

Coprime Factor Model Reduction for Discrete-time Uncertain Systems

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Abstract

This paper presents a contractive coprime factor model reduction approach for discrete-time uncertain systems of LFT form with norm bounded structured uncertainty. A systematic approach is proposed for coprime factorization and contractive coprime factorization of the underlying uncertain systems. The proposed coprime factor approach overcomes the robust stability restriction on the underlying systems which is required in the balanced truncation approach. Our method is based on the use of LMIs to construct the desired reduced dimension uncertain system model. Closed-loop robustness is discussed under additive coprime factor perturbations.

Keywords: Model reduction; Uncertain systems; Discrete-time systems; Coprime factorization

1. Introduction

This paper addresses the coprime factorization (CF) and model reduction problems for discrete-time uncertain systems which are possibly *robustly unstable*. The uncertain systems under consideration are described in terms of linear fractional transformations (LFTs) [1] with structured norm bounded uncertainty.

Model reduction has been an active research area in the control society since 1960s. A large number of model reduction methods have appeared in the literature, among which one of the most commonly applied methods for stable linear time invariant (LTI) systems is the balanced truncation method [2] with guaranteed error bounds [3, 4]. For unstable LTI systems, a coprime factor approach [5] is proposed to avoid the stability issues. Discrete-time related topics can be found, for example, in [6, 7] and the references therein.

Model reduction problems for uncertain systems have attracted much attention in recent years; see, for example, LFT systems [8, 9, 10, 11, 12, 13], gain scheduling [14, 15], linear parameter-varying systems [16, 17, 18, 19], linear time-varying systems [20, 21], nonlinear systems [22], linear parameter dependent (LPD) systems [23], and related approximation, truncation and simplification problems [24, 25]. The balanced truncation method for *robustly stable* uncertain systems is studied in [8, 9, 26] within the LFT framework. Concerning those uncertain systems which may be *robustly unstable*, a coprime factorization based approach is proposed in [12], which extends coprime factor approach [5] for LTI systems to the underlying uncertain systems. However, no indication is given in [12] on the contractiveness of the resulting coprime factors. This motivates the question as to whether a contractive CF can be obtained for uncertain systems. Contractive CF, as an alternative to normalized CF, has properties similar to normalized CF. In the meanwhile, it enables us to take advantage of linear matrix inequality (LMI) techniques, providing more flexibility to accommodate structure constraints including topological structures and uncertainty structures, and thus can be effectively solved by available softwares. Particularly for discrete-time uncertain systems, contractive CF is motivated by the following two observations. Firstly, for discrete-time LTI systems, applying balanced truncation to normalized coprime factors of original systems would result in contractive coprime factors of reduced systems, rather than normalized ones as in continuous cases. Therefore, it is not necessary to consider normalized CF in the first place in balanced truncation approaches. Secondly, in the presence of uncertainty, it is very difficult to obtain normalized coprime factors for the underlying systems because the corresponding Riccati equations are hard to solve and most probably lead to infeasible solutions.

In this paper, the coprime factor model reduction problem studied in [12] is revisited. The study of this problem is based on the results in [12] and the author's previous work on uncertain systems [26, 10, 13, 23]. In [26, 10, 23], model reduction problems for two classes of continuous uncertain systems are studied. By introducing generalized controllability and observability Gramians, balanced truncation and balanced LQG truncation model reduction approaches are investigated. In this paper, following the idea of balanced LQG truncation, instead of just balancing the solutions to the control/filter Riccati inequalities, coprime factors are constructed based on Riccati inequalities. The advantage of coprime factor model reduction over balanced LQG truncation is that coprime factor model reduction can provide quantitative robust stability margin which will be discussed in Section 5. In [13], coprime factor model reduction for a class of continuous-time uncertain systems is investigated. In this paper the method is extended to

discrete uncertain systems. It should be emphasized here that this extension is not trivial because of the significant difference between continuous and discrete systems especially in the presence of uncertainty. The contribution of this paper, compared to the results of [12], is three folds. Firstly, we eliminate the full column rank restriction on the B-matrix in [12], providing a more general solution to constructing coprime factorization for uncertain systems. Secondly, a systematic approach to obtain the coprime factorization for the underlying uncertain systems is presented based on the use of LMIs. A sufficient and necessary condition to ensure the feasibility of the derived LMI is also specified. Contractiveness is subsequently accomplished by choosing a specific feedback gain, which extends the similar LTI results to the uncertain systems under consideration. This enables us to apply balanced truncation [8, 9] to the resulting contractive coprime factors to obtain the reduced-order uncertain systems. It is shown that the resulting reduced coprime factors are contractive as well. Thirdly, closed-loop robustness is discussed for the reduced uncertain system under model reduction error on coprime factors. A sufficient condition is presented to guarantee the closed-loop stability when the original model is replaced by the reduced model. This robustness property could potentially contribute to the analysis of gap metric for uncertain systems which will be the topic of future research. Although in this paper we only focus on the uncertain systems, the results can be readily applied to multidimensional systems by replacing the uncertainty variables with frequency parameters. A preliminary version of this work appeared in [27].

While this paper focuses on model reduction problems, its results related to coprime factorization of uncertain systems could be used in many branches of robust control problems, for example, analysis of gap metric [28] for uncertain systems, robust controller design using coprime factorization [29] and Youla parametrization [30], to list a few. Future work will be carried on to apply the results of this paper to other relevant control problems.

Notation The notation is quite standard. $\mathbf{R}^{m \times n}$ and $\mathbf{C}^{m \times n}$ denote the set of real and complex, $m \times n$ matrices, and \mathbf{H}^m denotes the set of Hermitian $m \times m$ matrices. Let l^m and l_2^m be the space of all the sequences and square summable sequences in \mathbf{R}^m respectively. Let $\mathcal{L}(l^m)$ denote the space of all linear operators mapping from l^m to l^m , and $\mathcal{L}(l_2^m)$ denote the space of all linear bounded operators mapping from l_2^m to l_2^m . The gain of an operator Δ in $\mathcal{L}(l_2^m)$ is given by $\|\Delta\| = \sup_{z \in l_2^m, z \neq 0} \frac{\|\Delta z\|}{\|z\|}$, and the adjoint operator of Δ is denoted as Δ^* if Δ is linear, and if $\Delta = \Delta^*$, $\Delta < 0$ means that $x^* \Delta x < 0$ for any $x \neq 0$ in \mathbf{R}^m . We also use M^* to denote the complex

conjugate transpose of a complex matrix M . $FM(\cdot)^*$ and $(\cdot)^*MF$ denote FMF^* and F^*MF respectively for a Hermitian matrix M .

2. Problem Formulation

We consider the uncertainty structure

$$\mathbf{\Delta}^c = \{\text{diag}(\delta_1 I_{h_1}, \dots, \delta_k I_{h_k}) : \delta_i \in \mathcal{L}(l_2), \delta_i \text{ causal}, \|\delta_i\| \leq 1\},$$

and the following uncertain system:

$$\mathcal{G}_\Delta : \begin{cases} \begin{bmatrix} z \\ y \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} \xi \\ u \end{bmatrix}, \\ \xi = \Delta z, \quad \Delta \in \mathbf{\Delta}^c, \end{cases} \quad (1)$$

where $u(t) \in \mathbf{R}^m$ is the *control input*, $z(t) \in \mathbf{R}^h$ is the *uncertainty output*, $y(t) \in \mathbf{R}^l$ is the *measured output* and $\xi(t) \in \mathbf{R}^h$ is the *uncertainty input*; here $h = h_1 + \dots + h_k$. Similar to the typical setting for one-dimensional discrete-time uncertain systems, we define $\delta_1 = z^{-1}$, the time shift operator, and other δ_i 's are regarded as uncertainties.

Let the nominal system be denoted by $G = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$. Then, the uncertain system (1) is defined by an LFT representation as follows. For any bounded linear operator $\Delta \in \mathcal{L}(l_2^h)$ such that $I - A\Delta$ is non-singular, define $\mathcal{F}_u(G, \Delta) := D + C\Delta(I - A\Delta)^{-1}B$. In what follows, robust stability, stabilizability and detectability of the uncertain system (1) are defined.

Definition 1 (Robust Stability [12]). *The uncertain system (1) is said to be robustly stable, or equivalently, $(A, \mathbf{\Delta}^c)$ is said to be robustly stable, if $(I - A\Delta)^{-1}$ exists in $\mathcal{L}(l_2^h)$ and is causal, for all $\Delta \in \mathbf{\Delta}^c$.*

Definition 2. *The uncertain system (1) is said to be robustly stabilizable if there exists a matrix F , such that $(A + BF, \mathbf{\Delta}^c)$ is robustly stable. Similarly, the system (1) is said to be robustly detectable if the dual of the system (1) is robustly stabilizable.*

The following lemma from [12] states a necessary and sufficient condition for robust stability. This lemma is given in terms of the positive commutant set corresponding to $\mathbf{\Delta}^c$ defined as

$$\mathbf{P}_\Theta = \{\text{diag}(\Theta_1, \dots, \Theta_k) : \Theta_i \in \mathbf{H}^{h_i}, \Theta_i > 0\}. \quad (2)$$

Lemma 3. (see [12, Proposition 3 and Remark 4]) *The system (1) is robustly stable if and only if there exists $P \in \mathbf{P}_{\Theta}$, such that*

$$APA^* - P < 0. \quad (3)$$

3. Balanced Truncation

In this section we briefly review the balanced truncation model reduction technique for the uncertain system (1) presented in [8, 9]. It is assumed in this section that the uncertain system (1) is robustly stable. Similar to the LTI balanced truncation approach [2, 3, 4], this robust stability assumption is essential for the balanced truncation of the uncertain system (1), and guarantees the existence of the solutions $S, P \in \mathbf{P}_{\Theta}$ to following Lyapunov inequalities,

$$ASA^* - S + BB^* < 0, \quad (4)$$

$$A^*PA - P + C^*C < 0. \quad (5)$$

Theorem 4. [12, Remark 4] *The following statements are equivalent:*

- (i) *The uncertain system (1) is robustly stable.*
- (ii) *The LMI (4) admits a solution $S \in \mathbf{P}_{\Theta}$.*
- (iii) *The LMI (5) admits a solution $P \in \mathbf{P}_{\Theta}$.*

Definition 5. *An uncertain system of the form (1) is said to be balanced if it has solutions to (4) and (5) which are identical diagonal matrices.*

We summarize the proposed model reduction algorithm as follows.

Procedure 6 (Balanced Truncation).

1. *Solve the LMIs (4) and (5) to obtain $S = \text{diag}(S_1, \dots, S_k) \in \mathbf{P}_{\Theta}, P = \text{diag}(P_1, \dots, P_k) \in \mathbf{P}_{\Theta}$.*
2. *Balance S_i, P_i by a transformation matrix T_i [4] such that*

$$\begin{aligned} T_i S_i T_i^* &= (T_i^{-1})^* P_i T_i^{-1} = \Sigma_i = \text{diag}(\Sigma_{i,1}, \Sigma_{i,2}) \\ &= \text{diag}(\gamma_1 I_{h_{i,1}}, \dots, \gamma_d I_{h_{i,d}}, \gamma_{d+1} I_{h_{i,d+1}}, \dots, \gamma_q I_{h_{i,q}}). \end{aligned} \quad (6)$$

Here $\gamma_1 > \dots > \gamma_d > \gamma_{d+1} > \dots > \gamma_q > 0$ are eigenvalues of $(PS)^{1/2}$ with multiplicities $\nu_j, j = 1, \dots, q$ respectively; $h_{i,j} \geq 0$ satisfies $\nu_j = \sum_{i=1}^k h_{i,j}, j = 1, \dots, q$ and $h_i = \sum_{j=1}^q h_{i,j}, i = 1, \dots, k; \Sigma_{i,1} = \text{diag}(\gamma_1 I_{h_{i,1}}, \dots, \gamma_d I_{h_{i,d}}), \Sigma_{i,2} = \text{diag}(\gamma_{d+1} I_{h_{i,d+1}}, \dots, \gamma_q I_{h_{i,q}})$.

3. Write the transformed nominal system of (1) as $\bar{G} = \begin{bmatrix} \bar{A} & \bar{B} \\ \bar{C} & D \end{bmatrix}$, where $\bar{A} = TAT^{-1}$, $\bar{B} = TB$, $\bar{C} = CT^{-1}$, $T = \text{diag}(T_1, \dots, T_k)$. The sub-matrices of Δ and \bar{G} corresponding to the matrix $\Sigma_{i,2}$, $i = 1, \dots, k$ are truncated to obtain the reduced dimension uncertain system as $\mathcal{G}_{r\Delta} = \mathcal{F}_u(G_r, \Delta_r)$, where $G_r = \begin{bmatrix} \bar{A}_r & \bar{B}_r \\ \bar{C}_r & D \end{bmatrix}$, $\Delta_r = \text{diag}(\delta_1 I_{\tilde{h}_1}, \dots, \delta_k I_{\tilde{h}_k})$; here $\tilde{h}_i = \sum_{j=1}^d h_{i,j}$, $i = 1, \dots, k$.

Theorem 7. Consider the uncertain system (1) and suppose that the reduced dimension uncertain system $\mathcal{G}_{r\Delta}$ is obtained as described in Procedure 6. Then $\mathcal{G}_{r\Delta}$ is also balanced and robustly stable. Furthermore,

$$\sup_{\Delta \in \Delta^c} \|\mathcal{G}_\Delta - \mathcal{G}_{r\Delta}\| \leq 2(\gamma_{d+1} + \dots + \gamma_q). \quad (7)$$

4. Contractive Coprime Factor Model Reduction for Uncertain Systems

As introduced in the last section, the balanced truncation technique requires the underlying uncertain systems to be robustly stable. For those uncertain systems which may be robustly unstable, one of the common approaches is coprime factorization approach. Coprime factorization of uncertain systems is explored in [12] for discrete-time systems, [13] for continuous-time system and [31] for parameter-dependent systems, and a model reduction algorithm based on coprime factorization is given in [12]. However, no indication is given in [12, 31] on the contractiveness of the obtained coprime factors. The balanced LQG truncation for uncertain systems is presented in [10]. It is shown in [32, 33] that the balanced LQG approach and coprime factor model reduction approach lead to identical reduced models in the continuous-time LTI cases. Inspired by these facts, in this section we follow the ideas in [10] to construct a contractive coprime factorization for uncertain systems of the form (1) and derive the corresponding model reduction algorithm.

4.1. Coprime Factorization of Uncertain Systems

Suppose that the uncertain system (1) is robustly stabilizable and robustly detectable, as stated in Def. 2. Consider the following LQG control and filter Riccati inequalities for the uncertain system (1),

$$A^*WA - W + C^*C - (A^*WB + C^*D)(I + D^*D + B^*WB)^{-1}(\cdot)^* < 0, \quad (8)$$

$$AVA^* - V + BB^* - (AVC^* + BD^*)(I + DD^* + CVC^*)^{-1}(\cdot)^* < 0, \quad (9)$$

in the variables $W \in \mathbf{P}_\Theta, V \in \mathbf{P}_\Theta$.

Note that the above Riccati inequalities have the same form as those LQG control and filter Riccati equations in the discrete-time LTI cases [34, 35, 36]; see also [7, 37] for continuous-time cases. In these references, it is shown that the solutions to the LQG control and filter Riccati equations can be used for coprime factorization of the underlying LTI systems. In what follows, we will show that, similar to the LTI cases, the solutions of (8) and (9) can also be used to construct the coprime factors and contractive coprime factors of our uncertain systems (1).

Definition 8. *Given a pair of uncertain systems $\mathcal{M}_\Delta = \mathcal{F}_u(M, \Delta), \mathcal{N}_\Delta = \mathcal{F}_u(N, \Delta)$, $\Delta \in \mathbf{\Delta}^c$, where M and N are constant matrices, $(\mathcal{M}_\Delta, \mathcal{N}_\Delta)$ is said to be a right coprime factorization (RCF) of \mathcal{G}_Δ (1) if the following conditions hold.*

1. \mathcal{M}_Δ and \mathcal{N}_Δ are robustly stable.
2. For any fixed $\Delta \in \mathbf{\Delta}^c$, \mathcal{M}_Δ is invertible in $\mathcal{L}(l^m)$ and \mathcal{M}_Δ^{-1} is causal.
3. For any fixed $\Delta \in \mathbf{\Delta}^c$, $(\mathcal{M}_\Delta, \mathcal{N}_\Delta)$ is right coprime, and $\mathcal{G}_\Delta = \mathcal{N}_\Delta \mathcal{M}_\Delta^{-1}$.

Furthermore, if $\mathcal{M}_\Delta^* \mathcal{M}_\Delta + \mathcal{N}_\Delta^* \mathcal{N}_\Delta \leq I$ for all $\Delta \in \mathbf{\Delta}^c$, we say $(\mathcal{M}_\Delta, \mathcal{N}_\Delta)$ is a contractive RCF of \mathcal{G}_Δ (1).

Theorem 9. *An uncertain system \mathcal{G}_Δ (1) is robustly stabilizable if and only if there exist matrices $\bar{P} \in \mathbf{P}_\Theta$ and $X \in \mathbf{R}^{m \times h}$ solving the following LMI:*

$$\begin{bmatrix} -\bar{P} & \bar{P}A^* + X^*B^* & X^* & \bar{P}C^* + X^*D^* \\ \star & -\bar{P} & \mathbf{0}_{h \times m} & \mathbf{0}_{h \times l} \\ \star & \star & -I_m & \mathbf{0}_{m \times l} \\ \star & \star & \star & -I_l \end{bmatrix} < 0. \quad (10)$$

Furthermore, if (\bar{P}, X) is a feasible solution to (10), then \bar{P}^{-1} verifies (8).

Proof. (Only if part) Assume that the uncertain system \mathcal{G}_Δ in (1) is robustly stabilizable. From Definition 2 and Lemma 3, there exist matrices F and $P_1 \in \mathbf{P}_\Theta$, such that

$$(A + BF)^* P_1 (A + BF) - P_1 < 0.$$

Then we can apply Theorem 4 to show that there exists $P \in \mathbf{P}_\Theta$ such that

$$(A + BF)^* P (A + BF) - P + \begin{bmatrix} C + DF \\ F \end{bmatrix}^* \begin{bmatrix} C + DF \\ F \end{bmatrix} < 0. \quad (11)$$

Define $\bar{P} = P^{-1}$, $X = F\bar{P}$. Left and right multiply both sides of (11) with \bar{P} , and we obtain

$$(\bar{A}\bar{P} + BX)^* \bar{P}^{-1} (\bar{A}\bar{P} + BX) - \bar{P} + \begin{bmatrix} C\bar{P} + DX \\ X \end{bmatrix}^* \begin{bmatrix} C\bar{P} + DX \\ X \end{bmatrix} < 0.$$

It is easy to derive (10) by Schur complement from the above inequality.

(If part) Suppose that (\bar{P}, X) is a feasible solution to (10). Defining $P = \bar{P}^{-1}$, $F = XP$, it is easy to show that (10) is equivalent to (11). Therefore \mathcal{G}_Δ is robustly stabilizable.

Now we prove that \bar{P}^{-1} verifies (8). By Schur complement, (10) is equivalent to

$$-\bar{P} + X^*X + (\bar{P}C^* + X^*D^*)(\cdot)^* + (\bar{P}A^* + X^*B^*)\bar{P}^{-1}(\cdot)^* < 0,$$

which is

$$\begin{aligned} & -\bar{P} + \bar{P}CC^*\bar{P} + \bar{P}A^*\bar{P}^{-1}A\bar{P} - (\bar{P}C^*D + \bar{P}A^*\bar{P}^{-1}B)R^{-1}(\cdot)^* \\ & + [X^* + (\bar{P}C^*D + \bar{P}A^*\bar{P}^{-1}B)R^{-1}]R(\cdot)^* < 0, \end{aligned} \quad (12)$$

where $R = I + D^*D + B^*\bar{P}^{-1}B$.

Therefore, we have

$$\bar{P}A^*\bar{P}^{-1}A\bar{P} - \bar{P} + \bar{P}CC^*\bar{P} - (\bar{P}C^*D + \bar{P}A^*\bar{P}^{-1}B)R^{-1}(\cdot)^* < 0.$$

It is clear that \bar{P}^{-1} verifies (8). \square

Remark 10. The LMI (10) arises from the fact [38, 31] that the solution of the LQG control inequality (8) is related to a special state feedback \mathcal{H}_2 problem, that is, finding a static state feedback gain F , such that $\|\mathcal{F}_l(\mathcal{G}_{SF\Delta}, F)\|_{\mathcal{H}_2} < \gamma$ with a

given $\gamma > 0$, where $\mathcal{G}_{SF\Delta} = \mathcal{F}_u(\mathcal{G}_{SF}, \Delta)$, $\mathcal{G}_{SF} = \begin{bmatrix} A & I & B \\ 0 & 0 & I \\ C & 0 & D \end{bmatrix}$; here $\mathcal{F}_l(\cdot, \cdot)$ denotes

the lower LFT representation. The LMI (10) is actually obtained by substituting A, C in (5) with $A + BF$, $\begin{bmatrix} C + DF \\ F \end{bmatrix}$ respectively, letting $\bar{P} = P^{-1}$, $X = F\bar{P}$ and then applying the Schur complement.

Theorem 11. Given an uncertain system \mathcal{G}_Δ (1) which is robustly stabilizable and robustly detectable, suppose matrices $\bar{P} \in \mathbf{P}_\Theta$ and $X \in \mathbf{R}^{m \times h}$ satisfy the LMI (10). Let

$$F = X\bar{P}^{-1}, \quad (13)$$

and consider the following system

$$\mathcal{G}_{F\Delta} = \begin{bmatrix} \mathcal{N}_\Delta \\ \mathcal{M}_\Delta \end{bmatrix} = \mathcal{F}_u(G_F, \Delta), \quad (14)$$

$$G_F = \begin{bmatrix} A + BF & B \\ C + DF & D \\ F & I_m \end{bmatrix}. \quad (15)$$

Then $(\mathcal{M}_\Delta, \mathcal{N}_\Delta)$ is an RCF of the uncertain system \mathcal{G}_Δ .

Proof. From the proof of Theorem 9, it is clear that (10) is equivalent to (11). Thus F is robustly stabilizing. Then invoke [12, Theorem 9] to complete the proof. \square

Remark 12. Compared with the coprime factorization presented in [12], the method introduced above leads to a more general approach to constructing the coprime factorization. Based on the control/filter Riccati inequalities (8) and (9), the proposed approach solves them by using LMI technique and then constructs coprime factors for underlying uncertain systems in a systematic manner. It is shown in the next section that, by picking up a specific state-feedback gain F , this approach can be extended naturally to the contractive coprime factorization for uncertain systems. It should also be noted that the proposed method removes the full rank assumption of the matrix B which is used in [12] to construct the robustly stabilizing feedback gain F in (15) with the form $F = -(B^*S^{-1}B)^{-1}B^*S^{-1}A$.

4.2. Contractive Coprime Factorization of Uncertain Systems

In the LTI case (without uncertainty), when seeking model reduction methods in the coprime factor description, we are particularly interested in normalized coprime factorizations, since robustness results on closed-loop stability are available. We also note that this property is closely related to the graph metric or gap metric [28, 39] between original models and reduced models. However, it is difficult, if not impossible, to find normalized coprime factorizations for the uncertain systems under consideration. Thus, in this section, contractive coprime factorizations are considered for uncertain systems of the form (1). We remark here that similar contractiveness ideas have been explored in [11, 40, 37, 13].

Theorem 13. Given a robustly stabilizable and detectable uncertain system \mathcal{G}_Δ (1), suppose there exist matrices $\bar{P} \in \mathbf{P}_\Theta$ and $X \in \mathbf{R}^{m \times h}$ solving the LMI (10). Let

$$R = I + DD^* + B^*\bar{P}^{-1}B, \quad (16)$$

$$F^c = -R^{-1}(B^*\bar{P}^{-1}A + D^*C), \quad (17)$$

and consider the following system,

$$\mathcal{G}_{F\Delta}^c = \begin{bmatrix} \mathcal{N}_\Delta^c \\ \mathcal{M}_\Delta^c \end{bmatrix} = \mathcal{F}_u(G_F^c, \Delta), \quad (18)$$

$$G_F^c = \begin{bmatrix} A + BF^c & BR^{-\frac{1}{2}} \\ C + DF^c & DR^{-\frac{1}{2}} \\ F^c & R^{-\frac{1}{2}} \end{bmatrix}. \quad (19)$$

Then $(\mathcal{M}_\Delta^c, \mathcal{N}_\Delta^c)$ is a contractive RCF of the uncertain system \mathcal{G}_Δ .

Proof. Suppose the LMI (10) has a feasible solution (\bar{P}, X) . From the proof of Theorem 9, (10) is equivalent to (12). It is obvious that \bar{P} , $X^c = F^c \bar{P}$ also satisfy (12), therefore satisfy the LMI (10). It follows from Theorem 11 that $(\mathcal{M}_\Delta^c, \mathcal{N}_\Delta^c)$ is an RCF of \mathcal{G}_Δ . Note that here $(\mathcal{M}_\Delta^c, \mathcal{N}_\Delta^c)$ are scaled by $R^{-\frac{1}{2}}$.

To prove that $(\mathcal{M}_\Delta^c, \mathcal{N}_\Delta^c)$ is contractive, that is $\|\mathcal{G}_{F\Delta}^c\| \leq 1$, we show an equivalent claim that $\|\mathcal{G}_{F\Delta}^c\| < \beta$ for any $\beta > 1$. By [41, Theorem 11.1], this claim is equivalent to find $P \in \mathbf{P}_\Theta$ such that

$$\begin{pmatrix} \cdot \\ \cdot \end{pmatrix}^* \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} A + BF^c & BR^{-\frac{1}{2}} \\ (C + DF^c) & (DR^{-\frac{1}{2}}) \\ F^c & R^{-\frac{1}{2}} \end{bmatrix} - \begin{bmatrix} P & 0 \\ 0 & \beta^2 I \end{bmatrix} < 0, \quad (20)$$

which is

$$\begin{bmatrix} \mathcal{N}_{11} & \mathcal{N}_{12} \\ \star & \mathcal{N}_{22} \end{bmatrix} < 0, \quad (21)$$

where

$$\begin{aligned} \mathcal{N}_{11} &= (A + BF^c)^* P (A + BF^c) - P + (F^c)^* F^c \\ &\quad + (C + DF^c)^* (C + DF^c), \\ \mathcal{N}_{12} &= [(A + BF^c)^* P B + (C + DF^c)^* D + (F^c)^*] R^{-\frac{1}{2}}, \\ \mathcal{N}_{22} &= R^{-\frac{1}{2}} (-\beta^2 R + I + DD^* + B^* P B) R^{-\frac{1}{2}}. \end{aligned}$$

It is easy to verify that $P = \bar{P}^{-1}$ satisfies (21). Indeed, substituting $P = \bar{P}^{-1}$ into (21), we have $\mathcal{N}_{12} = 0$ and $\mathcal{N}_{11} < 0$ by the fact that \bar{P} , $X^c = F^c \bar{P}$ also satisfy the LMI (10) and the fact that (10) is equivalent to (11); see proof of Theorem 11. Also, $\mathcal{N}_{22} = -(\beta^2 - 1)I < 0$. Then (21) holds, and this completes the proof. \square

Remark 14. *The construction of contractive coprime factors for the underlying uncertain systems is discussed in [11]. A two-step iteration algorithm is suggested. However, the two LMIs in [11] are not jointly convex in the decision variables, therefore there is no computationally tractable method to ascertain its feasibility. It is shown that the proposed method in Theorem 13 provides a tractable approach to the design of contractive coprime factors based on solving only one LMI. In the absence of uncertainty, the above results also recover those in the discrete-time LTI cases [34, 35, 36].*

4.3. Contractive Coprime Factor Model Reduction

With the contractive RCF (18) in place, the model reduction method in [12] can be applied to the resulting contractive RCF. The only problem left is to compute the controllability and observability Gramians of the contractive RCF (18), as stated in the following theorem.

Theorem 15. *Given that all the conditions in Theorem 13 are satisfied, the following statements hold.*

(i) \bar{P}^{-1} is a generalized observability Gramian for the uncertain system $\mathcal{G}_{F\Delta}^c$ (18).

(ii) The LMI

$$(A + BF^c)S(A + BF^c)^* - S + BR^{-1}B^* < 0 \quad (22)$$

has a feasible solution $S \in \mathbf{P}_{\Theta}$ which is a generalized controllability Gramian for the uncertain system $\mathcal{G}_{F\Delta}^c$ (18).

Proof. (i) From the proof of Theorem 13, $\mathcal{N}_{11} < 0$ in (21). This verifies that $P = \bar{P}^{-1}$ is a generalized observability Gramian for the uncertain system $\mathcal{G}_{F\Delta}^c$ (18).

(ii) Since $\mathcal{G}_{F\Delta}^c$ is robustly stable, invoking Theorem 4, it is straightforward that the LMI (22) is feasible, and S is a generalized controllability Gramian for $\mathcal{G}_{F\Delta}^c$. \square

The above theorem provides a numerical way to compute generalized Gramians $P = \bar{P}^{-1}$ and S for the contractive RCF $(\mathcal{M}_{\Delta}^c, \mathcal{N}_{\Delta}^c)$ of the uncertain system \mathcal{G}_{Δ} . We are ready to summarize the proposed coprime factor model reduction algorithm as follows.

Procedure 16 (Coprime Factor Model Reduction).

1. Solve the LMI (10) to obtain \bar{P} . Define R as in (16), F^c as in (17) and $P = \bar{P}^{-1}$;
2. Solve the LMI (22) to obtain S ;
3. Apply Steps 2-3 in Procedure 6 to the uncertain system \mathcal{G}_Δ (1) to obtain the reduced dimension uncertain system as $\mathcal{G}_{r\Delta} = \mathcal{F}_u(G_r, \Delta_r)$.

Theorem 17. Suppose that all the conditions in Theorem 13 are satisfied, and that the reduced dimension uncertain system $\mathcal{G}_{r\Delta} = \mathcal{F}_u(G_r, \Delta_r)$, where G_r is obtained as described in Procedure 16. Under the assumption that δ_i 's are strictly causal, consider the following system,

$$\mathcal{G}_{rF\Delta}^c = \begin{bmatrix} \mathcal{N}_{r\Delta}^c \\ \mathcal{M}_{r\Delta}^c \end{bmatrix} = \mathcal{F}_u(G_{rF}^c, \Delta), \quad (23)$$

$$G_{rF}^c = \begin{bmatrix} \bar{A}_r + \bar{B}_r F_r^c & \bar{B}_r R^{-\frac{1}{2}} \\ \bar{C}_r + D F_r^c & D R^{-\frac{1}{2}} \\ F_r^c & R^{-\frac{1}{2}} \end{bmatrix}, \quad (24)$$

where $F_r^c = -R^{-1}(\bar{B}^* \Sigma \bar{A} + D^* \bar{C})\mathcal{P}^*$, and \mathcal{P} is the corresponding truncation matrix in Procedure 16 defined as $\mathcal{P} = \text{diag}(\mathcal{P}_1, \dots, \mathcal{P}_k)$, $\mathcal{P}_i = [\mathbf{I}_{\tilde{h}_i} \ \mathbf{0}]$. Then the following statements hold.

(i) $(\mathcal{M}_{r\Delta}^c, \mathcal{N}_{r\Delta}^c)$ is a contractive RCF of $\mathcal{G}_{r\Delta}$.

(ii)

$$\sup_{\Delta \in \Delta^c} \|\mathcal{G}_{F\Delta}^c - \mathcal{G}_{rF\Delta}^c\| \leq 2(\gamma_{d+1} + \dots + \gamma_q). \quad (25)$$

Proof. As δ_i 's are strictly causal, the reduced-order system $(\mathcal{M}_{r\Delta}^c, \mathcal{N}_{r\Delta}^c)$ is well-posed [12]. It follows the proof of [12, Theorem 11,] that $(\mathcal{M}_{r\Delta}^c, \mathcal{N}_{r\Delta}^c)$ is an RCF of $\mathcal{G}_{r\Delta}$ and the error bound (25) holds. It only remains to prove that $(\mathcal{M}_{r\Delta}^c, \mathcal{N}_{r\Delta}^c)$ is contractive.

For simplicity, here we only consider the case of $k = 1$. As described in Procedure 16, let T be the transformation matrix to balance P, S and $\mathcal{P} = [I \ 0]$ be the corresponding truncation matrix. Then

$$\begin{aligned} TST^* &= (T^{-1})^* P T^{-1} = \text{diag}(\Sigma_1, \Sigma_2), \\ \bar{A} &= T A T^{-1} = \begin{bmatrix} \bar{A}_r & \bar{A}_{12} \\ \bar{A}_{21} & \bar{A}_{22} \end{bmatrix}, \quad \bar{B} = T B = \begin{bmatrix} \bar{B}_r \\ \bar{B}_2 \end{bmatrix}, \\ \bar{C} &= C T^{-1} = [\bar{C}_r \quad \bar{C}_2]. \end{aligned} \quad (26)$$

Define the following matrices, partitioned accordingly with the partition in (26),

$$\begin{aligned}\mathcal{A} &= \bar{A} + \bar{B}F^cT^{-1} = \begin{bmatrix} \mathcal{A}_{11} & \mathcal{A}_{12} \\ \mathcal{A}_{21} & \mathcal{A}_{22} \end{bmatrix}, \mathcal{B} = \bar{B}R^{-\frac{1}{2}} = \begin{bmatrix} \mathcal{B}_1 \\ \mathcal{B}_2 \end{bmatrix}, \\ \mathcal{C} &= \begin{bmatrix} \bar{C} + DF^cT^{-1} \\ F^cT^{-1} \end{bmatrix} = [\mathcal{C}_1 \quad \mathcal{C}_2], \mathcal{D} = \begin{bmatrix} DR^{-\frac{1}{2}} \\ R^{-\frac{1}{2}} \end{bmatrix}.\end{aligned}$$

Note that, from the proof of Theorem 13, (20) holds for $P = \bar{P}^{-1}$. Left- and right-multiply both sides of (20) with $\text{diag}((T^{-1})^*, I)$ and $\text{diag}(T^{-1}, I)$, and we have

$$\left(\cdot\right)^* \begin{bmatrix} \Sigma & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} \mathcal{A} & \mathcal{B} \\ \mathcal{C} & \mathcal{D} \end{bmatrix} - \begin{bmatrix} \Sigma & 0 \\ 0 & \beta^2 I \end{bmatrix} < 0. \quad (27)$$

Left- and right-multiply both sides of (27) with $\text{diag}(\mathcal{P}, I)$ and $\text{diag}(\mathcal{P}^*, I)$ to obtain

$$\begin{aligned}\left(\cdot\right)^* \begin{bmatrix} \Sigma_1 & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} \mathcal{A}_{11} & \mathcal{B}_1 \\ \mathcal{C}_1 & \mathcal{D} \end{bmatrix} - \begin{bmatrix} \Sigma_1 & 0 \\ 0 & \beta^2 I \end{bmatrix} \\ < -\left(\cdot\right)^* \Sigma_2 [\mathcal{A}_{21} \quad \mathcal{B}_2] < 0.\end{aligned} \quad (28)$$

It is easy to verify that $\mathcal{A}_{11}, \mathcal{B}_1, \mathcal{C}_1, \mathcal{D}$ are the system matrices of G_{rF}^c in (24). Therefore $(\mathcal{M}_{r\Delta}^c, \mathcal{N}_{r\Delta}^c)$ is contractive; see the proof of Theorem 13. \square

Remark 18. *Note that solutions to the LMIs (10) and (22), if they exist, are not unique. In the absence of uncertainty, minimizing \bar{P}^{-1} subject to (10) and minimizing S subject to (22) would lead to a normalized coprime factor model reduction algorithm. A possible heuristic is to seek approximate normalization in the presence of structured uncertainty, that is, solve the following two semi-definite programs (SDPs):*

$$\begin{aligned}\min \text{trace}(Z) \text{ with } \bar{P} \in \mathbf{P}_{\Theta} \\ \text{subject to (10) and } \begin{bmatrix} Z & I \\ I & \bar{P} \end{bmatrix} > 0,\end{aligned} \quad (29)$$

$$\min \text{trace}(S) \text{ with } S \in \mathbf{P}_{\Theta} \text{ subject to (22)}. \quad (30)$$

Also note that although the two conditions in (10) and (22) are convex (separately), similar to the balanced truncation in the LTI case, the computation of a solution of the LMI constraints which leads to the best reduced model introduces a non-convex problem.

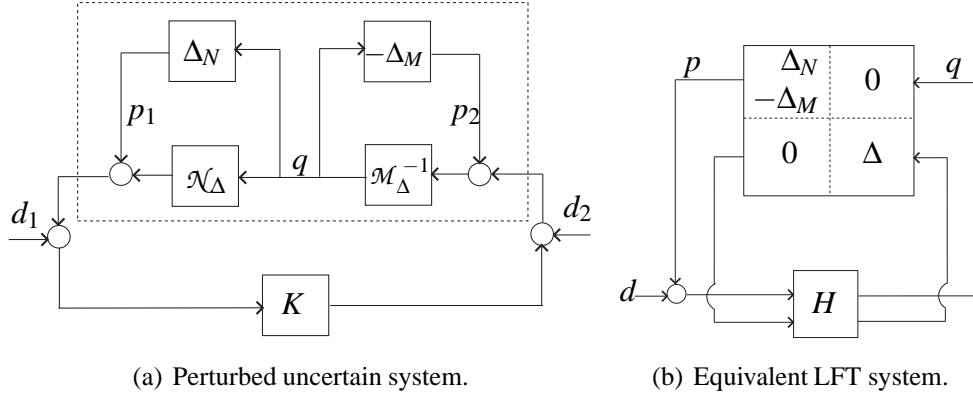


Figure 1: Feedback Interconnection for Robustness Analysis.

5. Robustness Analysis

In the last section, a coprime factor based model reduction algorithm for uncertain systems with structured uncertainty has been derived. It is well known that, in the LTI case, coprime factor model reduction is a model reduction approach in the closed-loop sense. Specifically, for a standard feedback setup consisting of a nominal plant G with normalized coprime factors (M, N) and a stabilizing controller K , in the normalized coprime factor model reduction, if the coprime factor error is bounded by the stability margin $b_{G,K} = \left\| \begin{bmatrix} I \\ G \end{bmatrix} (I - KG)^{-1} [K \ I] \right\|_{\infty}^{-1}$, the controller stabilizing the original plant also stabilizes the reduced model. Motivated by the above fact, this section is devoted to exploring the closed-loop robustness of uncertain systems with structured uncertainty in the coprime factor description.

Consider an uncertain system $\mathcal{G}_{\Delta} = \mathcal{N}_{\Delta} \mathcal{M}_{\Delta}^{-1}$, where $\mathcal{N}_{\Delta} = \mathcal{F}_u(N, \Delta)$ and $\mathcal{M}_{\Delta} = \mathcal{F}_u(M, \Delta)$ are defined in Theorem 11; here $N = \begin{bmatrix} N_{11} & N_{12} \\ N_{21} & N_{22} \end{bmatrix}$ and $M = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix}$ are partitioned accordingly. In order to analysis the the closed-loop robustness, we assume that the uncertain system \mathcal{G}_{Δ} is stabilized by an LTI controller K . Now suppose that the underlying uncertain system is replaced by the reduced uncertain system as $\mathcal{G}_{r\Delta} = (\mathcal{N}_{\Delta} + \Delta_N)(\mathcal{M}_{\Delta} + \Delta_M)^{-1}$, where $\Delta_N = \mathcal{N}_{r\Delta} - \mathcal{N}_{\Delta}$, $\Delta_M = \mathcal{M}_{r\Delta} - \mathcal{M}_{\Delta}$ are coprime factor based model reduction errors. We aim to derive the robustness condition under which $\mathcal{G}_{r\Delta}$ is stabilized by K .

The standard feedback interconnection for the perturbed uncertain system $\mathcal{G}_{r\Delta}$ is plotted in Fig. 1(a). The system inside the dashed box indicates $\mathcal{G}_{r\Delta}$. This closed-loop system can be reformulated to an equivalent standard LFT configura-

tion, as shown in Fig. 1(b), where $p = [p_1^T, p_2^T]^T$, $d = [d_1^T, d_2^T]^T$ and

$$H = \begin{bmatrix} 0 & 0 \\ 0 & N_{11} \end{bmatrix} + \begin{bmatrix} I \\ N_{12} \end{bmatrix} (M_{22} - KN_{22})^{-1} \begin{bmatrix} [K \ I] & -M_{21} + KN_{21} \end{bmatrix}.$$

Invoking the scaled small gain theorem, we are able to define the robust stability margin as

$$\bar{\varepsilon} = \sup \left\{ \varepsilon : \left\| \begin{bmatrix} \varepsilon I & 0 \\ 0 & \Theta \end{bmatrix} H \begin{bmatrix} I & 0 \\ 0 & \Theta^{-1} \end{bmatrix} \right\| < 1, \Theta \in \mathbf{P}_\Theta \right\},$$

and the following result can be easily derived.

Theorem 19. *If an LTI controller K robustly stabilizes $\mathcal{G}_\Delta = \mathcal{N}_\Delta \mathcal{M}_\Delta^{-1}$, where $(\mathcal{M}_\Delta, \mathcal{N}_\Delta)$ is an RCF of \mathcal{G}_Δ , then K robustly stabilizes the reduced uncertain system $\mathcal{G}_{r\Delta} = (\mathcal{N}_\Delta + \Delta_N)(\mathcal{M}_\Delta + \Delta_M)^{-1}$ for all robustly stable $\begin{bmatrix} \Delta_N \\ \Delta_M \end{bmatrix}$ such that $\left\| \begin{bmatrix} \Delta_N \\ \Delta_M \end{bmatrix} \right\| < \bar{\varepsilon}$.*

The above result provides robustness condition on closed-loop stability for uncertain systems with underlying structured uncertainty, which extends the LTI results to uncertain system cases. Under the current coprime factor model reduction framework, this robustness result explicitly specifies the bound on the coprime factor reduction error such that the interconnection of the reduced plant and the original controller is also guaranteed to be robustly stable.

Remark 20. *Note that here we only consider the case where controller K is LTI. In some situations, controller K has the structure similar to \mathcal{G}_Δ , that is, $\mathcal{K}_\Delta = \mathcal{F}_u(G_K, \Delta_K)$ where G_K is a constant matrix; for example, in the multi-dimensional systems [9, 40], or in the LPV gain scheduling problems [14, 15]. A similar result can still be obtained by replacing Δ with an augmented structure $\tilde{\Delta} (\Delta \oplus \Delta_K)$, H with a corresponding constant matrix in Fig. 1(b).*

In the absence of uncertainty, it is well known that the stability margin characterized by normalized coprime factors is closely related to gap metric [28]. We remark as well that the derived robustness property in this section for uncertain systems is only a preliminary conceptual step forward to derive a quantitative robust stability margin in a closed-loop sense for the coprime factor model reduction approach to uncertain systems. The results could potentially contribute to the analysis of gap metric for uncertain systems, however, a great deal of research has yet to be done in order to be able to apply gap metric theory to problems of model reduction to uncertain systems that address closed-loop properties in a systematic way. The future research will focus on the new gap metric and closed-loop model reduction theory for uncertain large-scale systems.

6. Example

Consider the same example in [12] with

$$A = \begin{bmatrix} 0.5034 & 0.1768 & -0.2340 & -0.1406 & 0.5814 \\ 0.0096 & 0.5498 & -0.0362 & -0.6744 & 2.2496 \\ 0.0337 & 0.2546 & 0.0984 & -0.4051 & 1.3599 \\ -0.2709 & 0.1470 & 0.3249 & 0.0484 & 0.6356 \\ -0.0909 & 0.0491 & 0.1075 & -0.1019 & 0.5681 \end{bmatrix},$$

$$B = \begin{bmatrix} 0.3306 & 0.1700 \\ 0.8951 & 0.3442 \\ 0.5487 & 0.2143 \\ 0.8748 & 0.8821 \\ 0.5217 & 0.4479 \end{bmatrix},$$

$$C = \begin{bmatrix} 3.0622 & -0.9986 & -0.7126 & 6.4339 & -10.4291 \\ 3.0396 & -0.9913 & -0.7073 & 5.2369 & -8.4887 \end{bmatrix},$$

$$\Delta = \text{diag}(\delta_1 I_3, \delta_2 I_2).$$

Solving the SDP (29), we obtain

$$P = \bar{P}^{-1}$$

$$= \begin{bmatrix} 96.1453 & -24.7774 & -30.4131 & 0.0000 & 0.0000 \\ -24.7774 & 7.5136 & 6.4620 & 0.0000 & 0.0000 \\ -30.4131 & 6.4620 & 12.5545 & 0.0000 & 0.0000 \\ 0.0000 & 0.0000 & 0.0000 & 98.5330 & -163.4846 \\ 0.0000 & 0.0000 & 0.0000 & -163.4846 & 275.9870 \end{bmatrix},$$

$$F^c = \begin{bmatrix} 1.2027 & -0.1404 & -0.5680 & 0.8741 & -2.2285 \\ -0.0957 & -0.2160 & -0.2979 & -1.0129 & 1.5355 \end{bmatrix}.$$

We can then construct the contractive RCF as in (18), (19) with

$$M_{\bar{F}} = \begin{array}{cc|cc|cc} \hline 0.8847 & 0.0937 & -0.4724 & -0.0238 & 0.1057 & 0.1758 & 0.0555 \\ 1.0532 & 0.3498 & -0.6471 & -0.2406 & 0.7834 & 0.4883 & 0.0886 \\ 0.6731 & 0.1313 & -0.2771 & -0.1425 & 0.4662 & 0.2990 & 0.0560 \\ 0.6968 & -0.1663 & -0.4347 & -0.0804 & 0.0406 & 0.4197 & 0.3764 \\ 0.4937 & -0.1209 & -0.3222 & -0.0996 & 0.0933 & 0.2585 & 0.1829 \\ \hline 3.0622 & -0.9986 & -0.7126 & 6.4339 & -10.4291 & 0.0000 & 0.0000 \\ 3.0396 & -0.9913 & -0.7073 & 5.2369 & -8.4887 & 0.0000 & 0.0000 \\ 1.2027 & -0.1404 & -0.5680 & 0.8741 & -2.2285 & 0.5860 & -0.1053 \\ -0.0957 & -0.2160 & -0.2979 & -1.0129 & 1.5355 & -0.1053 & 0.5311 \\ \hline \end{array}.$$

Solving the SDP (30), we obtain

$$S = \begin{bmatrix} 0.0772 & 0.1973 & 0.1214 & 0.0000 & 0.0000 \\ 0.1973 & 0.5222 & 0.3203 & 0.0000 & 0.0000 \\ 0.1214 & 0.3203 & 0.1968 & 0.0000 & 0.0000 \\ 0.0000 & 0.0000 & 0.0000 & 0.5599 & 0.3169 \\ 0.0000 & 0.0000 & 0.0000 & 0.3169 & 0.1827 \end{bmatrix}.$$

Then the balanced Gramian is

$$\Sigma_1 = \text{diag}(0.8370, 0.3146, 0.0268), \Sigma_2 = \text{diag}(1.1436, 0.8147).$$

Truncating the system matrices corresponding to the last generalized Hankel singular value in Σ_1 , the reduced dimension uncertain system model is defined by

$$\begin{aligned} \bar{A}_r &= \begin{bmatrix} 0.3830 & 0.0865 & -0.3771 & 0.7548 \\ -0.1633 & 0.6255 & -0.0157 & 0.1556 \\ -0.6731 & 0.5150 & 0.3777 & -0.2194 \\ -0.3692 & 0.2832 & 0.0094 & 0.2388 \end{bmatrix}, \\ \bar{B}_r &= \begin{bmatrix} 1.0572 & 0.0349 \\ -0.2642 & -0.5105 \\ -0.6643 & -1.5790 \\ 0.9864 & 0.0412 \end{bmatrix}, \\ \bar{C}_r &= \begin{bmatrix} -0.2745 & -0.0669 & -0.6423 & -0.2425 \\ -0.2725 & -0.0664 & -0.5228 & -0.1973 \end{bmatrix}, \\ \Delta_r &= \text{diag}(\delta_1 I_2, \delta_2 I_2). \end{aligned}$$

and the error bound on the coprime factors is given by

$$\sup_{\Delta \in \Delta^c} \|\mathcal{G}_{F\Delta}^c(s) - \mathcal{G}_{rF\Delta}^c(s)\| \leq 2 \times 0.0268 = 0.0536.$$

7. Conclusions

The paper considers the problem of coprime factor model reduction for a class of discrete-time uncertain systems with structured norm bounded uncertainty. The proposed method is applicable to the uncertain systems which may be robustly unstable, overcoming the robust stability restriction in the balanced truncation approach. A systematic approach is presented to construct a contractive coprime

factor for the underlying uncertain system, based on the use of LMIs. This enables the balanced truncation to be applied to the contractive coprime factor to obtain the reduced uncertain system. Closed-loop robustness is analyzed under additive coprime factor perturbations.

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