.1 (b) and Fig.1 (c) can be moved to the new position shown in Fig.2 (a). As the D_1 and T_2 haven't influences on ERS, both of them are cancelled in Fig.2 (a). By replacing the actual dc motor and other actual components by their corresponding equivalent circuit in Fig.2 (a), then the equivalent circuit with actual components is obtained and shown in Fig.2 (b). The circuit shown in Fig.2 (b) is the typical circuit of the boost converters, where E_m , R_m , and L_m are the back emf, the resistance of armature, and the inductance of armature of dc motor correspondingly; the diode in the ON state is modeled by a constant-voltage battery V_{2F} and a constant forward resistance R_{2ON} and in the OFF state by an infinite resistance, all its junction capacitance and lead inductance are omitted; The power MOSFET in the ON state is modeled by a constant resistance R_{1ON} and in the OFF state by an infinite resistance, and its output capacitance and lead inductance are omitted; the rechargeable battery is modeled by a constant battery E_B and a constant resistance R_B . As all the resistances in Fig.2 (b) and the V_{2F} are very small and be omitted, then the equivalent circuit with idea components is obtained and shown in Fig.2 (c). Fig.2 (c) shows the typical boost converters with idea components.

As the output electro-magnetic torque of permanent dc motor is proportional to its armature current, the model of CBT can be seen as the model of constant braking current (CBC), and then the typical PI control system of ERS under the model of CBC is shown in Fig.2 (d), where I_m is the armature current, I_i is the preset current, d is the turn on ratio cycle of PWM duty cycle, f_s is the frequency of sawtooth wave and m_c is its slop, IC is a comparator, PI is the controller of proportion and integrator with the saturation limiting output.

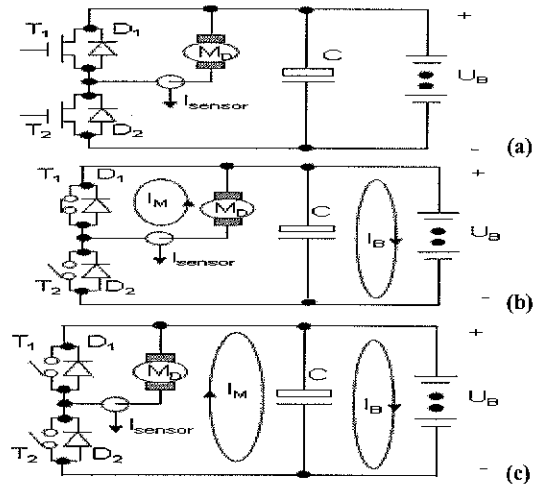


Fig. 1. MPC circuit of ERS based on the permanent dc motor. (a) MPC circuit. (b) Storing the kinetic energy in motor. (c) The Releasing the energy stored in motor to battery.

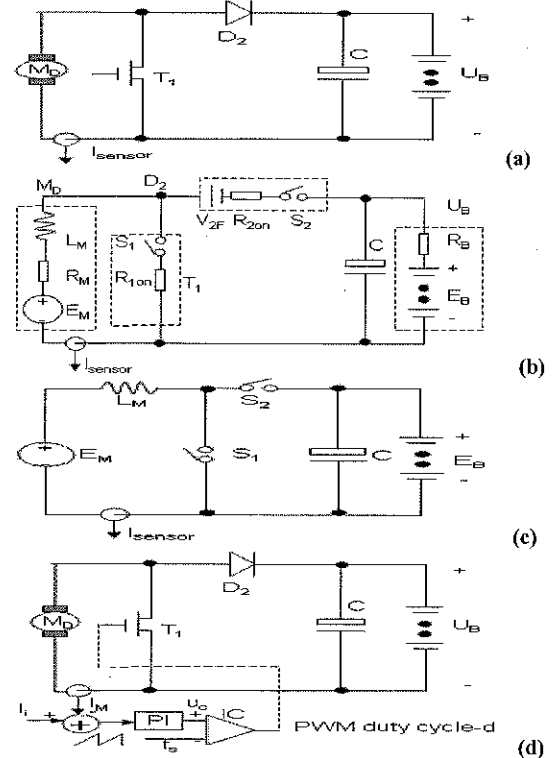


Fig. 2 MPC equivalent circuit of ERS based on the permanent dc motor. (a) Equivalent circuit with actual components. (b) Equivalent circuit with actual equivalent components. (c) Equivalent circuit with idea equivalent components. (d) PI control system of ERS under the model of CBC.

B. Large Signal Time Domain Average Model

The model of ERS is comprised of three parts: the signal average model of boost converter, the system dynamics model, the model of permanent dc motor and system performance calculation model. According to Fig.2 (c) and (d), the inductance L_m currents can follow in continuous conduction mode (CCM) or in discontinuous conduction mode (DCM). The typical inductor current waveform of DCM is shown in Fig.3, where d_1 , d_2 and d_3 are ratio cycle of PWM duty cycle, correspondingly. In CCM, as the $d_3=0$, CCM can be seen as a special condition of DCM.

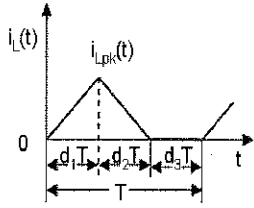


Fig.3 Typical inductor current waveform of DCM

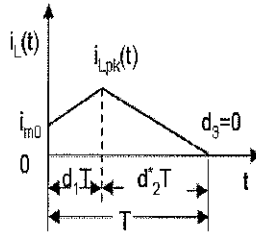


Fig.4 General critical mode

The signal average model of boost converter PI controlled can be obtained by following steps:

$$\begin{cases} \frac{di_m}{dt} = \frac{1}{L_m} [E_m * d_1 + (E_m - E_B) * d_2 + 0 * d_3] \\ d_1 = \frac{U_c}{m_e} f_s \\ U_c = K_p e(t) + K_i \int e(t) dt \\ e(t) = i_i - i_m \end{cases} \quad (4)$$

where K_p and K_i are the coefficients of proportion and integrated, correspondingly.

As the equations for calculating the value of d_2 and d_3 in the mode of CCM and DCM are different, a method of identifying the operation mode by using the past average current of inductance was introduced in paper [5]. Its process of identifying the operation mode as follows:

$$d_2^* = \frac{2 * I_m * f_s * L_m}{E_m * d_1} - d_1 \quad (5)$$

where I_m is the average current of inductance L_m .

If $d_2^* \geq 1 - d_1$, operation in CCM; If $d_2^* < 1 - d_1$, operation in DCM. In CCM and DCM, d_2 and d_3 are decided by the equations of (6) and (7), correspondingly.

$$\begin{cases} d_2 = 1 - d_1; \\ d_3 = 0; \end{cases} \quad (6)$$

And

$$\begin{cases} d_2 = d_2^*; \\ d_3 = 1 - d_1 - d_2; \end{cases} \quad (7)$$

It is obvious to find that the method in paper [5] will delay system analysis for one cycle; this may cause unbeknown question. Considering on that fault, a method based on identifying current of inductance at the start up of each cycle is

introduced in paper [6]. As the current state of inductance at start up can't decide the operation mode (CCM or DCM), there still exists disparity. Further more, the equation (5) is also used in paper [6] and the I_m is the average current of inductance L_m in past time, the delay will also happen; this method can't solve the delay question. Here a new method is introduced.

Supposing that system is operating in critical mode during one cycle (shown in Fig.4), and the start current of inductance in each cycle is i_{m0} , then the duty cycle d_2^* can be obtained at the start up of each cycle by following equation ahead:

$$i_{m0} + \frac{E_m}{L_m} * d_1 * T = \frac{E_B - E_m}{L_m} * d_2^* * T$$

Then,

$$d_2^* = \frac{i_{m0} * f_s * L_m + E_m * d_1}{E_B - E_m} \quad (8)$$

Then, if $d_2^* \geq 1 - d_1$, operation in CCM; If $d_2^* < 1 - d_1$, operation in DCM. In CCM and DCM, d_2 and d_3 are still decided by the equations (6)-(7), correspondingly. As the Equation (8) can identify the operation mode at start up by using current data, it constitutes a state forecast viewer and has solved the above delay question. As the process of calculating the average current of L_m is omitted in the new method, it is helpful to increase the efficiency of simulation. The signal average time domain model of PWM boost converters is comprised of equations (4), (6)-(8).

The model of permanent dc motor driving system is shown in the equations (9).

$$\begin{cases} E_m = K_e * \omega \\ T_e = K_T * i_m \\ F_q = (T_e - \sigma_0 \omega) / r \\ v = \omega * r \end{cases} \quad (9)$$

where K_e is the coefficient of back emf, K_T is the coefficient of electro-magnetic output torque of motor, ω is the angular velocity of motor, σ_0 is the damp coefficient of motor. As the motor with hubcap structures, both the transferring ratio and transferring efficiency are 1.

Based on this model of equations (1)-(4) and (6)-(9), several performances of the CBT can be obtained. During the vehicle run from the start speed v_0 to the speed v_B , the power of energy regeneration P_r is calculated by

$$P_r = E_B * I_m * d_2 \quad (10)$$

The braking distance S_{Brake} and the efficiency of energy regeneration η_{Brake} are calculated by equations of (10) and (11).

$$S_{Brake} = \int_0^{t_B} v dt, \quad ; v(0) = v_0, v(t_B) = v_B \quad (11)$$

$$\eta_{Brake} = \frac{\int_0^{t_B} P_r dt}{0.5 \sigma m (v_0^2 - v_B^2)} \quad (12)$$

All the equations (1)-(4) and (6)-(12) constitute the complete large signal average time domain model of EV.

IV. IMPLEMENT IN MATALB/SIMULINK

Comparing with the simulation with actual components, the signal average method can transform some nonlinear systems to linear systems which can run faster. From the complete large signal average time domain model of EV (equations (1)-(12)),

the ERS of EV with two wheels under the model of CBC is still nonlinear; This nonlinear characteristic causes the question that the signal average time domain model can't be transferred to the system transferring function model and implemented in MATLAB/Simulink surrounding directly. In order to take more advantages from the signal average method as possible as it can, some simply process is being proceed in implementing the signal average time domain model in Matlab/Simulink surrounding. Firstly, considering on 10 kHz frequency of the PWM, the system dynamics model varies in rather lower speed, then the back emf $-E_m$ of dc motor can be seen as a constant variable during one PWM cycle, and then the large signal average model of boost converters (CCM or DCM) can also be seen as a linear model. Secondly, in system dynamics model, only the wind baffle equation is nonlinear. As it has definite analytical equation and varies in rather lower speed, it can be solved by the analytical method in lower frequency. All left model can be transferred to frequency domain model and can be implement in MATLAB/Simulink surrounding directly. This divide the system into two parts: one varies faster, and the other

varies slower. This fast and low system simulation model in MATLAB/Simulink surrounding can be obtained and shown in Fig. 5. Fig. 6 is the detail structure of ERS simulation model. The parameters for simulation as follows:

$K_e=K_T=1.31$, $r=0.28$ m, $v_0=20$ km/h, $v_e=3.6$ km/h, $f_s=10$ KHz, $m_e=5e4$, $E_b=36$ v, $L_m=1.26$ mh, $v_f=0$, $\alpha=0$, $m=110$ kg, $f=0.007$, $A=0.6$ m², $C_d=0.9$, $\rho=1.225$ kg/m. $\delta=1.05$, $\sigma_0=0.015$.

By inputting all above data to simulation model and running, several important performances such as the braking distance, the braking time, the efficiency and the sum of energy regeneration system can be obtained automatically. Further more, the braking distance-S, the energy regeneration efficiency-eff and braking time-t from the 20km/h-3.6km/h under different braking current-Ii can also be calculated. The simulation results are shown in Fig.6 and Fig.7. From the simulation results, it is easy to find that the efficiency of ERS is larger than 21.6%, and the speed of EV, the duty cycle d_2 will tends to smaller while ERS works continuously, all these phenomena are in accordance with analysis result theoretically.

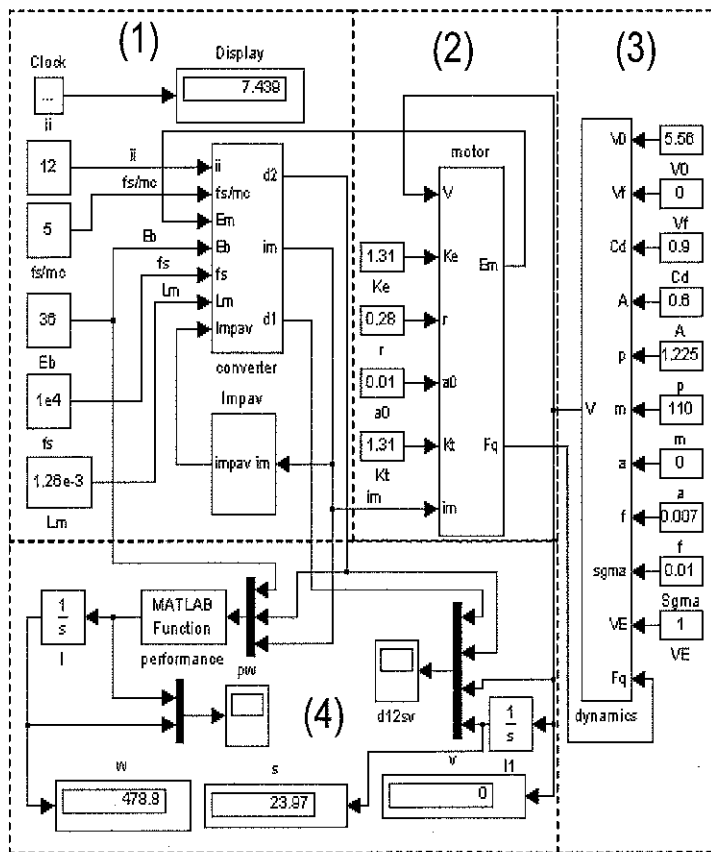
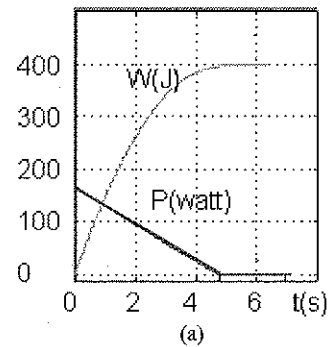
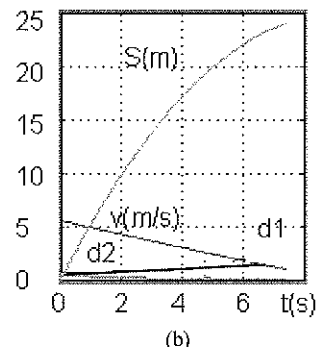


Fig.5 The complete simulation model based on Matlab/Simulink: (1) ERS model; (2) dc motor driving system model; (3) system dynamics model; (4) performance analysis model.



(a)



(b)

Fig.7 Simulation results under the constant braking current-12A: (a) regeneration energy -W and regeneration power-P vs braking time-t; (b) the braking distance-S, the speed during braking-V, the duty cycle-d1 and d2 vs braking time-t.

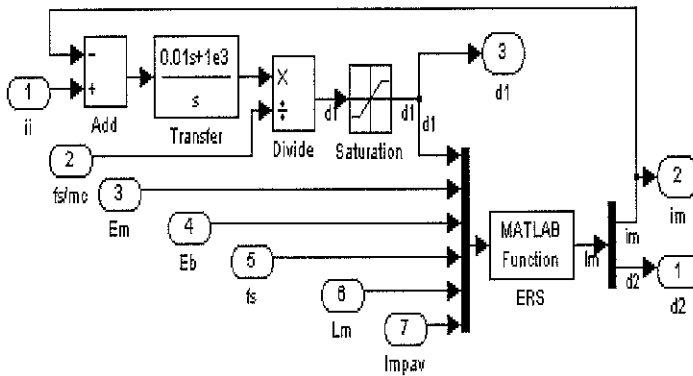


Fig.6 the detail structure of ERS simulation model

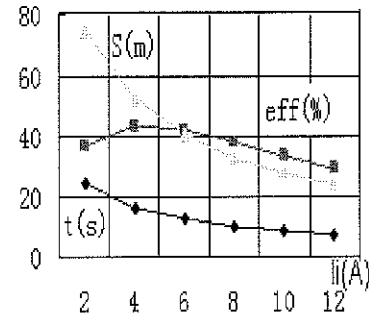


Fig.8 Performance analysis: the braking distance- S , the energy regeneration efficiency- eff and braking time- t from the 20km/h-3.6km/h under different braking current- I_i .

V. CONCLUSIONS

This paper has presented the performance analysis of energy regeneration system (ERS) of electric vehicle (EV) with two wheels under the model of constant braking torque (CBT). A boost equivalent circuit for main power case (MPC) of ERS, the complete model of ERS and its simulation model are obtained. Both the new method based on state forecast viewer for identifying the state (CCM or DCM) of the MPC and the method based on different sampling period for implementing nonlinear system into MATLAB/Simulink surrounding are proposed. The model has proved to be efficient, by running this model, several important performances of ERS for the application in designing ERS are calculated automatically.

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