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# Investigation of a Proposed Long Span Timber Floor for Non-Residential Applications

By

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BEng, MEngSc (From BIHE)

Thesis submitted in fulfilment of requirements for the degree of **Doctor of Philosophy** 

October 2014

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#### **ABSTRACT**

Design of floor systems for commercial and multi-residential buildings in many parts of the world is currently dominated by the use of structural materials other than timber, such as reinforced concrete systems. Recent research in Australia has shown that the major barriers to using timber in non-residential buildings are the fire performance and the lack of designer confidence in commercial and industrial timber-based constructions. In this regard, significant research initiatives have commenced in Australia and New Zealand with the aim of developing timber and timber hybrid systems for large span commercial and industrial applications. This PhD research provides a detailed procedure for designing and investigating the short term static behaviour of a proposed long span timber floor system for non-residential applications that meets serviceability and ultimate limit design criteria, with the use of timber as the only structural load bearing part of the system. The specimen's responses to long-term loading, in-plane loading, dynamic excitation, cyclic loading and loading history are outside the scope of this PhD research. Moreover, other aspects of performance such as assessment of acoustic performance, dynamic performance and the possible interconnection systems alongside floor modules are not covered in the scope of this research project.

In this study the behaviour of two types of LVL are investigated through a number of experimental and analytical tests. As a result of the tension and compression tests, a suitable constitutive law is developed which can accurately capture the stress-strain relationship and the failure behaviour of LVL, and it can also be incorporated into FE analysis of any LVL beam with similar structural features to the tested specimens. Further, the results of the full scale four point bending tests on LVL sections are used to identify the behaviour of LVL up to the failure point and to develop a finite element model to capture the behaviour and failure of LVL.

Moreover, after investigating the long span timber floors, one system is proposed to be fabricated for the extensive experimental and numerical investigation. The experimental investigation involved subjecting the full scale proposed floor modules (6m and 8m

clear span LVL modules) to both serviceability and ultimate limit state static loading to assess the strength and serviceability performance of the proposed system. A continuum-based finite element model is also developed to capture the behaviour and failure of the long span LVL modules and to adequately predict the serviceability and ultimate limit performance of the proposed floor system.

To evaluate the partially-composite strength and serviceable performance of LVL floor system, a series of push-out tests are conducted on the fabricated timber connections using normal screws as the shear connectors, and the stiffness of the connections are assessed at serviceability and ultimate limit state. A number of LVL beams (3.5m "T" shaped beams) were also fabricated using only normal screws as the load bearing shear connectors at the interfaces, and are tested under serviceability and ultimate limit state loads with different screw spacing. Furthermore, a closed-form prediction analysis is conducted to calculate the partially-composite ultimate load of the beams. A comparison between the experimental results and the closed-from predicted results is undertaken, and the results are used for predicting the partially-composite behaviour of long span 6m and 8m LVL modules.

The results of the full scale experimental tests together with the numerical investigation provide a robust model for predicting the performance of any timber beams with similar structural features to the proposed system while the dimensions and spans can be varied according to special requirements such as dynamic performance or fire resistance requirements.

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### LIST OF PUBLICATIONS BASED ON THIS THESIS

Zabihi, Z., Samali, B., and Crews, K. (2010), "Modern trends in long span timber flooring systems", *Proceedings, 21<sup>st</sup> Australasian Conference on the Mechanics of Structures and Materials, ACMSM 21*, Melbourne, Australia, 7-10 December.

Zabihi, Z., Samali, B., Shrestha, R., Gerber, C. and Crews, K. (2012), "Serviceability and Ultimate Performance of Long Span Timber Floor Modules", *Proceedings, Twelfth World Conference on Timber Engineering, WCTE 2012*, Auckland, New Zealand, 16-19 July.

Zabihi, Z., Samali, B., Shrestha, R., and Crews, K. (2012), "Ultimate Performance of Timber Connection with Normal Screws", *Proceedings, 22<sup>nd</sup> Australasian Conference on the Mechanics of Structures and Materials, ACMSM 22*, Sydney, Australia, 11-14 December.

#### LIST OF NOTATIONS

 $\alpha$  modification factor in Glos model

 $\alpha_{\scriptscriptstyle ff}$  distance between point of zero bending moment to centroid of top

flange

 $lpha_{\it bf}$  distance between point of zero bending moment to centroid of bottom

flange

 $\alpha_{tf}$  distance between point of zero bending moment to centroid of web

 $\gamma_{tf}$  partial factor for material properties of the top flange

 $\gamma_{bf}$  partial factor for material properties of the bottom flange

 $\gamma_{web}$  partial factor for material properties of the web

 $\delta_{max}$  maximum mid span deflection

 $\delta_{Mid}$  measurements of LVDTs under mid-span measurements of LVDTs under third-span

 $\epsilon_t$  tensile strain

 $\epsilon_c$  compressive strain  $\epsilon_0$  strain coefficient

 $\phi$  Capacity factor for imposed load as per AS1720.1 (2010)

 $\phi N$  axial design capacity of the timber cross-section  $\phi M$  bending design capacity of the timber cross-section  $\phi N_p$  bearing design capacity of the timber cross-section

 $\phi\sigma_{tf.axial}$  top flange axial stress design capacity

 $\phi\sigma_{bf,axial}$  bottom flange axial stress design capacity

 $\phi\sigma_{tf.bending}$  top flange bending stress design capacity

 $\phi\sigma_{bf.bending}$  bottom flange bending stress design capacity

 $\rho$  density

 $\sigma^*_{tf,axial}$  axial stress in top flange due to design action

 $\sigma^*_{bf,axial}$  axial stress in bottom flange due to design action

 $\sigma^*_{tf,bending}$  bending stress in top flange due to design action

 $\sigma^*_{bf,bending}$  bending stress in bottom flange due to design action

 $\sigma_{f,t,\max}$  tensile design stress of the extreme fiber of flange

 $\sigma_{f,t}$  mean tensile design stress of the flange

v Poisson's ratio

v relative slip of timer connections

Ψ coefficient for long term load combination

 $\Delta F/\Delta e$  linear elastic slope of the load-displacement graph

 $\Delta_{vib}$  mid span deflection of the floor beams as a result of impact loading

 $\Delta_b$  mid span flexural deflection of the floor beams

1-D one-dimensional
2-D two-dimensional
3-D three-dimensional
A<sub>tf</sub> top flange area

A<sub>bf</sub> bottom flange area

 $A_{\rm w}$  web area

b width (breadth) of the timber cross section

b<sub>tf</sub> top flange width

b<sub>bf</sub> bottom flange width

b<sub>w</sub> web width

CoV coefficient of variation

d total depth of the timber cross section

d<sub>tf</sub> top flange depth

d<sub>tf</sub> bottom flange depth

 $d_{\mathrm{w}}$  web depth

E<sub>tf</sub> top flange modulus of elasticity

E<sub>bf</sub> bottom flange modulus of elasticity

E<sub>w</sub> web modulus of elasticity

E modulus of elasticity

 $E_t$  modulus of elasticity in tension

 $E_c$  modulus of elasticity in compression

EI flexural stiffness

(EI)<sub>eff, LT</sub> long term effective flexural stiffness

 $(EI)_{eff}$ effective flexural stiffness $(EI)_{Mid}$ flexural stiffness at mid-span $(EI)_{Trd}$ Flexural stiffness at third-span

F, P point load  $F_{est}$  peak load

*F<sub>max</sub>* Ultimate/failure load

 $F_{ave}$  average reading of load cells 1 and 2

 $F_{bf}$  shear load on a single screw in bottom flange  $F_{tf}$  shear load on a single screw in bottom flange

 $f'_b$  characteristic strength in bending (bending design capacity)

 $f'_c$  characteristic strength in compression (compression design capacity)

f's characteristic strength in shear (shear design capacity)

 $f'_{s,glue}$  shear strength (shear design capacity) of glue

 $f'_t$  characteristic strength in tension (tensile design capacity)

 $f'_{b,bf}$  top flange bending strength (design capacity)  $f'_{b,bf}$  bottom flange bending strength (design capacity)

 $f'_{b,w}$  web bending strength (design capacity)

 $f'_{t,tf}$  top flange tension strength (parallel to grain) (design capacity)  $f'_{t,bf}$  bottom flange tension strength (design capacity) parallel to grain

 $f'_{t,w}$  web tension strength (design capacity) parallel to grain

 $f'_{c,tf}$  top flange compression strength(design capacity) parallel to grain

f'c,bf bottom flange compression strength (design capacity) parallel to grain

 $f_{c,w}$  web compression strength (design capacity) parallel to grain

 $f'_{s,tf}$  top flange shear strength(design capacity)

 $f'_{s,bf}$  bottom flange shear strength (design capacity)

 $f'_{s,w}$  web shear strength (design capacity)

 $f_1$  fundamental frequency (first natural frequency of the structure)

 $f_s^*$  shear stress due to loading (design action)

f'<sub>p</sub> bearing strength of the bottom flange

 $f_b$  mean bending strength

 $f_c$  mean compression strength

 $f_t$  mean tension strength

f<sub>c,y</sub> yielding compression strength

 $f_t$  mean tensile strength  $f_v$  mean shear strength

G self-weight & permanent loading

g acceleration due to gravity  $(9.81 \text{ m/s}^2)$ 

 $G_s$  shear modulus; Modulus of rigidity

h<sub>tf</sub> distance between the neutral axis of the cross section and the centroid

of htop flange

h<sub>w</sub> distance between the neutral axis of the cross section and the centroid

of webs

h<sub>bf</sub> distance between the neutral axis of the cross section and the centroid

of botom flanges flange

I moment of inertia

 $I_{eff}$  effective moment of area

*j*<sub>2</sub> creep factor (stiffness modification factor)

K stiffness

 $K_{Mid}$  stiffness at third-span of the beam  $K_{Trd}$  stiffness at mid-span of the beam  $K_i$  initial stiffness of the connection

 $K_{s,0.4}$  serviceability stiffness

 $K_{s,0.6}$  ultimate stiffness  $K_{s,0.8}$  near collapse

 $K_p$  the strain-hardening stiffness in Richard-Abbott model

 $K_0$  initial stiffness in Richard-Abbott model

 $k_1$  duration of load (timber)  $k_{12}$  stability factor (timber)

 $k_4$  moisture condition factor (timber)

 $k_6$  temperature factor (timber)

 $k_7$  length and position of bearing factor (timber)

*k*<sub>9</sub> strength sharing between parallel members factor (timber)

 $K_{(II)}$  coefficient factor in Glos model

 $K_{(22)}$  coefficient factor in Glos model  $K_{(33)}$  coefficient factor in Glos model  $K_{(44)}$  coefficient factor in Glos model

 $(K_{(11)})_{mod}$  modified coefficient factor in Glos model

L span of the floor modules or length of the timber beams

LL live Load

LVDT Linear Variable Differential Transformers m mass of the floor; mass per unit area (kg/m<sup>2</sup>)

 $M^*$  maximum bending moment due to design action

MCmoisture content $M_0$ oven dried mass

 $M_i$  initial mass N.A. neutral axis

N power in Glos model (chapter 4)

 $N^*$  maximum axial force due to design action

N\*<sub>p</sub> bearing load due to design action

n a parameter associated with the sharpness of the curve in Richard-

Abbott

 $n_w$  modular ratios for web of the LVL modules (Chapter 3)

 $n_{bf}$  modular ratios for bottom flange of the LVL models (Chapter 3)

 $P_0$  reference shear force in in Richard-Abbott model

 $Q_{tf}$  first moment of area of top flange about the neutral axis

 $Q_{bf}$  first moment of area of bottom flange about the neutral axis

 $Q_{max}$  maximum first moment of area

Q imposed loading

R<sup>2</sup> coefficient of determination

S joist spacing

SDL superimposed permanent load

S<sub>s</sub> screw spacing

S<sub>tf</sub> screw spacing in top flange interface

S<sub>bf</sub> screw spacing in bottom flange interface

 $V^*$  maximum acting shear force (shear force due to design action)

$\bar{y}_c$ , $y_c$	neutral axis of the LVL floor module
$\overline{\mathcal{Y}}$ tf	location of centroid of top flange from the base of the cross section
$\overline{\mathcal{Y}}_{\mathrm{w}}$	location of centroid of web from the base of the cross section
$y_{ m bf}$ , $\overline{\mathcal{Y}}$ $_{ m bf}$	location of centroid of bottom flange from the base of the cross section
ybf/2	the distance between the half of the depth of bottom flange and the
	centroid of the section