Investigation into the Design of Ultra-Wideband (UWB) and Multi-band Antennas

 \mathbf{i}

Xiaoning Qiu

Faculty of Engineering University of Technology, Sydney

A Thesis Submitted for the degree of Master of Engineering (Thesis) June 2006

Statement of Originality

I hereby declare that this thesis has not previously been submitted for a degree nor has it been submitted as part of requirements for a degree except as fully acknowledged within the text.

I also certify that the thesis presents my own work and has been written by me. Any help that I have received in my research work and the preparation of this thesis have been acknowledged. In addition, I certify that all information sources and literature used are indicated in the thesis

> Production Note: Signature removed prior to publication.

()_,.,,_ l *Xtc* . 0 *n-. 11/("* ----------------------------- *Ll*

Xiaoning Qiu

Dedication

To my dear parents and relatives, for their love and patience

Abstract

The rapid development of high speed wireless communications as well as other applications such as microwave imaging place extraordinary demands on spectrums for which ultra-wideband (UWB) and multi-band, e.g.: dual-band, techniques are useful. These UWB and multi-band services require UWB and multi-band antenna designs. Motivated by these applications, we first carried out the investigations on the family of square plate monopole (SPM) antennas for UWB applications. The family of square plate monopole (SPM) UWB antennas yields quite attractive features, viz.: ease of fabrication and freedom of dielectric material selection. Next, we considered the use of coplanar waveguide (CPW) fed printed UWB antenna for compact, body-worn applications. We investigated the antenna performance using empirical optimisation. The work on CPW-fed printed antennas has led to the development of multi-band antennas also.

For UWB antennas, we have first considered the modifications of well know square plate monopole (SPM) antennas. Our approach differs from other similar approaches on SPM antennas published in the literature. We have introduced symmetrical modifications to both bottom and top portions of the SPM antenna element. This has led to the development of these types of symmetrically modified SPM antennas, viz.: symmetrically beveled SPM (SB-SPM) antenna, symmetrical semi-circular base SPM (SSCB-SPM) antenna and symmetrically notched SPM (SN-SPM) antenna. All these antennas have been empirically optimised using Feko® and the theoretical and experimental results are provided, in the point of view of reflection coefficient, radiation characteristics, phase response of antenna transfer function and time domain response.

For better suiting the compact and body-worn UWB applications, we have investigated the design of CPW-fed printed antenna. We have explored the antenna characteristics using empirical optimisation. The theoretical and experimental results for the completed CPW-fed printed antenna are provided, in the point of view of reflection coefficient, radiation characteristics, phase response of antenna transfer function, group delay and time domain response.

Lately, for multi-band antennas, we have investigated the design of multi-band printed antennas, which are fed by CPW, to suit emerging design requirements. Two CPW-fed dual-band printed antennas for GSM and DCS/PCS as well as DCS/PCS and IEEE 802.11b applications are proposed, which have C-shape and T-shape structures respective1y. The theoretical and experimental results for these antennas are provided, in the point of view of reflection coefficient and radiation characteristics.

Due to the use of substrate material for the designs of UWB CPW-fed printed antenna as well as C-shaped and T-shaped dual-band CPW-fed printed antennas, the effects of substrate material tolerances on UWB characteristics and dual-band characteristics are investigated. Furthermore, as these UWB and dual-band CPW-fed printed antennas are

the promising candidates for wireless body-worn applications, which include wireless body area network (WBAN), the interactions between them and lossy material, such as human tissue, are investigated, which might help to decide the suitability of them for wireless body-worn applications.

Acknowledgments

A large number of people and organisations have assisted with this thesis written, which contains two years of research work. With all my respect to them, I would like to sincerely and gratefully thank them for their contributions to this thesis.

The first and most must be to thank my supervisor-Associate Professor Ananda Mohan Sanagavarapu (A. S. Mohan), who has shown his expert guidance, advice and knowledge so successfully in supervising his Master and Ph. D students in his research group. With his commitment and encouragement and training, I am able to improve and produce high quality research output during my research candidature, as well as my other group mates. I am so proud and pleasant to take this opportunity to appreciate him for these. Furthermore, the consolidation of my research work and the writing of this thesis and other technical papers during these years cannot be done successfully and smoothly without his efforts, which I want to show my appreciation to him again. Besides the efforts and help from my supervisor, I also need to thank my co-supervisor, Dr. K. K. Fung, who has delivered me lots of great help, advice and encouragement in consolidating my research work. At last, I need to thank Professor Hung T. Nguyen for his leadership in the research and development in Engineering Faculty at UTS.

I would also like to express my deep gratitude to my group mates and colleagues, who were in the past and some currently are the research students of my supervisor. These people are Dr. Andrew R. Weily, Dr. Heng-Mao (Hank) Chiu, Dr. Zhongwei (David) Tang, Dr. Kwok L. Chung and Mr. Tony Huang. The first person I mostly want to thank is Dr. Heng-Mao (Hank) Chiu. I earnestly appreciate his patience, intelligence and

sincere help and guidance at the early stage of my research work. It is really an honour to me to know this person. Dr. Zhongwei (David) Tang is not only a friend to me, but a mentor in many other aspects of my life. Dr. K wok L. Chung influenced me much with his diligence and precision in every tiny piece of thing he does and encouraged me to pursue the best in my work. I really appreciate these above people who helped me to get trained to be a good researcher. It is such a pleasure for me to know and thank Dr. Andrew R. Weily for his enthusiastic help and support in using the Near-field Systems for antenna radiation patterns measurements. I value his friendly and intelligent advice. At last, I would like to give me appreciation to Mr Tony Huang, who is one of the most intelligent people I have met, especially in the field of software. During these two years, he has taught and helped me a lot, especially in programming and writing, although he often pretends not to be interested in anything to do with this field.

I am grateful to Rosa Tay, Mr. Ray Clout and Richard Tumell for their kind supports and technical help during my research candidature as well.

I would like to acknowledge that the work reported in this thesis is part of an Australian Research Council funded Discovery Project Grant: DP0346540 as well as a UTS internal Research Excellence Grant.

Table of Contents

List of Figures

SPM) notched SPM antennas 33

- Fig. 2.7 Prototypes of the symmetrically modified SPM antennas: (a) SB-SPM antenna and (b) SSCB-SPM antenna (Continued in next page) ... 34
- Fig. 2.7 (Continued from last page) Prototypes of the symmetrically modified SPM antennas: (c) SN-SPM antenna 35
- Fig. 2.8 Reflection coefficient comparisons between asymmetrically and symmetrically modified SPM antennas (a) SB-SPM and ASB-SPM antennas; (b) SSCB-SPM and ASSCB-SPM antennas (Continued in next page) ... 36
- Fig. 2.8 (Continued from last page) Reflection coefficient comparisons between asymmetrically and symmetrically modified SPM antennas (c) SN-SPM and ASN-SPM antennas .. 37
- Fig. 2.9 (a) Bandwidth below -1 OdB comparison between SB-SPM and ASB-SPM antennas with $BW = 15$ mm and BH varying from 1mm to 15mm. (b) Percentage bandwidth below -15dB comparison of SB-SPM antenna between $BH = 6, 7, 8$ and 9mm with BW varying from 1mm to 15mm. (c) Bandwidth below -10dB comparison between SB-SPM and ASB-SPM antennas with BH = 7mm and BW varying from 1mm to l5mm. (d) Bandwidth comparison of impedance bandwidth lower than -15dB in UWB band (3.1GHz-10.6GHz) between SB-SPM and ASB-SPM antennas with BH = 7mm and BW varying from l mm to 15mm 39
- Fig. 2.10 (a) Bandwidth below -lOdB comparison between SSCB-SPM and ASSCB-SPM antennas with R varying from 1 to 15mm, (b) Percentage bandwidth below - 15dB comparison between SSCB-SPM and ASSCB-SPM antennas with R varying from 1 to 15mm ... 40
- Fig. 2.11 (a) Bandwidth below -IOdB comparison between SN-SPM and ASN-SPM antennas with $NW = 7$ mm and NH varying from 1mm to 14mm. (b) Bandwidth below -10dB comparison between SN-SPM and ASN-SPM antennas with $NH =$ 3rnm and NW varying from lmm to 14mm .. 41
- Fig. 2.12 (a) Coefficient of omni-directionality vs. frequency of SB-SPM antenna (Fig. 2.7 (a)); (b) xy-plane normalised radiation patterns of SB-SPM antenna at spot frequency 4.5GHz; (c) xy-plane normalised radiation patterns of SB-SPM antenna at spot frequency 7.5GHz and (d) xy -plane normalised radiation patterns of SB-SPM antenna at spot frequency 10.5GHz ... 42
- Fig. 2.13 (a) Coefficient of omni-directionality vs. frequency of SSCB-SPM antenna (Fig. 2.7 (b)); (b) xy-plane normalised radiation patterns of SSCB-SPM antenna at spot frequency 4.5GHz; (c) xy-plane normalised radiation patterns of SSCB-SPM antenna at spot frequency 7.5GHz and (d) xy-plane normalised radiation patterns of SSCB-SPM antenna at spot frequency 1 0.5GHz .. 43
- Fig. 2.14 (a) Coefficient of omni-directionality vs. frequency of SN-SPM antenna (Fig. 2.7 (c)); (b) xy-plane normalised radiation patterns of SN-SPM antenna at spot frequency 4.5GHz; (c) xy-plane normalised radiation patterns of SN-SPM antenna at spot frequency 7.5GHz and (d) xy-plane normalised radiation patterns of SN-SPM antenna at spot frequency 1 0.5GHz .. .44

X

- Fig. 2.15 The antenna positioning schemes for a link in 3-D schematic diagrams on separate ground planes and a single ground plane: (a) Face to face; (b) Side by side and (c) Face to side. For simplicity, square plate monopole (SPM) antenna is used in these schematic diagrams .. 46
- Fig. 2.16 Phase response of SB-SPM antenna for configurations shown in Figs. 2.15 .. 47
- Fig. 2.17 Phase response of the SSCB-SPM antenna for configurations shown in Figs. 2.15 (Continued in next page) ... 47
- Fig. 2.17 (Continued from last page) Phase response of the SSCB-SPM antenna for configurations shown in Figs. 2.15 ... 48
- Fig. 2.18 Phase response of the SN-SPM antenna for configurations shown in Figs. 2.15 ... 48
- Fig. 2.19 (a) Waveform of input pulse and (b) power spectral density of the input pulse normalised to the FCC indoor and out door EIRP masks 50
- Fig. 2.20 Analytical model of system configuration with a pair of antennas for the theoretical investigations ofUWB time-domain characteristics 50
- Fig. 2.21 (Continued from last page) Normalised received waveforms of UWB pulses for the SB-SPM antenna for configurations shown in Figs. 2.15. The dotted waveforms at the left indicate the normalised transmitted UWB pulse....................53
- Fig. 2.22 Normalised received waveforms of UWB pulses for the SSCB-SPM antenna for configurations shown in Figs. 2.15. The dotted waveforms at the left indicate the normalised transmitted UWB pulse .. 53
- Fig. 2.23 Normalised received waveforms of UWB pulses for the SN-SPM antenna for configurations shown in Figs. 2.15. The dotted waveforms at the left indicate the normalised transmitted UWB pulse 54
- Fig. 2.24 Bandwidth comparison of SB-SPM antenna with dimension schemes shown in Beveled column of Table 2.4. Subscripts "B" and "T" stand for bottom and top respectively. (Continued in next page) 57
- Fig. 2.24 (Continued from last page) Bandwidth comparison of SB-SPM antenna with dimension schemes shown in Beveled column of Table 2.4. Subscripts "B" and "T" stand for bottom and top respectively 58
- Fig. 2.25 Bandwidth comparison of SSCB-SPM antenna with dimension schemes shown in Semi-Circular Base column of Table 2.4. Subscripts "B" and "T" stand for bottom and top respectively .. 58
- Fig. 2.26 Bandwidth comparison of SN-SPM antenna with dimension schemes shown in Notched column of Table 2.4. Subscripts "B" and "T" stand for bottom and top respectively 59

Fig. 3.1 The initial prototype of the antenna which formed basis for improvement. 66

- Fig. 3.2 (a) Electric field and (b) Magnetic field on the cross-section plane of CPW at spot frequency of *S.SGHz* ... 67
- Fig. 3.3 (a) Distributions of magnetic field and (b) electric field on prototype antenna at spot frequency of *S.SGHz* ... 67
- Fig. 3.4 (a) Schematic diagram of the coplanar waveguide, (b) Side view of the proposed CPW-fed antenna element shown in Fig 3.1 ... 69
- Fig. 3.5 (a) Comparison of centre conductor width of CPW versus its slot width with $h =$ 1.524mm, $Z_0 = 50\Omega$ and $\varepsilon_r = 2.2, 3.38, 4.4, 6.15$ and 10.2; (b) Comparison of centre conductor width of CPW versus its slot width with $\varepsilon_r = 3.38$, $Z_0 = 50\Omega$ and h = O.S08mm, 0.813mm and l.S24mtn .. 71
- Fig. 3.6 Input characteristic impedance of coplanar waveguide with dimensions of ε_r = 3.38, h = 1.S24mm, Wr= *S.Smm* and g = 0.3mm ... 72
- Fig. 3.7 Antenna geometries with single-notched-step (SNS) modifications investigated in *Step 3 a):* (a) modifications applied only at bottom; (b) modifications applied only at top; (c) modifications applied at both bottom and top of the horizontal slots ······················· ···························· ································ ······································ ···· 73
- Fig. 3.8 Comparison of reflection coefficients for SNS modifications applied only at bottom, only at top and at both bottom and top of the horizontal slots. The dimensions of SNS modifications are (a) $NW = 6$ mm and $NH = 2$ mm and (b) NW = 6mm and NH = 3mm 74
- Fig. 3.9 General antenna geometry with SNS modifications investigated in *Step 3 b) .. 7S*
- Fig. 3.10 A designation method for categorising the cases in investigations 76
- Fig. 3.11 Comparison of reflection coefficients between VMOB and VMOT for: (a) *wfive-two-three* cases; (b) *h-two-six-five* cases; (c) w~six-two-three cases; (d) *hthree-six-five* cases; (e) *w-seven-three-four* cases; (f) *h-four-seven-six* cases 81
- Fig. 3.12 Comparison of reflection coefficients between different variables: (a) *w-fivethree-four* cases; (b) *h-four-five-six* cases; (c) *w-six-two-three* cases; and (d) *hthree-six-six* cases 82
- Fig. 3.13 Comparison of reflection coefficients between different sub-classes: (a) *w-six*cases and (b) *h-three-* cases 83
- Fig. 3.14 Enlarged illustration of the centre portion of the antennas studied in *Step 4* .. 84
- Fig. 3.15 Comparison of reflection coefficients for antennas studied in *Step 4,* between different gap widths 8S

xii

- Fig. 3.16 (a) Illustration of antenna configuration after introducing symmetrical SNS modifications; (b) Antenna configuration with further symmetrical SNS modifications; (c) Antenna configuration with further symmetrical SBS modifications ... 86
- Fig. 3.17 Comparison of reflection coefficients between further symmetrical SNS and SBS modifications: (a) $NH = BH = 1.5$ mm, $NW = BW = 3$ mm; (b) $NH = BH =$ 2mm, NW = BW = 4mm ... 88
- Fig. 3.18 Comparison of reflection coefficients between different BW for further symmetrical SBS modifications when BH = 1.5mm 88
- Fig. 3.19 (a) Comparison of reflection coefficients between different L1; (b) Comparison of xy-plane normalised co-polarization component at 8.5GHz between different L1 ... 89
- Fig. 3.20 (a) Comparison of reflection coefficients between different L2; (b) Comparison of xy-plane normalised co-polarization component at 8.5GHz between different L2 ... 90
- Fig. 3.21 (a) The geometry and (b) prototype of the compact printed CPW-fed UWB antenna .. 92
- Fig. 3.22 The simulated and measured reflection coefficients of the proposed printed CPW-fed UWB antennas .. 93
- Fig. 3.23 The coefficient of omni-directionality vs. frequency of the compact printed CPW-fed antenna 94
- Fig. 3.24 xy-plane normalised radiation patterns of the compact printed CPW-fed antenna at (a) 4.5GHz, (b) 6.5GHz, (c) 8.5GHz and (d) 10.5GHz 95
- Fig. 4.1 Hypothetical antenna model for theoretical modelling of signal dispersion: (a) front view and (b) top view 101
- Fig. 4.2 The antenna positioning schemes for a link in 3-D schematic diagrams. (a) Face-to-face with substrates facing each other, (b) Narrow sides of substrate facing each other with antennas looking at identical direction (Continued in next page) 105
- Fig. 4.2 (Continued from last page) The antenna positioning schemes for a link in 3-D schematic diagrams. (c) Face-to-face with antennas facing each other, (d) Narrow sides of substrate facing each other but antennas looking at opposite directions, (e) Narrow side of one substrate facing antenna of the other one forming a T-section, (f) Narrow side of one substrate facing the wide substrate side of the other one forming a T -section and (g) Antenna side of one facing the wide substrate side of the other one. The black and grey areas indicate the copper and substrate of the printed antenna 106
- Fig. 4.3 The phase response of the compact printed antenna in the antenna positioning schemes shown in Fig. 4.2 (a) Face-to-face with substrates facing each other, (b)

Narrow sides of substrate facing each other with antennas looking at identical direction, (c) Face-to-face with antennas facing each other, (d) Narrow sides of substrate facing each other but antennas looking at opposite directions, (e) Narrow side of one substrate facing antenna of the other one forming a T-section, (f) Narrow side of one substrate facing the wide substrate side of the other one forming aT -section. (Continued in next page) ... 107

- Fig. 4.3 (Continued from last page) The phase response of the compact printed antenna in the antenna positioning schemes shown in Fig. 4.2 (g) Antenna side of one facing the wide substrate side of the other one ... 108
- Fig. 4.4 The group delays of compact printed antennas in the antenna positioning schemes shown in Fig. 4.2 .. 108
- Fig. 4.5 (a) Waveform of input pulse and (b) power spectral density of the input pulse normalised to the FCC indoor and out door EIRP masks 11 0
- Fig. 4.6 Normalised received waveforms of UWB pulses for the compact CPW-fed printed antenna in the antenna positioning schemes shown in Figs. 4.2 (a) Substrate face substrate, (b) Side by side with coppers facing identical, (c) Copper face copper, (d) Side by side with copper facing opposite, (e) T -shaped relative position with one copper side facing inwards and (f) T-shaped relative position with one copper side facing outwards. The dotted waveforms at the left indicate the normalised transmitted waveform of UWB pulse. (Continued in next page)....... 111
- Fig. 4.6 (Continued from last page) Normalised received waveforms of UWB pulses for the compact CPW-fed printed antenna in the antenna positioning schemes shown in Figs. 4.2 (g) Copper side of one antenna facing the substrate side of the other one antenna. The dotted waveforms at the left indicate the normalised transmitted waveform of UWB pulse 112
- Fig. 4.7 The variation of reflection coefficients for the UWB CPW-fed printed antenna due to dielectric constant and thickness tolerances on substrate $RO4003CTM$ in four extreme-case scenarios 115
- Fig. 4.8 The variation of coefficients of omni-directionality vs. frequency for the UWB CPW-fed printed antenna due to dielectric and constant thickness tolerances on Rogers® R04003C ™ in four extreme-case scenarios .. 116
- Fig. 4.9 (a) Geometry of the printed CPW-fed UWB antenna, the units are in mm; (b) Side view and top view of a lossy circular cylinder placed close to the antenna. 118
- Fig. 4.10 Reflection coefficients of UWB printed antenna close to a lossy cylinder with spacing D = 2, 8, 15 and 25mm .. 119
- Fig. 4.11 Normalised radiation patterns at spot frequency 4.5GHz: (a) $D = 2$ mm, (b) D = 8mm. (c) D = 15 mm and (d) D = 25mm ... 119

Fig. 4.12 (a) Front-to-back ratio and (b) front-to-side ratio of co-polarization component of radiation patterns for the printed antenna in the presence of lossy cylinder for different spacing D = 2, 8 and 25mm .. 120

Fig. 4.13 Power absorbed of lg lossy material due to the UWB CPW-fed printed antenna with spacing $D = 15$ mm: (a) 4.5GHz; (b) 6.5GHz; (c) 8.5GHz and (d) 10.5GHz .. 122

Fig. 4.14 Power absorbed of lOg lossy material due to the UWB CPW-fed printed antenna with spacing $D = 15$ mm: (a) 4.5 GHz; (b) 6.5 GHz; (c) 8.5 GHz and (d) 10.5GHz .. 123

Fig. 5.1 Empirical model of dual-band antenna, (a) monopole antennas and (b) idea behind dual-band antenna ... 130

- **Fig. 5.2** Proposed structure of the dual-band C-shaped CPW-fed printed antenna (unit: mm) ... 132
- Fig. 5.3 Current distributions of dual-band C-shaped CPW-fed printed antenna with identical scale: (a) 0.9GHz, (b) 1.8GHz and (c) 2.65GHz 134
- **Fig. 5.4** The comparison of simulated reflection coefficients of proposed dual-band Cshaped CPW -fed printed antenna with gap distance (the distance between the bottom of the C-shaped element and the ground plane) of 7, 10, 13, and 16mm respectively ... 135
- **Fig. 5.5** The comparison of simulated reflection coefficients of proposed dual-band Cshaped CPW-fed printed antenna with gap distance (the gap distance of the mouth ofthe C-shaped element) of2, 3, and 4mm respectively l35
- **Fig. 5.6** The comparison of simulated reflection coefficients of proposed dual-band Cshaped CPW-fed printed antenna with different (a) widths and (b) heights of the ground planes .. 13 7
- **Fig.** 5.7 Proposed structure of the dual-band T-shaped CPW-fed printed antenna (unit: mm) ... 138
- **Fig. 5.8** Current distributions of printed dual-band T-shaped CPW-fed antenna with identical scale: (a) 1 .85GHz and (b) 2.4GHz .. l39
- **Fig. 5.9** The schematic diagram for the investigation on the effect of the length of the horizontal strip of the L-shaped element for the proposed T-shaped antenna 141
- **Fig. 5.10** The comparison of simulated reflection coefficients of proposed dual-band Tshaped CPW-fed printed antenna, studied in Fig. 5.15, with lengths of -3.5, 0, 3, 6.5, 10.5, 14.5 and 18.5mm for the horizontal strip of L-shaped element. $^{(1)}$ The minus value represents the short-circuited L-shape element residing at the right side of the vertical strip of the T-shaped element.⁽²⁾ Zero represents that no short circuiting L-shaped element is used .. 141

XVI

- **Fig. 5.25** Radiation patterns of T-shaped CPW-fed printed antenna with spacing $D =$ 2mm and 15mm to the lossy cylinder at resonant frequencies: (a) 1.85GHz and (b) 2.5GHz .. 157
- **Fig. 5.26** Power absorbed of 1g and 10g lossy material due to the dual-band C-shaped CPW-fed printed antenna with spacing $D = 15$ mm: (a) 0.9GHz and (b) 1.8GHz 158
- **Fig. 5.27** Power absorbed of lg and lOg lossy material due to the dual-band T-shaped CPW-fed printed antenna with spacing $D = 15$ mm: (a) 1.85GHz and (b) 2.5GHz 159
- **Fig. A.l** Antenna measurement conducted by the author inside the anechoic chamber at CSIRO ICT centre. Photo courtesy of Dr. Andrew Weily of Macquarie University, NSW, Australia 180

xvii

List of Tables

Table 4.1 Summary of fidelity factor between the transmitting and receiving UWB pulses for the CPW -fed printed antenna in the antenna positioning schemes of Fig. 4.2 .. 113

List of Acronyms

