

Challenges in Biogas Production from Anaerobic Membrane Bioreactors

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Abstract

Spectacular applications of anaerobic membrane bioreactors (AnMBRs) are emerging due to the membrane enhanced biogas production in the form of renewable bioresources. They produce similar energy derived from the world's depleting natural fossil energy sources while minimizing greenhouse gas (GHG) emissions. During the last decade, many types of AnMBRs have been developed and applied so as to make biogas technology practical and economically viable. Referring to both conventional and advanced configurations, this review presents a comprehensive summary of AnMBRs for biogas production in recent years. The potential of biogas production from AnMBRs cannot be fully exploited, since certain constraints still remain and these cause low methane yield. This paper addresses a detailed assessment on the potential challenges that AnMBRs are encountering, with a major focus on many inhibitory substances and operational dilemmas. The aim is to provide a solid platform for advances in novel AnMBRs applications for optimized biogas production.

32 **Keywords:** anaerobic membrane bioreactor, biogas production, methane, inhibitors

33

34 **1. Background**

35

36 **1.1. Biogas and its sustainability**

37

38 Biogas represents one of the most highly appreciated opportunities to utilize certain
39 categories of biomass to fulfill partially the world's energy needs. Biogas commonly refers to
40 a mixture of gases produced by the biological breakdown of organic matter in the absence of
41 oxygen, of which methane, hydrogen and carbon monoxide can be combusted or oxidized
42 with oxygen. The energy output/ input can reach up to 28.8 MJ/MJ under favorable
43 conditions, contributing to a very efficient use of the valuable biomass [1]. The resultant
44 energy release allows biogas to be used as a biofuel to replace conventional fossil energy
45 sources (coal, oil, natural gas) in power and heat production, and also as a versatile renewable
46 energy source to fuel vehicles with lower sale price compared to diesel and petrol [2, 3].

47 In general, widespread installation and proper functioning of biogas production systems
48 can provide many benefits to users and the wider community. Advantages include energy
49 sustainability, resource preservation and environmental conservation. On the one hand, the
50 long-term utilization of declining fossil fuels is considered unsustainable because of their
51 limited reservoirs and non-renewable nature. Biogas derived from various biological sources
52 can reduce the heavy dependence on these depleting natural resources, and address the energy
53 insecurity concerns due to its renewable, widely applicable, and abundant characteristics [2,
54 4]. On the other hand, the valorization of the generated biogas is that it is energy efficient (a
55 typical value for electrical efficiency is 33% while for thermal efficiency it is 45%) and
56 environmentally friendly due to the low emission of hazardous pollutants, for example
57 volatile organic compounds (VOCs) [5]. In terms of the current CO₂-mitigation policy, biogas,

58 as a nearly GHGs-neutral replacement for fossil fuels, can be produced from widely available
59 renewable feedstocks, and their production barely contributes to the net carbon emission [6].
60 Optimistically, the rapid development of biogas production not only can reduce the world's
61 heavy reliance on fossil fuel and thereby global energy needs, but also reduce the carbon
62 footprint from fossil fuel utilization. This means decelerating the drift to global warming and
63 climate change.

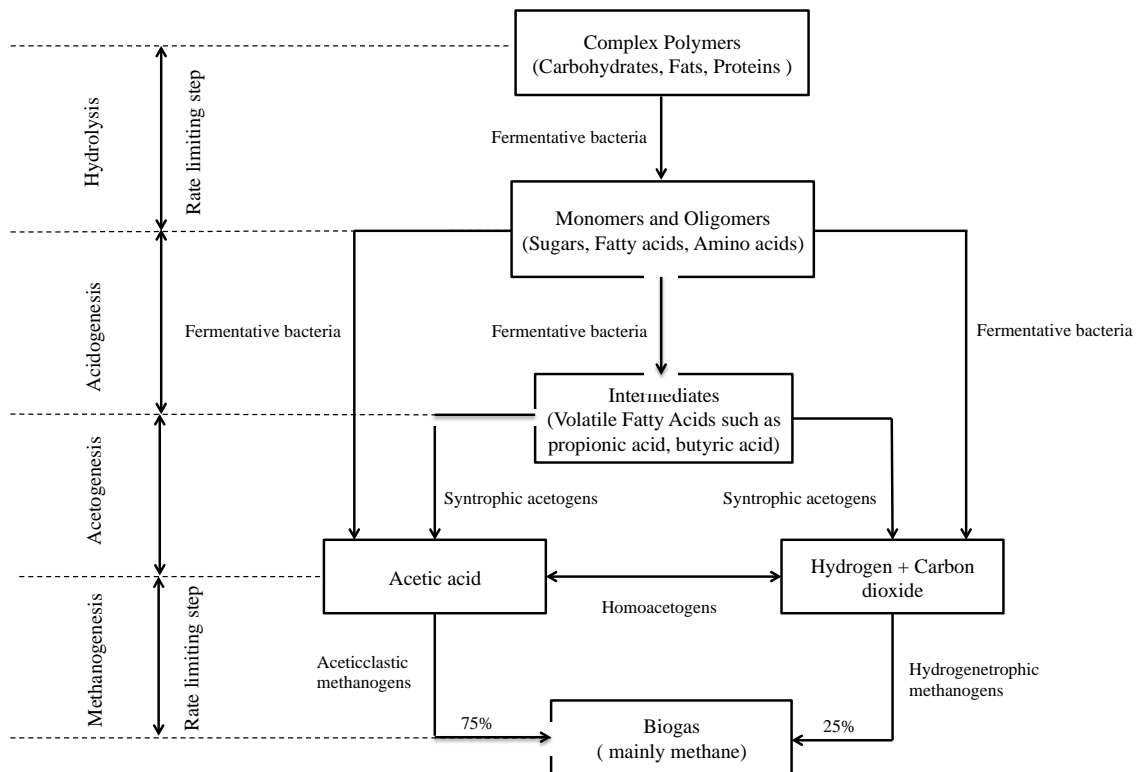
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65 **1.2. Mechanisms of biogas production**

66

67 Biogas can be produced from anaerobic digestion using the locally available residual
68 biomass from various sources (animal waste, domestic sewage, industrial wastewater,
69 agricultural waste, etc.). The anaerobic digestion of complex organic matter to biogas (mainly
70 methane and carbon dioxide) involves four key steps, these being hydrolysis, acidogenesis,
71 acetogenesis and methanogenesis (see **Fig. 1.**). A balanced methane fermentation process
72 requires individual degradation phases to be carried out by distinct consortia of bacteria,
73 namely fermentative bacteria, syntrophic acetogens, homoacetogens, hydrogenotrophic
74 methanogens and aceticlastic methanogens. The symbiotic relationship among these
75 microorganisms contributes to efficient anaerobic digestion and biogas production. [3,7,8].
76 The final phase, conducted by methane-forming bacteria, is the most crucial stage in biogas
77 production where the methanogens convert their primary substrates including acetate,
78 hydrogen and carbon dioxide into methane. There are two pathways for methane formation, in
79 which approximately 75% of methane production derives from decarboxylation of acetate and
80 the remaining 25% originates from CO₂ and H₂ [9]. The methane-forming stage is also the
81 most sensitive and rate limiting step in the whole process since methane-forming bacteria
82 have a much slower growth rate compared to acid-forming bacteria, and are sensitive to
83 inhibitors such as ammonia, temperature, pH and other operational conditions. It is therefore

84 imperative to retain sufficient slow-growing methanogenic bacteria and prevent active
 85 biomass from being washed out from the fermenter, and to reduce inhibitory levels.
 86



87
 88 **Fig. 1.** A schematic diagram showing the comprehensive processes of biogas production from
 89 anaerobic processes [2,7].

90
 91 **1.3. Biogas production by anaerobic membrane bioreactors (AnMBRs)**

92
 93 The slow growing nature of methanogenic organisms and microbial complexity in the
 94 systems have made the operation of biogas fermenters difficult. The success of efficient
 95 biogas production depends on the effective retention of methanogenic bacteria in the reactor
 96 through decoupling of solids retention time (SRT) and hydraulic retention time (HRT) [10].
 97 Research has mostly focused on retaining a high density of functioning anaerobic
 98 microorganisms, in order to achieve efficient biogas production. The most recent
 99 development in biogas production is the incorporation of anaerobic bioprocesses with

100 membrane separation techniques in a membrane bioreactor (MBR), the purpose being to
101 increase biomass concentration extensively in the bioreactor. In an anaerobic membrane
102 bioreactor (AnMBR), high cell concentrations can be sustained under reasonably high
103 hydraulic load and sufficient mixing due to completely decoupling HRT from SRT [11].

104 Moreover, due to the sufficient retention of active microorganisms, AnMBRs generally
105 have high product concentration and productivity and relatively good toxic resistance, and
106 simplify the separation of product and/or biomass by using micro-filtration or ultra-filtration,
107 thus leading to an improved biogas production economy [6]. The reported biogas production
108 was well documented with the methane yield up to 0.36 L CH₄/g COD_{removed} (0.30 L CH₄
109 (STP)/g COD_{removed}, the volume of methane produced at 0 °C Standard Temperature and 1
110 atm Standard Pressure) and the high methane content up to 90% [12]. However, the
111 optimization of biogas production from AnMBRs has not gained much attention due to the as
112 yet under-developed nature of AnMBRs [7]. For extreme conditions, such as high salinity,
113 thermophilic temperature, high organic loading rate (OLR) and presence of toxicity,
114 membrane assisted anaerobic processes can be hampered and biogas productivity can be
115 compromised.

116 Several review papers on biogas production (most are recent) are available in the literature.
117 Ylivero et al. [6] provided a general review of the MBR technology in ethanol and biogas
118 processes and summarized the development of MBRs and the membrane technologies for
119 these biofuels. Wang et al. [11] reviewed the progress in biogas technology in China and
120 briefly introduced AnMBRs as one of the emerging technologies. Mao et al. [2] discussed
121 advances in biogas production from anaerobic digestion in recent years and provided brief
122 information on AnMBRs for biogas production. He et al. [4] summarized the recent
123 performance of AnMBRs for methane and hydrogen production. Minardi et al. [13] reviewed
124 membrane applications for biogas production and purification processes. While these reviews
125 increased researchers' knowledge of AnMBRs for biogas production, they did not

126 simultaneously either: extensively address detailed application concerns and potential
127 challenges encountered; or update the most recent studies. However, with the recent rapid
128 advances in AnMBR technology for bioenergy recovery, a detailed analysis of research
129 progress will be greatly appreciated.

130 The objective of this paper is to provide a comprehensive overview of such advances in
131 various AnMBRs, in view of both traditional and advanced reactor configurations for biogas
132 production. Moreover, with the focus on inhibitors and operational dilemmas, a detailed
133 assessment on the potential challenges that AnMBRs are facing is included in this paper. This
134 review provides perspectives on the outlook for an evolution in advanced AnMBRs
135 applications for more economically feasible and productive biogas yield.

136

137 **2. Types of AnMBRs for biogas production**

138

139 **2.1. Conventional AnMBRs**

140 2.1.1. Completely stirred tank reactor (CSTR) AnMBRs

141 CSTR is by far the most frequently researched anaerobic process in AnMBR systems for
142 biogas production due to the ease of construction and operation. In most cases, CSTRs are in
143 cylindrical or rectangular shapes and employ mechanical turbines for mixing. Side-stream
144 membranes are often used, resulting in high bioreactor liquid turnover rates and a well-mixed
145 hydraulic flow regime. The potential for biological conversion from substrate to methane can
146 be greatly increased due to the prevailing high shear stress and intensive mixing [14, 15].
147 Lab- and pilot-scale studies have been carried out with all three primary AnMBR
148 configurations: external side-stream membrane [16], submerged membrane [17], and
149 submerged membrane with external membrane tank [18]. In general, a CSTR coupled
150 membrane system is able to achieve a promising methane yield up to theoretical value [19].
151 Lin et al. [17] found a methane yield rate of 0.26 L CH₄/g COD_{removed} (0.23 L CH₄ (STP)/g

152 COD_{removed}) and high content of methane up to 85% when operating a pilot-scale submerged
153 anaerobic bioreactor (SAnMBR). The compact configuration of such module also allowed
154 more convenient biogas collection. The research on fermentative H₂ production is also
155 typically conducted in CSTR-AnMBRs. Having the largest amount of energy per mass unit
156 than any other known substance (142 kJ/g), H₂ is an ideal energy carrier free from harmful
157 emissions during utilization as it is combusted to form only water. As the hydrogen
158 production stage occurs briefly prior to the methanogenic process, biohydrogen production
159 can be realized by inhibiting the methanogenesis phase using various intervention means.
160 These include the manipulation of hydrogen partial pressure, pH control, chemical inhibition,
161 and promotion of ferric-reducing conditions (the addition of FeSO₄ solution) [6].

162 Previously, most research has been carried out in an external cross-flow type, but the
163 immersed type has become much more popular recently, due to requiring less energy
164 consumption and less need for fouling mitigation [20]. The carbon source conversion
165 efficiencies in the anaerobic hydrogen producing membrane bioreactor are promising with
166 two cases reaching 100% [21, 22]. FeSO₄ concentration, in particular, was seen as a crucial
167 factor impacting on the dark fermentation pathway for H₂ production from AnMBRs [21].
168 Hydrogen productivity from the AnMBRs ranged from 2.5 [23] to 66 L/L·d [24], and the
169 hydrogen content of biogas could reach as much as 62.6% [21].

170 However, to ensure a well-mixed flow regime and sufficient mass transfer, rigorous
171 mechanical mixing is required. Moreover, the disruption of particles as a result of sludge
172 recirculation through the membrane feed pump can have a negatively impact on the
173 orientation between acetogens and sensitive methanogens, thus limiting the essential
174 hydrogen transport for acquiring a superior specific methanogenic activity (SMA) [14, 25].
175 The impaired syntrophism often leads to a higher concentration of VFA in the system and
176 VFA inhibition is more severe particularly in the thermophilic system. Additionally, CSTR-
177 AnMBR usually operates at a lower biomass concentration (e.g. 5 g/L MLSS) compared to

178 other high rate anaerobic reactors due to fouling control issues, which results in a lower OLR
179 applied to the system, limiting the biomethane potential from high loading wastewater.

180

181 2.1.2. Upflow anaerobic sludge blanket (UASB) AnMBRs

182 The UASB concept was developed by Lettinga et al. in the 1970s for methane production.
183 The secret of such a novel high rate reactor design lies in its ability to: firstly, retain a high
184 concentration of biomass in the form of well settlable methanogenic sludge granules in a thick
185 dense sludge bed at the bottom of longitudinal reactor; and secondly, capture produced biogas
186 through a gas/liquid/solid (GLS) separator at the top. Many researchers have attempted to
187 combine UASB with membrane to optimize the joint benefits such as enhanced methane
188 production and less fouling problems [26, 27]. Xie et al. [28] have investigated the feasibility
189 of a submerged UASB-MBR system for recovering energy from kraft evaporator condensate
190 at 36°C to 38°C for 9 months. The methane production rate of 0.35 ± 0.05 L CH₄/g COD_{removed}
191 (0.31 ± 0.05 L CH₄ (STP)/g COD_{removed}), which were very close to the theoretical yield of
192 methane with 0.397 L CH₄/g COD_{removed} at 37°C (0.350 L CH₄ (STP)/g COD_{removed}), and the
193 methane content in the biogas, reached 90% in this study. Lin et al. [29] also reported a
194 similar methane production rate and excellent fuel quality with 80-90% methane for both
195 mesophilic and thermophilic SAnMBRs from kraft evaporator condensate treatment.

196 To assist with effective biomass retention, a hybrid UASB-MBR, in which fine fibers were
197 placed at the top of the sludge zone as a biofilter, served to treat real domestic wastewater for
198 biogas production at ambient temperature in Beijing, China [30]. Due to the sufficient
199 retention of biomass by the membrane (MLSS maintained as high as 21.5 g/L), this hybrid
200 Granular-AnMBR (G-AnMBR) system achieved maximum biogas production of 0.42 L/L·d,
201 and methane gas content of 66%. UASB reactors for methane fermentation from low strength
202 wastewater at low and moderate temperatures are often encountered by a poor mixing regime,
203 which undermines biogas productivity due to a decrease in soluble COD treatment efficiency.

204 The granulation process for UASB using non-granular seeding is also very lengthy, requiring
205 at the least a 3-month start-up period for stable biogas production. Direct Membrane
206 intervention into UASB eliminated the hydraulic selection pressure for sound granules. This
207 can negatively impact the granular sludge properties and hence the methane yield in the long-
208 term [14].

209

210 2.1.3. Expanded granular sludge bed reactor (EGSB) AnMBRs

211 EGSB reactors are tall reactors characterized by a higher ratio of height to width and
212 effluent recirculation, and they can provide a very high mixing intensity and sufficient
213 substrate-microbes contact induced by the high upflow force. However, to date, the studies on
214 the feasibility of the EGSB combined membrane process are limited. This is probably due to
215 the fact that manipulating sludge bed expansion in EGSB is relatively difficult due to the
216 absence of solid carriers under high hydraulic upflow force. The only study available was Chu
217 et al. [31] who reported biogas production ranging from 0.28 to 0.58 L/L·d, and 63–72%
218 methane at low HRT of 3.5 h from an EGSB reactor coupled with hollow fiber membrane
219 filtration for energy recovery from domestic wastewater at 15°C. However, granules
220 fragmentation and sludge washout may occur due to the applied high upflow velocity ($U_v > 4$
221 m/h), which may affect methane production. In addition, no granulation is expected in EGSB-
222 MBR, which would alter the properties of granular biomass and affect the biogas production
223 in the long-term.

224

225 2.1.4. Anaerobic fluidized-bed membrane bioreactor (AFBR) AnMBRs

226 AFBR is regarded as an effective anaerobic process to be coupled with membrane
227 filtration due to its good mass transfer characteristics and retention of high concentration of
228 active microorganisms at short HRT lasting from a minutes to a few hours. Compared to
229 other gas-sparged AnMBRs, membrane fouling was successfully controlled through the

230 energy efficient scouring effect of fluidized granular activated carbon (GAC) on the
231 membrane surface, resulting in fouling mitigation having significantly reduced energy costs
232 [32]. A two-stage anaerobic fluidized bed system is often required to fully reclaim methane
233 from wastewaters. Kim et al. [33] proposed a staged anaerobic fluidized membrane bioreactor
234 (SAF-MBR) system, which consisted of an AFBR and an anaerobic fluidized-bed membrane
235 bioreactor (AFMBR) for methane rebate from municipal wastewater primary clarifier effluent.
236 The methane production from this system was reported as $4.11 \text{ mol CH}_4/\text{m}^3$ (92.1 L CH_4
237 (STP)/ m^3) with methane composition of 86% at HRT less than 5h. Using only 30% of the
238 gaseous methane energy produced could satisfy total fluidization energy required for the
239 system, meaning such a SAF-MBR is a promising AnMBR for bioenergy production.
240 Similarly, Yoo et al. [34] and Dutta et al. [35] also worked on the SAF-MBRs and concluded
241 that the SAF-MBR system has excellent potential as a low-energy input, high-efficiency, and
242 cost-effective system using methane energy. This is despite the fact dissolved methane
243 representing 63% of the total methane production continued to represent a big issue that needs
244 to be solved if energy production is to increase [34].

245 Methane production is significantly affected by the temperature, and dissolved methane,
246 particularly in the winter period was a severe issue identified by researchers. Gao et al. [36]
247 investigated an integrated anaerobic fluidized-bed membrane bioreactor (IAFMBR) system
248 with simplified reactor operation and much smaller footprint compared with two-stage
249 systems. In this study the methane content in biogas had typical value of $(80 \pm 2\%)$ and nearly
250 50% of the influent COD was converted into methane, of which 25% of produced methane
251 was lost in the liquid phase. As a result of the restrained organic degradation capacity of the
252 AFBR-AnMBRs, VFA accumulation and inhibition was found at shorter HRT, which reduced
253 the specific methane productivity. Moreover, Shin et al. [32] reported that the specific
254 acetoclastic methanogenic activity (SAMA) on the GAC was much lower than the enriched
255 acetoclastic cultures, indicating low levels of such organisms in the GAC VSS. Therefore,

256 future research on biogas production optimization should consider the facilitation of attached
257 growth of syntrophic VFA-degrading acetogens and acetoclastic methanogens on GAC.

258

259 2.1.5. Jet flow anaerobic bioreactor (JFAB) AnMBRs

260 A jet flow anaerobic reactor has certain advantages when coupling with membrane
261 filtration to form an AnMBR for methane fermentation. The liquid circulation inside such a
262 reactor by using an inner tube and a nozzle system offers an adequate homogenization and
263 mass transfer [14]. Applying an UF membrane coupled to the JFAB, Saddoud et al. [37]
264 reported rich methane in biogas (70%) with the average methane yield being 0.27 L CH₄/g
265 COD_{removed} (0.24 L CH₄ (STP)/g COD_{removed}) from domestic wastewater treatment. However,
266 in another study, Saddoud et al. [38] reported the inefficient methanization of such AnMBR
267 with the average methane yield not exceeding even 0.1 L CH₄/g COD_{removed} (0.088 L CH₄
268 (STP)/g COD_{removed}). This was due to the considerable fluctuations in the substrate
269 composition and presence of toxic substances emanating from industrial effluents. Saddoud
270 and Sayadi [39], therefore proposed an innovative two-phase anaerobic digestion (TPAD)
271 system coupling anaerobic fixed bed reactor for optimized acidogenesis and the AnMBR for
272 optimized methanogenesis for biogas production from slaughterhouse wastewater. In this
273 combined process, the volatile fatty acid (VFA) inhibition was successfully overcome, and
274 biogas conversion was significantly improved with an average value of 0.31 L CH₄/g
275 COD_{removed} (0.27 L CH₄ (STP)/g COD_{removed}). **Table 1** summarizes the key features and
276 advantages and challenges of conventional AnMBRs for biogas production.

277 **Table 1** Key features, advantages and challenges of conventional AnMBRs
278

Conventional AnMBRs	Key features	Advantages	Challenges
CSTR-AnMBRs	<ul style="list-style-type: none"> • The first generation of high rate anaerobic reactor and most employed in AnMBR studies • A cylindrical or rectangular tank • Mechanical mixing 	<ul style="list-style-type: none"> • Good substrate-sludge contact with slight mass transfer resistance • High liquid turnover rates and well-mixed flow regime • Enhanced biomethane potential due to prevailing high shear stress and intensive mixing 	<ul style="list-style-type: none"> • Rapid acidification and VFA inhibition due to continuous mixing and high shear stress • Negatively impacted SMA • Lower organic loading leads to lower biomethane potential
UASB-AnMBRs	<ul style="list-style-type: none"> • A cylindrical or rectangular column • Biomass retention in the form of granules • Sufficient mixing provided by liquid upflow force and rising biogas bubbles 	<ul style="list-style-type: none"> • Good wastewater-biomass contact • Superior quality of granular sludge for higher biogas production • Significantly higher organic/hydraulic loading rates compared to flocculent sludge bed reactor • Moderate tolerance to toxic compounds • No mechanical mixing device required • Reduced gas sparging demand 	<ul style="list-style-type: none"> • Long start-up period • Dead space and poor mixing at psychrophilic conditions • Elimination of hydraulic selection pressure causes granules deterioration and disintegration, and unstable biogas production
EGSB-AnMBRs	<ul style="list-style-type: none"> • Tall column reactors with smaller footprint and effluent recirculation • High upflow velocity (>4m/h), very high mixing intensity, and efficient biomass-substrate contact 	<ul style="list-style-type: none"> • Improved mass transfer in a compact design • Resolve issues with UASB such as hydraulic short cuts, preferential flows, poor mixing regime (dead zones), and temperature constraints • Effective in generating biogas from soluble pollutants sources such as domestic 	<ul style="list-style-type: none"> • No granulation is expected, and this may affect the granule sludge properties and hence biogas production • Granules fragmentation and sludge washout due to the high upflow velocity

wastewater, and wastewater containing lipids and toxic/inhibitory compounds

AFBR-
AnMBRs

- Granular activated carbon as the medium for bacterial attachment and growth
- Tall column reactors with a smaller foot print and effluent recirculation
- Two stage submerged membrane configuration is most employed
- A greater surface area per unit of reactor volume

- Higher organic and hydraulic loading and greater resistance to inhibitors for biogas production
- Much lower capital cost due to reduced reactor volume.
- Efficient in biogas production from pharmaceuticals and suspended particles of domestic wastewater

- Two stage systems are often required for effective biogas production
- Dissolved methane remains as a big issue
- VFA accumulation and inhibition at shorter HRT.
- Low specific acetoclastic methanogenic activity (SAMA) on GAC

JFAB-
AnMBRs

- An inner tube and a nozzle system for mixing
- Jet flow module

- A sound homogenization inside the reactor
- Sufficient mixing and compact design

- VFA inhibition causing reduction in biogas production
- Ineffective in accommodating toxics and fluctuations in the feed

280 2.2. Modified AnMBRs

281

282 2.2.1. Anammox AnMBRs

283 Anammox-AnMBR is a novel process combining energy recovery in the form of methane
284 with effective nitrogen management. Compared to the conventional
285 nitrification/denitrification process, anaerobic ammonium oxidization (Anammox) has many
286 advantages such as high nitrogen removal, cost effectiveness and small footprint [40]. The
287 Anammox reaction allows microbial oxidation of ammonium to form nitrogen gas (N₂) under
288 anoxic conditions using nitrite as the electron acceptor [41]. Due to the complete separation of
289 HRT and SRT by membrane, effective domestication and cultivation of the slow growing
290 anammox bacteria was guaranteed in an Anammox-AnMBR. Dai et al. [42] investigated the
291 simultaneous methane production and nitrogen removal from concentrated municipal
292 wastewater by using a membrane-based process combining anaerobic digestion and
293 nitrification-anammox under ambient temperature. The system achieved a stable methane yield
294 of 0.223 L CH₄/g COD_{removed} (0.206 L CH₄ (STP)/g COD_{removed}) while a total nitrogen (TN)
295 removal efficiency of 81% was obtained in the sequential completely (CANON) MBR. This
296 study concluded that the proposed process was a sustainable approach for biogas recovery and
297 nitrogen removal. This research also revealed that further treatment is required to reclaim
298 dissolved methane released into the environment as a powerful GHG, as well as to enhance
299 the methane recovery efficiency.

300 Li et al. [40] investigated the sustainable operation of submerged Anammox AnMBR, and
301 found biogas sparging could greatly reduce small flocs attaching to the membrane to form a
302 cake layer, thereby alleviating membrane fouling. It should be noted that since nitrite and
303 ammonia were converted to nitrogen gas by anaerobic ammonia-oxidizing bacteria (AnAOB),
304 methane composition in the biogas would be lower than that of other types of AnMBRs as a
305 result of the accumulation of produced N₂ in the biogas. The interaction between AnAOB and

306 methane-producing bacteria is still unknown, requiring further studies to maximize the
307 methane yield from the Anammox-AnMBR. Last but not least, the feed for the Anammox-
308 AnMBR contains high levels of ammonia, which can inhibit the production of methane.

309

310 2.2.2. Anaerobic Dynamic Membrane bioreactors (AnDMBRs)

311 Dynamic membrane (DM) technology is a new approach for resolving problems such as
312 high cost of membrane modules, low membrane flux, and rapid membrane fouling
313 encountered in conventional AnMBR processes. In an AnDMBR, the solid-liquid separation
314 is mainly accomplished by the cake layer (e.g., dynamic membrane) formed on low cost
315 supporting materials such as meshes and fabrics with macropores [43]. Such a DM transforms
316 one of the most critical disadvantages of AnMBRs, namely membrane fouling, into a
317 competitive advantage. When the dynamic membrane is seriously fouled, the cake layer can
318 be easily removed, cleaned and then replaced by a new deposited layer, thus significantly
319 reducing the membrane cost [44]. The cleaning process and its frequency are determined by
320 the dynamic membrane material and chemical resistance of the filters [45]. Alibardi et al. [46]
321 developed a bench scale anaerobic dynamic MBR using a large pore-sized mesh at 200 μm .
322 They observed varying biogas production with maximum value of 1L/d and methane content
323 fluctuating from 50% to 79%, which was mainly due to the variability of COD removal and
324 HRT during operation. Low CFV (due to the use of larger pore size) contributed to the
325 sustainable aspect of the AnDMBR by reducing high energy input and led to improved
326 methanogenic activity by minimizing the shear stress on the biomass. Methane oversaturation
327 in the effluent was reported in the study. Due to the higher methanogenic activities of the cake
328 layer formed on the external dynamic membrane module, a great amount of biogas was
329 produced by the membrane unit and subsequently released with the effluent stream.

330 Ersahin et al. [43] applied a monofilament woven as support material for dynamic
331 membrane formation in the AnDMBR for biogas production from synthetic concentrated

332 wastewater. Average methane yields of 0.31 ± 0.02 L CH₄/g COD_{removed} (0.27 ± 0.02 L CH₄
333 (STP)/g COD_{removed}) and 0.34 ± 0.04 L CH₄/g COD_{removed} (0.30 ± 0.04 L CH₄ (STP)/g
334 COD_{removed}) were reported at SRTs of 20 days and 40 days, respectively, which were very
335 close to the maximum theoretical value. Methane was solubilized in the permeate. The study
336 also revealed that strong shear stress as a result of biogas sparging might create a physical
337 interruption on the syntrophic anaerobes associated with methane forming, based on the fact
338 that SMAs of the bulk sludge samples were lower than those of the seed sludge at both SRTs.
339 Xie et al. [47] achieved promising average methane yield at 0.34 L/g COD_{removed} (0.30 L CH₄
340 (STP)/g COD_{removed}) and methane content of 70-90% using Dacron mesh (pore size =40 μm)
341 in the AnDMBR for the treatment of raw leachate, high heavy metal concentrations, and high
342 total ammonium concentration above 3000 mg/L. Based on the archaeal taxonomic
343 identification, aceticlastic methanogens were the dominant functional group that produced
344 methane, while hydrogenotrophic methanogens were eliminated at the end of the experiment
345 when ammonium inhibition was observed.

346

347 2.2.3. Anaerobic Membrane distillation bioreactors (AnMDBRs)

348 Membrane distillation (MD) is a thermally driven separation process in which water vapor
349 transfers across a thermal gradient through a hydrophobic, microporous membrane such as
350 polypropylene (PP), polyvinylidene fluoride (PVDF) or polytetrafluoroethylene (PTFE)
351 membranes to form water [48, 49] The competitive advantages of anaerobic processes can be
352 readily utilized when they are combined with the MD process, as the mesophilic or
353 thermophilic operation for the methane fermentation can allow no or less heating requirement
354 for the subsequent MD treatment [49]. AnMDBRs usually require significantly reduced
355 footprints and provide complete retention of incoming organics and microorganisms for
356 maximum bioconversion from waste to energy in the form of biogas [48-50]. The other
357 highlight of the AnMDBR treatment is the complete removal of total phosphorus for the

358 purpose of controlling eutrophication, which has been recognized as a significant
359 environmental and ecological concern for decades [49].

360 In a typical AnMDBR system, biogas can be recovered from the system for gas sparging
361 for mixing and fouling control purposes, and additional gas can be utilized for heating and
362 energy use [48]. However, post-treatment is required to recover ammonium nitrogen and
363 methane dissolved in the permeate. Smith et al. [51] reported methane loss in the liquid phase
364 from the anaerobic MBR could be as much as 30% and 50% at 35°C and 15°C, respectively,
365 due to the fact that the solubility of methane gas decreases in response to temperature increase.
366 In an AnMDBR, most of the methane is more likely to exist in the gas phase, thus allowing
367 much easier methane extraction and recovery. Moreover, the dissolved methane is transported
368 with the permeate via the slower gas diffusion process in the thermally-driven AnMDBR,
369 whereas other AnMBRs are mostly pressure-driven, the methane gas would rapidly pass into
370 the permeate across the porous membrane via poiseuille flow. Therefore, dissolved methane
371 in the permeate from the anaerobic MDBR will most likely be much less than those from the
372 other AnMBRs [48]. Xie et al. [49] hybridized anaerobic moving bed biofilm reactor
373 (AMBBR) with the MD process for the treatment of domestic wastewater. A small quantity of
374 biogas with methane content at 58%-72% was produced from the AMMBR while no other
375 biogas data was available from the MD process. Further research regarding biogas production
376 from the AnMDBR and the effects of MD process on the methane-producing species would
377 be valuable so that the benefits of AnMDBR in the sense of bioenergy recovery can be fully
378 explored. It would also be possible to identify possible challenges in biogas production from
379 AnMDBRs.

380

381 2.2.4. Anaerobic osmotic membrane bioreactors (AnOMBRs)

382 AnOMBRs constitute a novel integrated system combining AnMBRs with the forward
383 osmosis (FO) process for effective retention of smaller sized contaminants and prolonging of

384 their residence time in the reactor, thus leading to improved biodegradation efficiency and
385 biogas yield in one integrated system [52]. In an AnOMBR the FO membrane is usually used,
386 in which water flows from a low-osmotic- pressure feed solution (FS) to a high-osmotic-
387 pressure draw solution (DS) across a semi-permeable membrane. One of the greatest
388 advantages of the FO process is that no energy input is required to drive the filtration process
389 as compared to traditional energy-intensive pressure-driven separation processes such as
390 MF/UF. Gu et al. [52] evaluated the extent of energy recovery in the form of methane gas
391 from an AnOMBR when treating low-strength wastewater at mesophilic temperature. A
392 promising methane production of 0.25–0.3 L CH₄/g COD_{removed} (0.22–0.27 L CH₄ (STP)/g
393 COD_{removed}) was obtained although a loss of methane in the effluent and a high salinity
394 environment (10 mM–200 mM NaCl equivalent) was discovered in the system. Although the
395 salt, alkalinity and ammonia accumulations in the reactor were reported to have no effects on
396 the bioactivity and biogas production, a long-term examination of salt inhibition, pH stability
397 and ammonia inhibition on the biogas production still requires a further assessment.

398 Chen et al. [53] demonstrated the feasibility of energy recovery from a FO-AnMBR
399 system and reported an average methane yield value of 0.21 L CH₄/g COD_{removed} (0.19 L CH₄
400 (STP)/g COD_{removed}) with methane content of 65-78%. Nevertheless, the methane yield
401 represented only 58% of the maximal theoretical value due to the loss of methane dissolved in
402 the permeate as well as the inhibition of methanogenic activity under accumulated salinity
403 environment. They also pointed out that under high osmotic conditions, anaerobic biomass
404 tended to consume substrate to produce compatible solutes through osmoregulation and
405 extracellular polysaccharides in order to survive. Therefore, a further investigation of
406 salinity's effect on the microbial kinetics and methanogenic activity is required to optimize
407 the biogas production rate. Other challenges associated with the FO-AnMBR were the
408 disposal of inorganic-rich supernatant, and the membrane's low tolerance to high temperature
409 solution and biological attachment to sustain stable biogas production in the long-term.

410

411 2.2.5. Anaerobic membrane sponge bioreactors (AnMSBRs)

412 For an AnSMBR, the medium for bacterial attachment and growth is low-cost
413 polyurethane sponges. These sponges represent a viable mobile carrier in many MBR
414 technologies due to their high porosity and endurance, which can immobilize microorganisms
415 and remove organics and nutrients effectively. Their sound mechanical features in relation to
416 membrane scouring are another advantage to counter-attack membrane fouling due to the
417 continuous rubbing behavior of the moving media. Kim et al. [54] investigated both single
418 and two-stage sponge-submerged AnMBRs using an anaerobic rotary disk MBR (ARMBR)
419 without the membrane cleaning and replacement. They found that disk rotation contributed to
420 enhanced shear force and mass transfer of media, and led to the effective collision between
421 the sponge and membrane surface, thus successfully alleviating fouling and enhancing the
422 membrane permeability in the ARMBR. Apart from the disk rotation, sponges were utilized
423 to maintain microbial growth in the mobile phase as well as effectively control membrane
424 fouling. The reported methane production yield and methane composition in the single system
425 were 12% and 13% higher than those of two-stage systems. Therefore it was suggested that
426 the single ARMBR process was superior to the two-stage process due to higher energy
427 production in the more simplified configuration of the single system. Further research on the
428 effects of sponge size, density and shape, and shear stress of the disk rotation on the
429 bioactivity and biogas production are very much appreciated.

430

431 2.2.6. Gas-lifting AnMBRs (GI-AnMBRs)

432 GI-AnMBR is considered to be an advanced hybrid treatment process that combines
433 anaerobic bioprocess with low-pressure membrane filtration. In both external cross-flow and
434 immersed configurations of conventional AnMBRs, considerable energy input is needed for
435 the gas scrubbing requirements of membrane. A GI-AnMBR, instead, applies the airlift

436 configuration by using headspace biogas for gas lift to maintain a reasonable membrane flux
437 with minimal energy input, thus optimizing the overall energy footprint of AnMBRs. The
438 utilization of biogas-assisted mixing also facilitates the methane stripping from the bulk liquid,
439 avoiding super-saturation, and allowing a minimum amount of methane dissolved in the
440 permeate [55]. Prieto et al. [56] developed a GI-AnMBR and evaluated its ability to recover
441 resource from sewage. This suspended-growth bioreactor coupled to a tubular PVDF UF
442 membrane was able to produce 4.5 L/d (0.28 L/gVSS d) biogas, which can be used for
443 membrane scrubbing and energy recovery. Biogas injection was introduced at the bottom of
444 this system where biogas was combined with the sludge to form a two-phase (liquid–gas)
445 flow through the lumen of vertically-placed tubular membranes. The introduction of biogas
446 bubbles into the membrane feed significantly reduced the membrane fouling because of the
447 increased shear force and turbulence over the membrane surface. The ascending biogas
448 bubbles also enhanced the sludge filterability by decreasing the feed density. Therefore,
449 pumping cost for feed flow and permeate extraction was minimized, meaning there were less
450 energy expenses. However, the biogas recirculation for scouring generated high shear force,
451 which was reported to negatively impact on the SMA and subsequently compromise biogas
452 production.

453

454 2.2.7. Vibrating AnMBRs (V-AnMBRs)

455 Membrane fouling is typically controlled by the recirculation of biogas to create shear and
456 turbulence on the membrane surface [57]. However, the high cost of gas pumping, the
457 difficulty of operating gas sparging in certain cases, and its shear stress on the anaerobic
458 microbes remain as major concerns for the gas-sparged AnMBRs. V-AnMBRs, which utilize
459 effective vibratory shear for enhancing the shear at the membrane surface, have attracted the
460 interest of researchers in recent years. Kola et al. [58] introduced a transverse vibration as an
461 innovative membrane fouling mitigation strategy into a membrane coupled UASB reactor.

462 Based on the observations of significantly increased critical flux and more reversible fouling
463 as compared with conventional fouling control, this study proved transverse hollow fiber
464 membrane vibration provided alternative enhancement of mass transfer. This type of
465 membrane vibration also created vortices in the wake of the vibrating surface, thus facilitating
466 the permeate filtration where gas sparging was often unfavorable. By appropriately
467 incorporating periodical backwash/relaxation with vibrational filtration, such a V-AnMBR
468 would be a promising technology for biogas production. However, the effects of vibratory
469 shear stress on the methane-producing microorganisms require further analysis for the optimal
470 biogas production.

471 Vrieze et al. [57] investigated a novel V-AnMBR using a magnetically induced vibration
472 membrane filtration system as the solo shear enhancement device in anaerobic digestion for
473 fouling mitigation. The biomethanation performance and membrane fouling of the V-AnMBR
474 was compared with a conventional SAnMBR with biogas scouring (known as NV-AnMBR).
475 Similar CH_4/CO_2 ratios (around 1.89) in the biogas were observed from both reactors only
476 when treating diluted molasses wastewater but the V-AnMBR resulted in a noticeable
477 increase in transmembrane pressure and failed to prevent the formation of a cake layer due to
478 the absence of a mixing system. The authors also justified that V-AnMBR is still a promising
479 technology and can be applicable if conventional mixing devices or other measures can be
480 implemented to avoid cake layer build-up. VFA accumulation and a decline in methane
481 production were reported when concentrated molasses were applied, which indicated the
482 inhibitory effects of concentrated molasses on biomethanation.

483

484 2.2.8. Anaerobic bio-entrapped membrane bioreactors (AnBEMRs)

485 In view of fouling being the major concern in AnMBRs, the anaerobic bio-entrapped
486 membrane reactor (AnBEMR) has been developed as an alternative to the conventional
487 AnMBRs, particularly those with high biomass concentrations. The competitive advantage of

488 the entrapped biomass technique was the superior simultaneous removal of carbon and
489 nitrogen within a simplified single throughput bioprocess. Its robust capacity to tackle
490 complex organic compounds, and handle high dissolved organics loading at low suspended
491 biomass concentration was observed in the aerobic bioprocesses [59]. In addition, when
492 combining the entrapped biomass technique with the membrane, membrane fouling can be
493 greatly reduced since less soluble organics and suspended biomass were produced in the bio-
494 entrapped system.

495 Ng et al. [59], as the sole example in the literature, proposed a novel lab-scale anaerobic
496 bio-entrapped membrane reactor (AnBEMR) packed with bio-ball carriers. In their study,
497 both the traditional AnMBR and AnBEMR were tested for biogas production from
498 pharmaceutical wastewater treatment. The authors found that the AnBEMR was able to
499 produce around 15% more methane than the AnMBR (0.142 ± 0.034 L CH₄/g COD_{removed}
500 (0.130 ± 0.034 L CH₄ (STP)/g COD_{removed}) while that of the AnBEMR was 0.159 ± 0.035 mL
501 CH₄/g COD_{removed} (0.145 ± 0.035 L CH₄ (STP)/g COD_{removed})) after a 70-day start-up period.
502 However, both systems encountered the inhibition of methane yield due to organic
503 overloading, high salinity conditions and accumulation of toxic organics when increasing
504 OLRs up to 34.0 ± 2.7 kg COD/m³·d. Furthermore, the AnBEMR showed a longer membrane
505 filtration operating period than the AnMBR due to the release of smaller concentrations of
506 EPS and SMP, and lower suspended biomass concentration. **Table 2** summarizes the key
507 features and advantages and challenges of modified AnMBRs for biogas production.

508

509 **Table 2** Key features, advantages and challenges of modified AnMBRs
 510

Modified AnMBRs	Key features	Advantages	Challenges
Annamox-AnMBRs	<ul style="list-style-type: none"> • Completely autotrophic nitrogen removal • Anammox bacteria • Homogeneous distribution of substrates and biomass • Anammox bacteria in forms of flocs or granules 	<ul style="list-style-type: none"> • Production of Anammox bacterial as flocs or granules with high growth rate • High nitrogen removal • Suitable for biogas production from wastewater containing a high ammonium concentration and low COD content • Overcome long start-up issue with the Anammox process 	<ul style="list-style-type: none"> • Dissolved methane • AnAOB compete with methane-producing bacteria • Methane composition can be altered due to the production of nitrogen gas • Ammonia inhibition
AnDMBRs	<ul style="list-style-type: none"> • Dynamic membrane was formed on the supporting materials such as meshes and fabrics with macropores 	<ul style="list-style-type: none"> • Much lower capital costs for membrane and its cleaning and replacement • Higher membrane flux • Reduced energy consumption and shear stress on the biomass by using low CFV • Cope well with large OLR, high heavy metal and high ammonium concentrations • Promising methane production due to the higher methanogenic activity 	<ul style="list-style-type: none"> • Methane oversaturation in the permeate • Strong shear stress due to biogas sparging for fouling control can affect methanogenic activity • Biogas escape from the external membrane unit and effluent collection vessel • Ammonium inhibition on hydrogenotrophic methanogens
AnMDBRs	<ul style="list-style-type: none"> • Thermally-driven MD process using microporous hydrophobic membranes • The organic retention times much greater than 	<ul style="list-style-type: none"> • Complete retentions of non-volatile organics • Lower operating pressures than conventional pressure-driven membrane processes • Particularly suitable for treating refractory organics which require a long residence time • Complete rejection of total phosphorus 	<ul style="list-style-type: none"> • High energy requirement for heating, and uneconomical for large-scale applications • Post-treatment required to recover methane from the permeate

	<p>the hydraulic retention time</p> <ul style="list-style-type: none"> • Thermophilic bacteria at about 50°C • Stable fluxes can be sustained 	<ul style="list-style-type: none"> • Shorter start-up time • Less dissolved methane 	
AnOMBRs	<ul style="list-style-type: none"> • High retention forward osmosis semi-permeable membrane • Draw solution (such as seawater) required • Separation driven by osmotic pressure difference • High rejection capacity 	<ul style="list-style-type: none"> • Better organic removal and higher biomethane potential • Suitable for methane fermentation from dilute wastewater under mesophilic conditions • Retention of alkalinity and avoiding reactor acidification • Complete total phosphorus removal and partial ammonia and total nitrogen removal • Promising methane production 	<ul style="list-style-type: none"> • Possible effects of alkalinity, salt and ammonia accumulation on the long term stable biogas production • The inorganic-rich supernatant disposal • Membrane's low endurance to biological attachment and high temperature solution for the long time operation
AnSMBRs	<ul style="list-style-type: none"> • Rotary disk-supporting media for membrane fouling control • Sponges for sustaining microbial growth and fouling control 	<ul style="list-style-type: none"> • Enhanced membrane permeability • Low cost sponge media for mobile carrier • Successful membrane fouling control (scouring) without any membrane cleaning 	<ul style="list-style-type: none"> • Limited data available to examine the biogas production from such AnSMBRs • Further studies required to determine the optimal sponge characteristics for the optimized biogas production
GI-AnMBRs	<ul style="list-style-type: none"> • Two-phase flow in the membrane unit • Enhanced sludge retentate recirculation 	<ul style="list-style-type: none"> • Lower cross-flow velocity • Biogas-assisted mixing can help with reducing methane super-saturation 	<ul style="list-style-type: none"> • Helium gas required for the start-up • Continuous scouring can cause varying gas equilibriums, methane oversaturation and changing pH • High shear stress on the methanogens due to the gas recirculation

V- AnMBRs	<ul style="list-style-type: none"> • Membrane vibration system for fouling control instead of traditional gas-sparging means 	<ul style="list-style-type: none"> • No mixing system required • Suitable for fouling control when biogas gas-sparging is not feasible • No biogas sparging shear stress on the biomass 	<ul style="list-style-type: none"> • Inhibited methanogenic activity due to high salinity and toxic sulfide levels • Vibratory shear stress may affect the microbial activity for biogas production and requires further investigation
AnBEMRs	<ul style="list-style-type: none"> • Biomass entrapped in the bio-carriers/bio-balls 	<ul style="list-style-type: none"> • Better organic removal and higher methane yield than conventional AnMBRs • High organic loading • Significantly reduced fouling • Suitable for claiming biomethane from complex wastewater (pharmaceuticals) 	<ul style="list-style-type: none"> • Acidogenesis and methanogenesis inhibition at high salinity conditions and organics overloading • Dissolved methane causes the lower methane yield • Long start-up period

511 **3. Inhibitors of biogas production**

512

513 **3.1. Ammonia**

514

515 During methane fermentation, ammonia is generated by the biodegradation of the
516 nitrogenous compounds mostly in the form of proteins [60]. As ammonia concentration grows
517 above 3500mg/L, methane yield starts to suffer from decreasing below the theoretical value
518 [61]. As ammonia concentrations climb up to the values of 4051–5734 mg NH₃-N L⁻¹, the
519 methanogenic bacteria can lose 56.5% of its activity. Ammonia inhibition includes the
520 increase of maintenance energy requirement, a change in the intracellular pH, and inhibition
521 of a specific enzyme reaction. Free ammonia (FA) (NH₃) is more toxic than ionized ammonia
522 (NH₄⁺) because it is able to penetrate through the cell membrane, resulting in the disruption of
523 cellular homeostasis, potassium deficiency and/or proton imbalance [60]. A higher
524 temperature and pH value can exacerbate the inhibition by releasing more FA [62]. Release
525 of ammonia is a primary concern for a high rate or intensified process such as AnMBR
526 treating high strength waste, where shorter HRT and higher OLR may cause substrate and
527 inhibitory intermediates to accumulate in the reactor [63].

528 Measures to minimize ammonia inhibition are demanded especially for thermophilic
529 methane fermentation from AnMBRs. Kanai et al. [61] proposed the Kubota Submerged
530 Anaerobic Membrane Bioreactor, in which the membranes could retain methanogenic
531 bacteria while ammonia could be filtered out with the permeate, allowing the efficient
532 production of methane from Japanese garbage with high protein levels (TN concentration at
533 10,000 mg/L). The recovered energy from this process was well above the overall energy
534 consumption, enabling such a SAnMBR to be a net energy producer. Meabe et al. [62]
535 suggested that the acclimatization of biomass due to the high SRT in the AnMBR system

536 could affect the degree of ammonia inhibition, and no critical inhibition by ammonia was
537 expected in their mesophilic and thermophilic study.

538 Jensen et al. [63] also reported a successful methanation process from anaerobic digestion
539 of slaughterhouse wastewater containing high proteins using a pilot-scale AnMBR. They
540 found over 95% of COD in the wastewater feed was converted into biogas with 70% methane,
541 and 78–90% of nitrogen was released to the permeate as ammonia, which meant ammonium
542 inhibition was minor in this system. Landfill leachate also features high concentrations of
543 organic contaminants and ammonia, which can be problematic when used for biogas
544 production. Xie et al. [47] have successfully applied an AnDMBR for biomethane production
545 with average methane yield at 0.34 L/g COD_{removed} (0.30L CH₄ (STP)/g COD_{removed}) from high
546 strength landfill leachate digestion. Although free ammonium nitrogen (FAN) concentration
547 was completely inhibitory in this case, detrimental effects were not observed on the
548 performance due to the microorganisms' adaption to high free ammonia concentrations. The
549 authors also suggested an interesting finding that the acetate-consuming methanogens were
550 less inhibited than hydrogen utilizing methanogens, despite high ammonium concentrations in
551 the reactor (over 3000 mg/L NH₃-N at mesophilic conditions). This has proved to be
552 controversial to other researchers [60, 64] indicating that aceticlastic methanogens were more
553 sensitive to ammonium inhibition compared with hydrogenotrophic methanogens.

554

555 **3.2. Sulfide**

556

557 Problems associated with the methane fermentation of sulphate-rich wastes are the toxicity
558 of sulphide to anaerobic microorganisms and the competition for the influent COD from the
559 sulphate reducing bacteria (SRB) (approx. 2g COD/g SO₄-S_{removed}), which suppresses
560 methane productivity [60,65,66]. In particular, methane production from municipal
561 wastewater can be challenging because it can be easily characterized by low COD/SO₄-S

562 ratios. The fierce competition between methane producing bacteria (MPB) and SRB can
563 negatively impact on the quantity and quality of the biogas produced. Although it is evident
564 that the AnMBRs are more resistant to toxics due to the sufficient SRTs for methanogens,
565 many studies have reported increased operational costs during the treatment of high sulphate
566 containing wastewaters by the AnMBR, especially at psychrophilic conditions and lower
567 SRTs. Both Ferrer et al. [65] and Pretel et al. [66] concluded that AnMBR systems
568 represented more energy surplus potential, thus being a net energy producer when treating
569 low-sulphate municipal wastewater in warm/hot climates. The cost savings of up to 28%
570 (Ferrer et al., [65]) in treating low-sulphate can be achieved as compared to the scenario with
571 sulphate-rich municipal wastewater. Liao et al. [12] reported the complete inhibition of
572 biological activity caused by feed toxic shock (high concentration of H₂S in feed) in a
573 thermophilic SAnMBR with mesophilic sludge as the inoculum. Thus, the pretreatment of the
574 feed should be in place to remove toxic sulfur substances so that the biological activity of
575 thermophiles can be maintained. Gimenez et al. [67] also observed a low methane yield at
576 0.069 L/g COD_{removed} (0.061 L CH₄ (STP)/g COD_{removed}) from a pilot-scale mesophilic
577 SAnMBR treating wastewater with a low COD/SO₄-S ratio, and this was mainly attributed to
578 the SRB competition for 90% of influent COD. The methane recovery efficiency from
579 SAnMBRs was greatly influenced by sulphate content in urban wastewater, and higher biogas
580 production would be expected if high COD/SO₄-S or no sulphate were present in the substrate
581 [55]. The effective countermeasures to sulfide toxicity include the dilution of the wastewater,
582 and the implementation of sulfide removal techniques such as physico-chemical measures
583 (stripping), chemical reaction (coagulation, oxidation, precipitation), and biological
584 conversions (micro-aerobic sparging and partial oxidation to sulfur) [60]. Acclimatization of
585 MPB to free H₂S to increase the tolerance of acetoclastic and hydrogenotrophic MPB to
586 sulfide can also be a possible solution. Nevertheless, above-mentioned sulfide toxicity control

587 techniques require further research to obtain valuable data from AnMBRs, in order to validate
588 their applicability and effectiveness in sulfide control.

589 On the other hand, methanogenic activities are not inhibited if the ratio of COD/sulphate in
590 substrate is higher than 10, and low concentrations of sulphate and sulphide are also necessary
591 for effective biogas production [68,69]. Li et al. [70] compared the performance of two
592 AnMBRs with and without the addition of sulphate for the anaerobic co-digestion of coffee
593 grounds, milk and waste activated sludge. They concluded that sulphate addition (at a
594 COD/SO₄²⁻ ratio of 200:1 to 350:1) yielded positive effects on propionate degradation and
595 methane fermentation in a thermophilic AnMBR at higher OLRs. Without the addition of
596 sulphate, the thermophilic AnMBR system at higher OLRs entered a “sub-health state” as a
597 consequence of propionate acid accumulation.

598

599 **3.3. Salinity**

600

601 The presence of high salt concentrations is common in many saline wastes from fish and
602 seafood processing, chemical, petroleum and pharmaceutical industries. High salinity can
603 cause bacterial cells to dehydrate due to the osmotic pressure. With its toxic effects on non-
604 adapted biomass mainly attributed to cations, high salinity is regarded as one of the most
605 important factors influencing methane fermentation processes [60]. Enzyme inhibition, cell
606 activity decline and plasmolysis are the typical manifestations of salt stress on anaerobic
607 microbes [10]. Ng et al. [59] investigated strong salinity conditions' inhibitory effect on
608 methane yield from both conventional AnMBR and advanced AnBEMR when treating the
609 pharmaceutical wastewater. They found microbial flora was negatively impacted (methane
610 yield below 0.16 L /g COD_{removed} (0.14 L CH₄ (STP)/g COD_{removed}) was reported) in a
611 hypersaline scenario, which was due to the disrupted ordinary metabolic functions and
612 degradation kinetics with high salt concentrations. Jeison et al. [71] attributed the presence of

613 very small sized and weak granules in both UASB and AnMBR systems to the high salinity
614 of the wastewater, despite the fact that membrane enhanced retention of active halotolerant
615 bacteria contributed to a superior sludge activity than UASB. They also revealed that the
616 long-term continuous adaption periods resulted in better levels of sodium tolerance, with the
617 observed 50% activity inhibitory concentration (IC₅₀) value for acetotrophic methanogenesis
618 at approximately 25 g Na⁺ /L. In addition, high salinity as a consequence of salt accumulation
619 in the reactors is regarded as a significant concern for the AnOMBR in terms of fouling and
620 excess flux loss rather than inhibition or toxic effects on the biological processes [52,53].

621

622 **3.4. Long chain fatty acids (LCFAs)**

623

624 Long chain fatty acids (LCFAs), are potentially suitable substrates for biogas production.
625 However, the toxicity of LCFAs is known to impair granule formation, sludge flotation and
626 washout, suppress methanogenic activity, mass transfer limitations of substrate, nutrients and
627 biogas in anaerobic granular sludge bed reactors when treating high strength-lipid
628 wastewaters [10, 60, 72, 73]. Dereli et al. [72] assumed that the major drawbacks mentioned
629 above could be addressed by membrane assisted biomass retention in AnMBRs. However,
630 they found the AnMBR process still suffered from reversible LCFA inhibition at 50 days SRT
631 and in turn process instability, which was mainly caused by LCFA adsorption, although the
632 membrane guaranteed excellent biomass retention when treating lipid rich wastewaters. The
633 authors suggested AnMBR operation at shorter SRTs was preferred due to the deliberate
634 washout of adsorbed and free LCFA, thus reducing high concentration LCFA inhibition or
635 transport limitation. Nevertheless, a major fraction of LCFA would not remain degraded,
636 therefore lowering the biomethane potential. Dereli et al. concluded that sustainable methane
637 fermentation from all LCFAs required only very low applied Lipid/Mass ratios. Furthermore
638 they [73] observed LCFA inhibition at high SRTs in their lab-scale AnMBR system when

639 treating wastewater with Fat, Oil, and Grease (FOG) concentration at $11.3 \pm 0.5\text{g/L}$. The
640 inhibitory effect accelerated biomass deflocculation and SMP release.

641 On the other hand the LCFA absorption on sludge flocs modified their hydrophobicity,
642 resulting in less fouling propensity. Jensen et al. [63] reported minor LCFA inhibition from an
643 AnMBR when treating slaughterhouse wastewater with average FOG concentration of 1407
644 mg/L. Ramos et al. [74] reported that the long-term sludge adaption to LCFAs was required
645 for high rate methanogenesis from LCFAs in an UASB coupled membrane system.
646 Acclimated sludge quickly reached maximum methane production from the digestion of
647 substrate with high oil and grease (O&G) content (4.6-36 g O&G/L) at OLR of 17 kg
648 COD/(m³d), without any notable inhibitory effects. The advantages and disadvantages of
649 AnMBRs to mitigate problems induced by inhibitors are summarized in **Table 3**.

650 **Table 3** Advantages and disadvantages of AnMBRs for the mitigation of problems induced by inhibitors.

651

Inhibitors	Inhibitory effects on biogas production	Advantages/Disadvantages of AnMBRs
Ammonia	<ul style="list-style-type: none">• Disrupting intracellular pH• Increasing maintenance energy requirement• Inhibiting a specific enzyme reaction• Methanogenic activity loss	<ul style="list-style-type: none">• Complete retention of biomass• Ammonia were filtered out with the permeate• Acclimatisation and adaption of biomass to free ammonia due to the applied high SRT in AnMBRs
Sulfide	<ul style="list-style-type: none">• The toxicity of hydrogen sulphide to anaerobes• The reduction on quality and quantity of biogas production• H₂S can cause corrosion in boilers, engines, and pipes causing higher maintenance and replacement costs• Downstream oxygen demand required for oxidising H₂S	<ul style="list-style-type: none">• Complete retention of slow-growing methanogens• Higher methane production potential at higher temperature and higher SRT• Sulfate content in the substrate significantly affected the overall operating cost.• Promising for treating low/non sulphate-loaded wastewater• Cost associated with membrane fouling
Salinity	<ul style="list-style-type: none">• Reduced methanogenic activity• Biomass decay• Long adaptation time• Negative impact on granule stability and granule size.	<ul style="list-style-type: none">• Enhanced retention of active halotolerant bacteria• Flux decline due to salt accumulation• Long term adaption leads to high tolerance
LCFAs	<ul style="list-style-type: none">• Impairment of granulation• Sludge flotation, washout, and foam/scum accumulation• LCFA precipitation on sludge particles• Methanogenic inhibition due to mass transfer limitations	<ul style="list-style-type: none">• No biomass washout• Lesser fouling due to increased sludge hydrophobicity• Inhibition due to floc deterioration and SMP release.

652

653 **4. Influential factors on biogas production**

654

655 **4.1. Temperature**

656

657 Temperature is a vital parameter that profoundly influences anaerobic processes. Attempts
658 to produce biogas from AnMBRs have been made under all three different temperature ranges:
659 psychrophilic (0-20°C) [18, 31], mesophilic (20-42°C) [19, 75] and thermophilic (42-75°C)
660 [76]. Thermophilic AnMBRs are known to have a rate-advantage over the others due to a
661 faster reaction time and higher volumetric loading rate, thus demonstrating higher biogas
662 productivity [2]. Both Liao et al. [12] and Lin et al. [29] investigated thermophilic SAnMBRs
663 for biogas production from kraft evaporator condensate treatment at $55\pm 1^\circ\text{C}$, and proved that
664 it was a feasible technology to produce a promising methane yield at average value of 0.35 L
665 $\text{CH}_4/\text{g COD}_{\text{removed}}$ ($0.29 \text{ L CH}_4(\text{STP})/\text{g COD}_{\text{removed}}$) with an excellent fuel quality close to 85–
666 90% methane in the biogas. They attributed higher methane yield to the higher sludge
667 digestion rate making a larger contribution under thermophilic temperatures. Qiao et al. [76]
668 also reported that producing methane from coffee grounds via the thermophilic co-digestion
669 SAnMBR was feasible, and traceable hydrogen content of 100–200 ppm was found in the
670 biogas. However, thermophilic AnMBRs are more sensitive to the presence of toxic
671 compounds such as hydrogen sulfide [12] and inhibitory substances in the feed, and
672 environmental changes. The thermophilic process's extreme temperature is also believed to
673 cause severe ammonia toxicity, digestion inhibition and unstable fermentation processes [3,
674 77].

675 Furthermore, higher membrane flux can be retained using lower energy requirements at
676 higher temperatures due to the reduced viscosity of the biomass suspension [10, 78].
677 Membrane permeability can be further enhanced by decreasing the transmembrane pressure
678 (TMP) due to a lower permeate viscosity at high temperature. However, Jeison and van Lier

679 [79] observed long-term fluxes in the thermophilic SAnMBR were in fact 2–3 times lower
680 than those attained under mesophilic conditions. Therefore, more studies regarding
681 temperature's effects on the sustainable flux are required so that biogas production from
682 AnMBRs is at its most efficient. Membrane fouling is another critical area of interest, which
683 impedes the development of thermophilic AnMBRs for biogas production. Lin et al. [29]
684 compared thermophilic and mesophilic AnMBRs at different OLRs but under similar
685 hydrodynamic conditions. A more compact, less porous cake layer with higher cake resistance
686 was observed in the thermophilic AnMBR, which was mainly due to the higher concentration
687 of fine particles and EPS release at higher temperatures. Furthermore, permeate from the
688 mesophilic AnMBR had much better quality than the thermophilic one. More attention should
689 therefore be paid to the sustainable fouling mitigation measures in order to ensure the
690 economic feasibility of thermophilic AnMBRs for biogas production.

691 Psychrophilic AnMBRs has recently attracted significant attention particularly in terms of
692 generating biogas from low strength wastewaters [18]. It was found that both psychrophilic
693 and mesophilic AnMBRs achieved comparable methane production rates [75, 80], although
694 the former corresponded to significant methane loss in the permeate [75, 81] and a slightly
695 higher fouling rate due to VFA accumulation [18, 75] and protein-dominated EPS release [82].
696 Last but not least, Gao et al. [83] reported temperature shocks led to a temporary increase in
697 biogas generation rate, but shocks with larger magnitude at higher temperatures resulted in
698 performance being significantly disrupted.

699

700 **4.2. pH**

701

702 Most AnMBR systems operate at near neutral pH since methane fermentation takes place
703 within the pH 6.5–8.5 range with the optimal range from 7.0 to 8.0 [3]. Such a pH range was
704 usually maintained through neutralization, which requires the excessive use of chemicals such

705 as sodium carbonate/biocarbonate or calcium carbonate since some streams have extreme pH
706 values, and hydrolysis and acidogenesis phases will decrease pH values. Extreme pH
707 conditions during AnMBRs operation can not only upset biological performance and methane
708 yield but also affect membrane permeability and lifespan [84]. Gao et al. [85] investigated the
709 effects of elevated pH shocks (pH 8.0, 9.1 and 10.0) on biogas production from a SAnMBR,
710 and found that the pH 8.0 shock had a minor impact, yet pH 9.1 and 10.0 shocks did exert
711 significantly negative impacts on the methane yield. This was mainly due to the ammonia
712 toxicity and VFA accumulation at increased pH value. Serious membrane fouling resistance
713 was reported, due to pH shock induced sludge flocs breakage and the accumulation of fine
714 particles in the bulk sludge. In light of the difference in growth rates, and optimum pH for the
715 growth of acidogens (5.5-6.5) and methanogens (6.5-8.2), many researchers have worked on
716 phased AnMBRs, which separate acidogenesis and methanogenesis processes into the two-
717 stage reactor configuration [86]. Optimizing each stage separately in its own reactor reduces
718 VFA accumulation, facilitates process stability, and enhances the system's tolerance to
719 greater loading rate and toxicity. These features will lead to higher methane production. Such
720 a phased AnMBR has been successfully applied to high loading wastewaters treatment for
721 maximum methane yield [39, 86, 87].

722

723 **4.3. Hydraulic retention time (HRT)**

724

725 HRT is a key parameter from an economic perspective as it has a significant impact on the
726 capital cost, meaning shorter HRTs allow smaller biogas-producing AnMBRs [88]. Many
727 researchers have worked on the influence of HRT on biogas production from AnMBRs.
728 Generally, HRTs can range from as low as 2 h [33] to as high as 30 d [89] depending on feed
729 characteristics, system hydraulics, sludge properties, etc. Ho and Sung [90] reported that
730 methane recovery decreased by 13% from municipal wastewater as a result of the increased

731 COD accumulation in the AnMBR when reducing HRT from 12 to 6 hours. Therefore,
732 AnMBR operation with relatively long HRTs may maximize methane recovery. However,
733 Yuzir et al. [91] observed reduced methane productivity from AnMBRs with longer HRT due
734 to less COD available as substrate for methane production. Significantly enhanced methane
735 production was evident when high hydraulic shock load was applied (HRT 1 d) and they
736 attributed this high yield to enhanced levels of hydrogenotrophic methanogenesis rather than
737 acetoclastic activity. Huang et al. [92] also reported that a shorter HRT increased biogas
738 production due to increased organic loading rate in a SAnMBR. However, too short an HRT
739 was not recommended due to higher biomass concentrations and higher SMP that could
740 worsen membrane fouling. Gao et al. [36] observed something different when they
741 investigated the effects of decreasing HRT on biogas production from an integrated anaerobic
742 fluidized-bed membrane bioreactor. They found that methane productivity increased when the
743 HRT decreased from 8h to 6h, which was linked to the increased OLR. Meanwhile the
744 productivity decreased as more VFAs accumulated with a much shorter HRT.

745 HRT was controlled as an independent parameter from upflow velocity in the studies using
746 CSTR-AnMBRs as the main biological component. However, An et al. [93] reported that in
747 the UASB-AnMBRs without the recirculation, the impacts of HRT and upflow velocity could
748 be assessed dependently because they were inversely correlated to each other. They reported
749 that biogas yield almost doubled from 0.062 to 0.12 L/g COD_{removed} (0.057 to 0.11 L CH₄
750 (STP)/g COD_{removed}), in which methane percentages also rose from 59.3 to 65.2% when HRT
751 of a membrane coupled UASB reactor was gradually decreased from 10 h to 5.5 h. They
752 attributed the enhanced gas production to the improved substrate distribution in the sludge
753 bed and enhanced mass transfer between biomass and substrate at a higher upflow velocity.

754 Based on the studies conducted by the researchers, it could be concluded optimized HRT
755 exists for each case depending on many factors such as feed characteristics, system hydraulics,
756 sludge properties, reactor design and configuration, substrate types, etc. Prolonged HRT may

757 cause AnMBRs reactor volume to be used inadequately and shortened HRT may lead to VFA
758 accumulation, reduced methane productivity and severe membrane fouling.

759

760 **4.4. Solid retention time (SRT)**

761

762 Unlike other types of anaerobic reactors, AnMBRs enable SRT to become completely
763 independent from HRT, irrespective of the sludge properties. SRT values ranged from 20 d
764 [72,94] to infinite days [92], although most researchers worked using SRT values higher than
765 160 d. As a thumb of rule, AnMBRs operating at longer SRTs produce greater quantities of
766 biogas because any decrease in the SRT may reduce the extent of reactions needed for stable
767 digestion. For example, Huang et al. [92] in 2011 reported that a longer SRT would enhance
768 the dominance of methanogenesis and lead to more biogas generation. In their study, methane
769 yield rates of 0.670 ± 0.203 L CH₄/d, 0.906 ± 0.357 L CH₄/d, 1.290 ± 0.267 L CH₄/d
770 (0.610 ± 0.203 L CH₄ (STP)/d, 0.825 ± 0.357 L CH₄ (STP)/d, 1.175 ± 0.267 L CH₄ (STP)/d) were
771 reported at SRTs of 30, 60 and infinite days, respectively. Yeo and lee [95] suggested that
772 AnMBR operation under a long SRT could permit low dissolved methane concentration in
773 AnMBR permeate, along with high methane recovery. They attributed 45% more methane
774 production at higher SRT to supplemental methane formation originating from biomass
775 electrons via endogenous decay.

776 It is obvious long SRTs are more favorable in AnMBRs' operation since it results in
777 minimal sludge production and hence significantly reduces disposal cost. However, longer
778 SRTs operation can also impact on methanogenic activity due to a decrease in viable biomass
779 concentration [10]. The effects of long SRTs on membrane fouling, furthermore, require
780 urgent attention. Prolonged SRTs can hinder sludge flocculation and reduce particle size, and
781 increase the release of soluble microbial products (SMP) [92]. On the other hand, high sludge
782 concentration at high SRT can result in a rapid cake formation and compaction, leading to

783 excess flux decline [10]. Additionally, the accumulation of inorganic solids at high SRTs may
784 also increase inorganic fouling, which in many studies was found to be serious [73, 96].

785

786 **4.5. Organic loading rate (OLR)**

787

788 AnMBR processes have the competitive advantage of accommodating fluctuations in the
789 organic loading, and OLRs ranging from 0.23 [37] to 33.7 kg COD/m³·d [76] have been
790 applied in AnMBRs for biogas production. In general, OLR represents the quantity of volatile
791 solids fed into a biogas digester per day under continuous operation [2]. When an increase in
792 OLR occurs, therefore, the biogas yield is supposed to also increase to a certain extent. An et
793 al. [93] reported that biogas yield from an AnMBR rose linearly with an increase in the
794 organic loading. Wijekoon et al. [97] also observed a continuous increase in biogas
795 production rate from 5L/d to 35L/d with increasing loading rate from 5 to 12 kg COD/m³·d in
796 a two-stage thermophilic AnMBR. Bornare et al. [16] reported an increase in the average
797 biogas generation from 159 to 289 L/d but a decrease in the biogas yield from 0.48 to 0.42 L
798 biogas/g COD_{removed} when increasing OLR from 0.62 to 1.32 kg COD/m³·d. They attributed
799 this conflicting outcome to a better food-to-microorganisms (F/M) ratio (0.08kg COD/kg
800 MLVSS/day) at a lower OLR. Dereli et al. [10], however, stated that the effect of OLR should
801 be assessed together with SRT and biomass activity as the system's OLR was not an
802 independent parameter.

803 Applied temperature also exerts a profound influence on the applicable OLRs in AnMBRs.
804 Thermophilic AnMBRs emerge as being more effective in coping with higher volumetric
805 loading than AnMBRs operating in the mesophilic range [98]. It should be also noted that as
806 the organic loading rate increases, the risk of deteriorating biogas production due to VFA
807 accumulation may occur due to the inhibition of microbial activity [97]. For example,
808 Saddoud and Sayadi [39] documented a process failure in their study, i.e. a drastic decrease in

809 the methane yield at OLR of 16.3 kg COD/m³·d due to VFA accumulation and methanogenic
810 inhibition in a one-phase AnMBR. They subsequently suggested a two-stage AnMBR with
811 the anaerobic filter as acidogenic reactor and jet flow AnMBR as methanogenic reactor at
812 high OLR and achieved a significant improvement in biogas conversion in the staged
813 AnMBR.

814 Serious fouling caused by the release of EPS/SMP and the accumulation of large fine
815 particles, became another issue associated with high loading AnMBRs when using AnMBRs
816 for biogas production [99]. In the face of the comprehensive effects of OLR on methane
817 production, Wei et al. [19] proposed the concept of sustainable OLR to optimize energy
818 recovery potential from typical municipal wastewater through mesophilic AnMBRs. They
819 reported sustainable OLR of 6kg COD/m³·d could result in maximum methane yield up to a
820 theoretical value of 0.382 L CH₄/g COD_{removed} (0.318 L CH₄ (STP)/g COD_{removed}). **Table 4**
821 summarizes the operational factors affecting biogas production from AnMBRs and the
822 recommendations for optimized biogas production.

823

824
825

Table 4 The effects of operational factors on biogas production from AnMBRs and possible suggestions for optimized biogas production

Factors	The effects on biogas production process	Possible suggestions for optimized biogas production from AnMBRs
Temperature	<p>Thermophilic:</p> <ul style="list-style-type: none"> • Faster reaction rates→higher-load bearing capacity→higher biogas productivity • Possible acidification→ inhibition of biogas production • Decreased stability and increased toxicity→poor methanogenesis→higher net energy input and larger investments • Difficulty in anaerobic biomass immobilization→poor sludge settling characteristics→ reduced methanogenic activities→poor effluent quality • Less cooling required→improved process economics • Sludge decay with non-adapted mesophilic sludge→serious membrane fouling • Reduced sludge viscosity→A higher flux→process efficiency →Lower shear rates→ lower energy requirement • A lower permeate viscosity→increased membrane permeability by decreasing TMP • More compact cake layer→higher cake layer resistance→server fouling issues→very low long-term flux→process inefficiency <p>Mesophilic:</p> <ul style="list-style-type: none"> • Better process stability, higher biomass richness, better permeate quality but possible low methane yields and poor biodegradability and nutrient imbalance <p>Psychrophilic:</p> <ul style="list-style-type: none"> • Enhanced methane solubility→loss of methane in effluent→lower methane recovery • TSS and soluble COD accumulation and a higher viscosity→increased filtration resistance→increased fouling and operational cost • Enhanced membrane removal and compensation for the decreased SMA and bulk sludge removal • Energy requirement for operating the system is lower • Reduced reaction and hydrolysis rates→reduced methanogenic activity 	<ul style="list-style-type: none"> • Two phase AnMBRs with thermophilic hydrolysis/acidogenesis and mesophilic methanogenesis • Avoidance of drastic temperature changes

Temperature changes:

- Temperature decrease→decreases in the VFA production rate, the ammonia concentration, the substrate utilization rate and the metabolic rate of the microorganisms→increased start-up times→decreasing CH₄ and H₂ yields
- Temperature increase→increase in pH, hydrolysis of organic particulates→increase in methane potential
- Temperature increase→ Free ammonia concentration→ methanogenic inhibition
- Temperature fluctuation→stress on biomass →increase membrane fouling and operational cost

pH

- Extremely low pH value→acidification and VFA accumulation→reduced methane yield
 - Extremely high pH value→increased ammonia toxicity and VFA inhibition→reduced methane yield
 - pH shocks→dispersion of sludge flocs→the accumulation of colloids, solutes or biopolymers in the bulk sludge suspension→deteriorated membrane performance and biogas production potential
- Two phase AnMBR with optimized conditions for both acidogenic and methanogenic reactor to bring biogas yield optimization
 - Minimize pH shock loading by neutralizing the feed with chemicals such as sodium bicarbonate

HRT

- Optimum HRT exists, which ensures the maximum methane productivity
 - HRT lower than the optimal value→VFA accumulation→ reduced methane yield→ server fouling
 - HRT above the optimal value→insufficient utilization of biogas digester component→reduced methane production
- Avoid operation at too high or too low a HRT
 - Operate AnMBRs for maximum biogas production at optimal HRT

SRT

- Long SRT→enhance dominance of methanogenesis→enhanced methane yield
 - Long SRT→reduced dissolved methane→higher methane recovery
 - Long SRT→ reduced sludge disposal and cost
 - Long SRT→reduced sludge particle size and release of SMP→membrane fouling
 - Long SRT→cake formation and consolidation→increased fouling cost
 - Long SRT→accumulation of inorganic solids→inorganic fouling
- Long SRT is generally recommended for AnMBRs operation
 - Additional care is required for fouling mitigation at long SRT
-

OLR

- Increased OLR→higher metabolic activity of methanogens→increase biogas yield and methane content in the biogas to certain extent
 - High OLR→VFA accumulation→irreversible acidification→risk of a deteriorated biogas yield
 - High OLR or organic shock loading→release of tight EPS/SMP and accumulation of fine particles→serious membrane fouling
- Operating AnMBR at sustainable OLR to maximize the methane yield.
 - Thermophilic systems and effluent recirculation can help relieve systems from the overloading issues
-

5. Future perspectives

The critical analysis of recent literature reveals that much progress has been made in the research and development of AnMBRs for biogas production. The green perspectives of AnMBRs including biogas production, high effluent quality, waste minimization, high capacity, footprint efficiency (reducing capital costs), lower energy requirements, and decentralized operation, mean that such a technology can produce bioenergy through a sustainable bioprocess. For example, a substantial commercial value of US\$341640/year could be obtained from a full-scale AnMBR's recovery of biogas [17]. Most research on AnMBRs has focused on investigating traditional configurations such as CSTR, UASB, AFBR, etc. Recent advances in the modification of conventional AnMBRs and the development of novel AnMBR processes have witnessed greater outcomes. Incorporating a dynamic membrane into AnMBRs significantly reduced capital exploitation costs for the membrane and its cleaning and replacement. Thermally-driven membrane distillation minimized the methane loss through the liquid phase and completely rejected total phosphorus when coupled with AnMBRs. The forward osmosis process in the AnOMBR provides nearly complete removal of total phosphorous and records a relatively good rejection rate for total nitrogen and ammonia [52, 53]. The developments of V-AnMBRs, GI-AnMBRs, AnBEMRs and AnSMBRs offer new insights into sustainable fouling mitigation strategies that enhance the economic feasibility of AnMBRs for biogas production. The literature review revealed that most of the research reported on biogas production from AnMBRs was confined to lab scale experiment. The results from lab testing most often could not directly transfer to industrial and commercial practical application. Fundamental information regarding the energy consumption of each specific AnMBR and its capital cost for installation and operation is still lacking. Further research at well controlled pilot or full scale AnMBRs studies is greatly appreciated to obtain valuable data, in order to support the wide

implementation of such green technology at industrial scale.

Depending on the origin, the feedstock for AnMBRs may contain inhibitory compounds such as ammonia, sulfide, salt or LCFAs. Accumulation of these inhibitors in AnMBR may cause process upset or even reactor failure, indicated by the reduction in daily biogas production and methane composition. Therefore, co-digestion with other wastes, acclimatization of microorganisms to toxic compounds, and pretreatment to remove or counteract toxicants can enhance the process stability and optimize biogas production [60]. Despite extensive research on the operational parameters' effects on the biogas productivity from AnMBRs, a universal operational protocol has not yet been developed to optimize biogas production due to the complexity for the consortia of microorganisms, variations in the feed characteristics, and differences in system hydraulics. Although thermophilic AnMBRs have a rate-advantage over mesophilic ones, greater investment is required to deploy thermophilic systems and mitigate the severe membrane fouling.

Prolonged SRT is believed to minimize the toxic impacts and enhance methanogenesis but the resultant fouling issues and subsequent flux decline are problems that remain unsolved. Decreasing the HRT to acquire the optimal OLR is a possibility. However, published information on the maximum sustainable loading rate is still lacking and its relationship to the applied HRT requires further investigation. Numerous researchers have reported the issues associated with dissolved methane at the effluent, despite variations in AnMBR configurations. Due to economic and environmental concerns, methane leakages must be minimized [75]. Developing effective and applicable dissolved methane recovery process is of great interest to optimize bioenergy recovery and minimize direct greenhouse gas emissions to the atmosphere.

6. Conclusions

AnMBR technology, as future green bioprocess has much potential for renewable energy production. Currently AnMBRs are starting to evolve to the next level. Advanced AnMBRs have attracted a lot of interest in producing high fuel quality biogas when they are combined with many novel technologies such as Anammox, dynamic membrane, membrane distillation, etc. The biogas production from AnMBRs is greatly influenced by many factors including temperature, pH, HRT, SRT, and other variables. The opportunity to apply such green technology on a commercial scale first needs prospective research studies to overcome many challenges such as methane recovery, product inhibition, membrane fouling, and membrane cost.

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