

were inserted. The total size of the packaged MMIC down-converter module is approximately $25 \times 27 \times 15 \text{ mm}^3$, which is very compact.

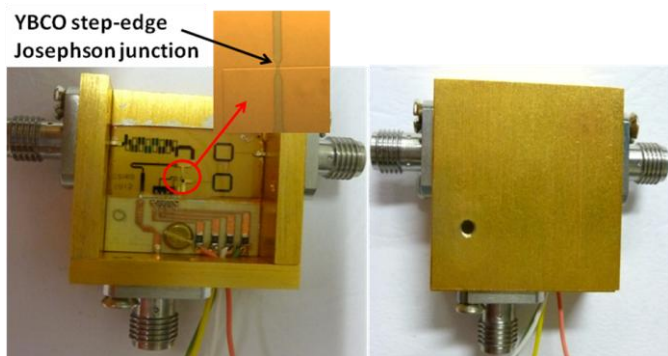


Fig. 1. Photographs of a packaged 10-12 GHz HTS MMIC Josephson frequency down-converter; the inset shows the close view of the step-edge Josephson junction.

The DC characteristics and RF performance of an optimized HTS MMIC down-converter of the same design have been fully characterized at temperatures ranging from 20 to 80 K on a large two-stage pulse-tube cryocooler (PTC) where the compressor is located outside the laboratory. The detailed design considerations and the mixer performance evaluation of the HTS MMIC circuit can be found elsewhere [11]. In this work, we focused on the design and integration of the HTS device with a commercial single-stage mini cooler into a single box to form a portable HTS MMIC receiver sub-module. We have evaluated the performance of the HTS Josephson down-converter module to demonstrate the feasibility of a portable HTS MMIC microwave receiver front-end.

III. MINI CRYOCOOLER AND SYSTEM INTEGRATION

The commercial mini cryocooler (Model CT4187B) was supplied by LIHAN Thermoacoustic Technologies Co. (www.lihantech.com), China. It is a modified split type pulse-tube cryocooler and has a cooling power of 10 W at 80 K. It reaches 70 K in about 30 minutes and the lowest attainable temperature is $\sim 55 \text{ K}$ after installation of all the cables and wires. The orientation of the split compressor and the cold finger was customer designed and implemented by LIHAN as shown in Fig. 2(a). It was designed in such a way that the anticipated magnetic flux generated by the compressor is parallel to the HTS chip surface so the step-edge junction would see minimum vertical flux. An instrument box was designed to accommodate all the parts including the compressor, cold finger, cooler power control circuits, fans and the sample vacuuming chamber as shown in Fig. 2 (b). Stainless steel plates were placed between the main parts to provide further isolation between the cold-head and the compressor and the power control unit. Fig. 2 (c) shows the customer-designed (built by LIHAN) vacuum chamber for housing the sample on the cold finger with vacuuming valve and the panels for cable and DC wire connections.

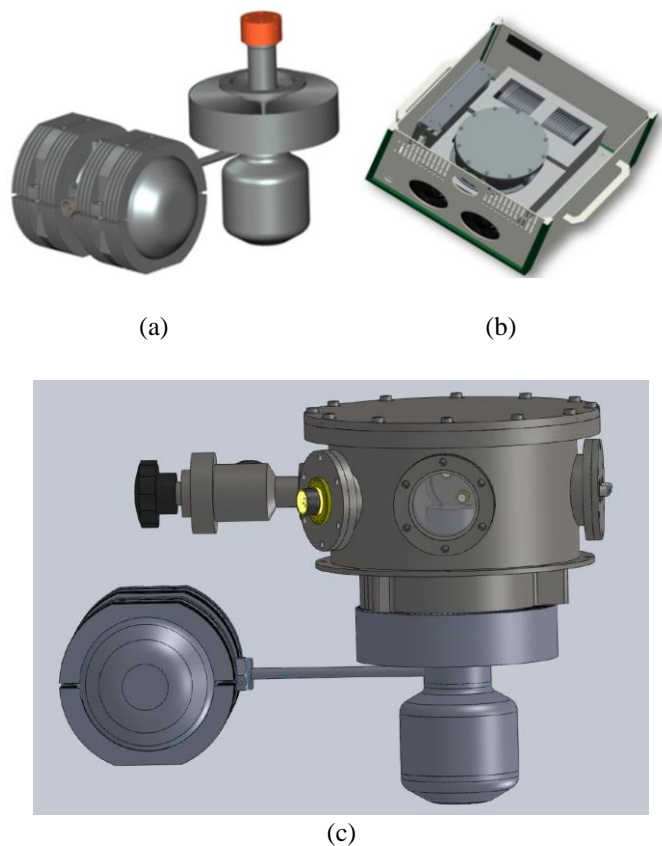


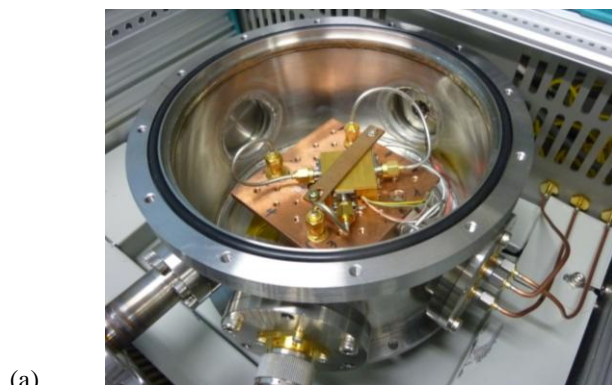
Fig. 2. Schematic diagrams of (a) LIHAN model CT4187B split-type mini cryocooler; (b) a housing box for all parts – compressor, cold finger, sample vacuuming chamber, cooler control circuit and fans; (c) sample vacuum chamber integrated with the coldfinger.

Fig. 3 (a) shows the photographs of the mounted HTS MMIC Josephson down-converter on the cold finger inside the vacuum chamber. A Cu sample plate was used to thermally anchor three coaxial cables to maintain temperature stability (reduce the thermal exchange via the coaxial cables). Semi-rigid stainless steel coaxial cables were used inside the chamber and Cu coaxial cables were used outside the chamber. Fig. 3 (b) shows the enclosed box of the HTS MMIC circuit intergarted with the mini cryocooler, which has a dimension of approximately $350 \text{ mm} \times 350 \text{ mm} \times 250 \text{ mm}$. This is a portable all-HTS microwave integrated receiver sub-system.

IV. EXPERIMENTAL RESULTS OF THE PORTABLE HTS MMIC DOWN-CONVERTER

The performance of one HTS MMIC down-converter integrated with the mini cryocooler was evaluated and the results at 55 K are presented here. The step-edge junction in this down-converter has an R_n value of $\sim 25 \Omega$ and unsuppressed $I_c = 15 \mu\text{A}$ at 55 K (note that the I_c , R_n values are different from the mixer reported in [11]). In this paper, we will not discuss in details the DC characteristics of the step-edge junction and their influence on the mixer performance such as the suppression of LO power P_{LO} on the junction I_c (i.e. $\partial I_c / \partial P_{LO}^{1/2}$) and the mixer conversion efficiency. More details of such discussion can be found in a recent paper [11].

A few measurement results of the HTS module integrated in the mini-cooler are presented here to demonstrate a working portable HTS receiver front-end. The cable losses have not been deducted from all the power levels shown in the graphs.



(a)



(b)

Fig. 3. The photographs of HTS down-converter module mounted in the vacuum chamber (upper picture) and the enclosed box that contains all parts (lower picture).

Figs. 4 and 5 are measured IF power outputs as the functions of the DC bias current, I_B , and the LO power level. Two maxima of the IF output against the bias current I_B have been observed in all our measurements and explained in [11]. The working range of the LO power is quite broad but optimal point is around -50 dBm (include ~ 5 dB cable loss). The required LO power is very small, which is one of the advantages of the Josephson mixer.

Fig. 6 shows the measured dynamic range and linearity of the IF output power for the MMIC Josephson down-converter. A highly linear relationship of the IF output versus the RF input power is displayed with a dynamic range over 40 dB. The conversion efficiency estimated from P_{IF}/P_{RF} less cable loss is approximately -11 dB, which is close to that (~ -10 dB at 55 K) subsequently measured on the large two-stage PTC.

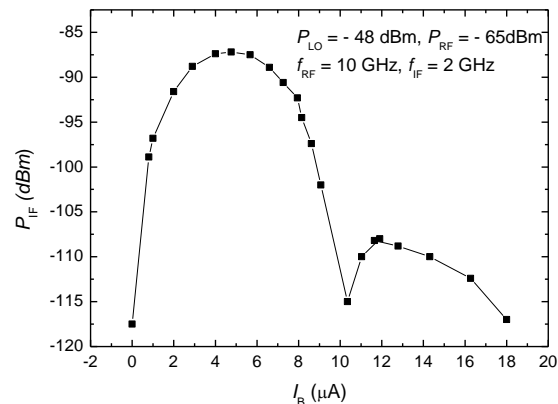


Fig. 4. IF output versus the bias current I_B at fixed RF frequency and LO power.

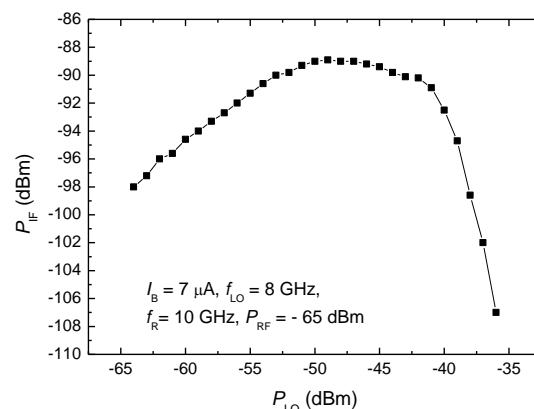


Fig. 5. IF output as function of the LO power level at fixed frequency and RF power level.

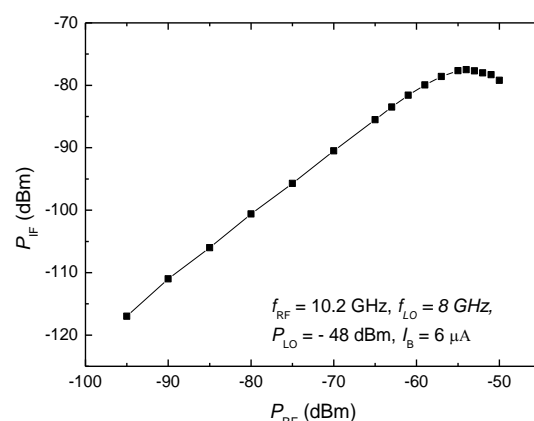


Fig. 6. IF output power versus input RF power for the MMIC down-converter

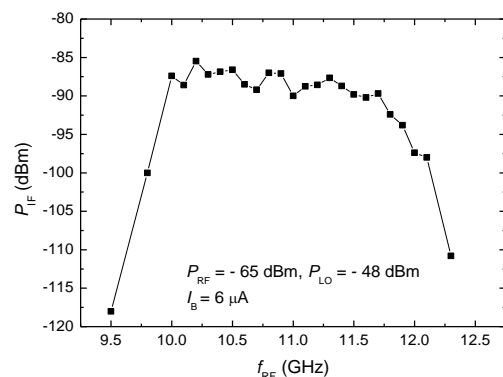


Fig. 7. Frequency response of the 10-12 GHz MMIC frequency down-converter at 55 K cooled by the mini cryocooler.

Fig.7 is the frequency response of the HTS down-converter, of which the response shape is defined by the HTS bandpass filter, i.e. 10-12 GHz passband [3]. The same device was subsequently measured on the large PTC at the same temperature and the results were very close. Given the limited page length, only the frequency response of the device measured on the large PTC is given below for comparison (uncorrected cable loss). Slightly discrepancy in both conversion efficiency and frequency response is expected given different coaxial cables installed which affect the frequency characteristics and the cable loss estimation.

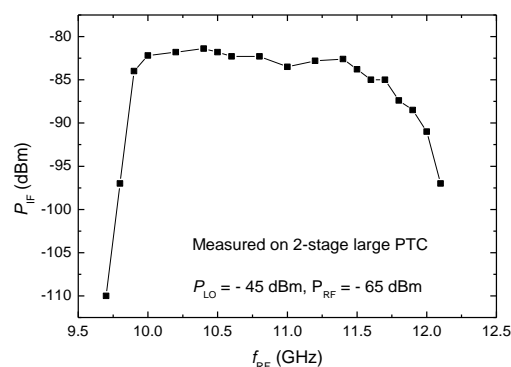


Fig. 8. Frequency response of the same MMIC down-converter but cooled by the large 2-stage PTC.

While only the measurement results of the HTS MMIC down-converter are presented here, we have also measured a number of other HTS junction-based microwave devices including the resistive-SQUID heterodyne oscillator and mixer [5, 9]. The linewidth of the heterodyne oscillator operating on the mini cryocooler was measured and compared to that obtained on the large PTC. No additional linewidth broadening was observed at measured frequencies between 300 MHz and 4 GHz indicating minimum magnetic fields and EMI noise influence on the Josephson junction from the cryocooler. The results presented in this paper were obtained unshielded although a customer-designed mu-metal shield has been made and will be assessed in future work.

V. CONCLUSIONS

In this work, a portable HTS MMIC Josephson frequency down-converter operating on a commercial mini cryocooler is demonstrated. A compact unit was designed and used to house all cryocooler components, sample chamber and the MMIC HTS circuit. The HTS Josephson junction-based microwave circuit was operated successfully in the mini cryocooler unshielded and without observable performance degradation. This work demonstrated the potential of a portable all-HTS receiver front-end for application in wireless communications.

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