

# Catalogue of Analytical Solutions for Consolidation of Unsaturated Soils Subjected to Various Initial Conditions and Time-Dependent Loadings

A thesis in fulfilment of the requirement for the award of the degree

**Doctor of Philosophy** 

from

University of Technology Sydney (UTS)

by

LIEM HUU HO, BEng (1<sup>st</sup> class Hons, UTS)

School of Civil and Environmental Engineering, Faculty of Engineering and Information Technology 2016

#### **CERTIFICATE OF ORIGINAL AUTHORSHIP**

I certify that the work in this thesis has not previously been submitted for a degree nor has it been submitted as part of requirements for a degree except as fully acknowledge within the text.

I also certify that the thesis has been written by me. Any help that I have received in my research work and the preparation of the thesis itself has been acknowledged. In addition, I certify that all information sources and literature used are indicated in the thesis.

Liem Ho February 2016

#### ABSTRACT

Soil consolidation has been a primary geotechnical interest for decades. Such phenomenon involves the gradual dissipation of excess pore pressures from the soil deposit subjected to an external applied load, resulting in a considerable reduction of soil volume. Majority of industrial and residential areas have been vigorously developed in arid and semi-arid climatic regions, where the underground water table is relatively deep. In these regions, construction activities can significantly influence the upper unsaturated zone. In particular, the earthworks, such as excavation and compaction, and changes in the climate and surface vegetation may result in further creation of unsaturated soils, whose properties are much more complicated than those of saturated soils. Past decades have witnessed the significant growth of engineering interests in unsaturated soils and that has motivated researchers to conduct more insightful research. A great attention has been given to the unsaturated consolidation theory due to many foundation-related problems particularly relate to time-dependent soil volume change and settlement. However, a typical unsaturated soil usually has nonlinear properties and intricate phase relationships, which result in theoretical difficulties in formulating a reliable model for the consolidation prediction.

This thesis presents a systematic catalogue of analytical solutions for the consolidation of unsaturated soils subjected to various loading and initial conditions. Particularly, eigenfunction expansions and standard Laplace transformation techniques are used to solve the consolidation equations. This research provides rigorous solutions to estimate the rates of excess pore-air and pore-water pressure dissipation and consolidation settlement under the one-dimensional (1D), two-dimensional (2D) plane strain and axisymmetric consolidation conditions. For the mathematical derivation, uniform and linearly depth-dependent initial conditions are adopted along with homogeneous boundary conditions, including one-way and two-way drainage boundary conditions. In addition, effects of time-dependent loadings are also captured in this study. Four primary types of external loads, namely ramping, asymptotic, sinusoid and damped sine wave, are simulated and then incorporated in the proposed solutions. On the other hand, the 1D consolidation of unsaturated soils under non-isothermal conditions is sufficiently discussed. This study also demonstrates that the proposed

analytical solutions can change back to the traditional equations for saturated soils. Most results are graphically presented in the semi-logarithmic plots. Changes in excess pore pressures and settlement are investigated against the air to water permeability ratio  $(k_a/k_w)$ . Moreover, pore pressure isochrones along the flow domains are also highlighted in each consolidation field. Verification exercises are conducted by comparing the predicted results with other solutions obtained from existing literature. The proposed equations can be used by practicing engineers. Programmable methods such as Microsoft Excel or MATLAB can be simply adopted to generate results from proposed equations to predict the time-dependent settlement of unsaturated soils.

For all consolidation cases, it is predicted that variations in the permeability ratio  $k_a/k_w$  result in double inverse S curves for the excess pore-water pressure and settlement, while forming a single S curve for the excess pore-air pressure. The study shows that the 1D consolidation process in the two-way drainage soil stratum tends to proceed more quickly than that in the one-way drainage system. However, the consolidation rates under these boundary conditions are almost comparable when drain wells (for the 2D plane strain and axisymmetric cases) are installed in the soil profile. In the 2D plane strain consolidation system, if the horizontal permeability is greater than the vertical permeability (i.e.  $k_x/k_z > 1$ ), the horizontal flow will govern the dissipation rate and the effects of vertical flow is much attenuated. This point is also supported in the axisymmetric analysis.

Additionally, the time-dependent loadings and temperature variations have significant impacts on changes in excess pore pressures and settlement. For the loading effects, it can be predicted that excess pore-water pressures and settlement are considerably influenced by the loading patterns irrespective of  $k_a/k_w$  values. However, in most loading cases, effects of the applied loads on the excess pore-air pressure are less pronounced as  $k_a/k_w$  increases. On the other hand, variations in soil temperature are substantially attributed to the air temperature and the heat from solar radiation. It is predicted that, for time-dependent linear temperature variations, the excess pore-air pressure initially increases dramatically and then attains a constant value, while the excess pore-water pressure diminishes a very long time after the heat begins to increase. Besides, excess pore-air and pore-water pressures near the ground surface increase faster than those at lower depths when the temperature increases exponentially. Both

pressures then are fully dissipated as the temperature approaches the maximum value. For the case of diurnal temperature wave, the excess pore pressure curves would oscillate capturing damping and retarding effects. Development of analytical solutions for the unsaturated consolidation incorporating the above influencing factors would provide fundamental understandings of deformation of unsaturated soils. To my father, *Tuan Huu Ho*, my mother, *Thu Thí Le*, my brothers, *Híeu Huu Ho* and *Taí Huu Ho*, and my sister, *Vy Khanh Ho*, who shared love and strength with me throughout this marvellous journey.

#### ACKNOWLEDGEMENT

Studying a doctoral course at University of Technology Sydney (UTS) has offered me profound experiences in my academic life. During the PhD program, I have developed a genuine passion for academic research through rigorous assessments. However, this marvellous achievement would not have been possible without immense supports from my supervisors, family members and research colleagues.

First of all, I would like to express the deepest gratitude to my principal supervisor, Dr Behzad Fatahi, and my co-supervisor, A/Prof Hadi Khabbaz, for their immeasurable kindness, exhaustive guidance and encouragements. They have provided me sufficient supports and opportunities to overcome challenging tasks successfully. My PhD project could not have been achievable without their constructive feedbacks and worthy recommendations.

Secondly, I also gratefully thank all geotechnical research fellows who have been directly or indirectly involved in my doctoral study. More specifically, I am very grateful to Thu Minh Le who efficiently assisted me to develop numerical codes for data generation, to Antonio Reyno and Lam Nguyen for the laboratory assistance, and to Ali Parsa-Pajouh, Aslan Sadeghi Hokmabadi, Harry Nguyen, Balaka Ghosh and many others for their restless supports during the academic program.

In addition, I would like to sincerely acknowledge UTS Faculty of Engineering and Information Technology, and Centre of Built Infrastructure Research (CBIR) for encouraging awards and scholarships which enable me to complete the PhD research. I also appreciate Van Le and Phyllis Agius for their kind assistance.

Last but not least, I would like to express the immeasurable appreciation to my parents who have always been watching over my progress from overseas. Their consistent encouragement and love give me strength to strive against many difficulties in life. I also specially thank my younger brothers and sister who always bring joys and happiness to the family. They are motivation for me to work hard and attain my goals successfully. I am very fortunate to have such lovely family.

### LIST OF PUBLICATIONS

#### Published Journal Articles

- Ho, L, Fatahi, B & Khabbaz, H 2014, 'Analytical solution for one-dimensional consolidation of unsaturated soils using eigenfunction expansion method', *International Journal for Numerical and Analytical Methods in Geomechanics*, vol. 38, no. 10, pp. 1058-1077.
- Ho, L, & Fatahi, B 2015, 'Analytical solution for the two-dimensional plane strain consolidation of an unsaturated soil stratum subjected to time-dependent loading', *Computers and Geotechnics*, vol. 67, pp. 1-16.
- Ho, L, Fatahi, B & Khabbaz, H 2015, 'A closed form analytical solution for twodimensional plane strain consolidation of unsaturated soil stratum', *International Journal for Numerical and Analytical Methods in Geomechanics*, vol. 39, no. 15, pp. 1665-1692.
- Ho, L, & Fatahi, B 2015, 'One-dimensional consolidation analysis of unsaturated soils subjected to time-dependent loading', *International Journal for Geomechanics*, vol. 16, no. 2, pp. 1-19.
- Ho, L, Fatahi, B & Khabbaz, H 2015, 'Analytical solution to axisymmetric consolidation in unsaturated soils with linearly depth-dependent initial conditions', *Computers and Geotechnics*, vol. 74, pp. 102-121.
- Ho, L, & Fatahi, B 2015, 'Axisymmetric consolidation in unsaturated soil deposit subjected to time-dependent loadings', *International Journal for Geomechanics*, doi: 10.1061/(ASCE)GM.1943-5622.0000686.

#### Published Conference Papers

- Ho, L, Fatahi, B & Khabbaz, H 2013, 'Exact solution to predict excess pore pressures and settlement of unsaturated soil deposit due to uniform loading', *GEO Montreal* 2013, Canadian Geotechnical Society, Montreal, pp. 1-6.
- Ho, L, Fatahi, B & Khabbaz, H 2014, 'One-dimensional consolidation of unsaturated soil deposit with various initial conditions', *Geo-Shanghai 2014*, American Society of Civil Engineers (ASCE), pp. 145-155.
- Ho, L, Fatahi, B & Khabbaz, H 2014, 'Analytical solution for one-dimensional consolidation of unsaturated soil deposit subjected to step loading', *Proceedings* of the 6<sup>th</sup> International Conference on Unsaturated Soils – UNSAT 2014, Taylor & Francis Group, Sydney, pp. 1763-1769.

Ho, L, Fatahi, B & Khabbaz, H 2015, 'Exact analytical solution for one-dimensional consolidation of unsaturated soil stratum subjected to damped sine wave loading', *Proceedings of the 12<sup>th</sup> Australia New Zealand Conference on Geomechanics*, New Zealand Geotechnical Society and the Australian Geomechanics Society, Wellington, pp. 1115-1122.

# **TABLE OF CONTENTS**

ABSTRACTiii
ACKNOWLEDGEMENT
LIST OF PUBLICATIONS
LIST OF FIGURES
LIST OF TABLES
LIST OF NOTATIONS
CHAPTER 1: INTRODUCTION
1.1. General
1.2. Statement of problem
1.3. Objectives and scope of research
1.4. Organisation of thesis
CHAPTER 2: LITERATURE REVIEW
2.1. General
2.1.1. Phases in unsaturated soil
2.1.2. Surface tension on the contractile skin
2.1.3. Soil suction
2.1.4. Fabric modifications induced by soil suction
2.2. Wetting-induced volume change issues
2.2.1. Problematic soils in response to saturation
2.2.2. Collapsible soils

2.2.3.	Expansive soils	26
2.3. Str	ress State Variables in Unsaturated Soils	29
2.3.1.	Single-valued effective stress equations	29
2.3.2.	Equilibrium analyses and newly proposed stress state variables	33
2.4. Vo	lume-Mass Constitutive Relation	40
2.4.1.	Continuity requirement	40
2.4.2.	Volume-mass constitutive models for unsaturated soils	41
2.4.3.	Uniqueness of constitutive surfaces	47
2.5. Ela	astoplastic (EP) constitutive models for unsaturated soils	50
2.5.1.	Introduction	50
2.5.2.	Independent net stress and matric suction approach (Approach 1)	50
2.5.3.	Effective stress approach (Approach 2)	51
2.5.4.	SFG approach (Approach 3)	52
2.6. Co	nsolidation analyses for saturated soils	54
2.6.1.	Classical consolidation theory and its governing equation	54
2.6.2.	Solution to consolidation of saturated soils	59
2.6.3.	Axisymmetric consolidation and its polar governing equation	62
2.6.4.	Solution to radial consolidation of saturated soils	66
2.7. Co	nsolidation analyses for unsaturated soils	71
2.7.1.	Consolidation theory and governing equation of flow	71
2.7.2.	Existing models for consolidation in unsaturated soils	74

2.8.	Summary
СНАРТ	TER 3: ANALYTICAL SOLUTION FOR ONE-DIMENSIONAL
CONSC	DLIDATION OF UNSATURATED SOILS USING EIGENFUNCTION
EXPAN	SION METHOD
3.1.	Introduction
3.2.	Governing equations of flow for unsaturated soils
3.3.	Analytical solution for 1D consolidation
3.4.	Settlement of unsaturated soils
3.5.	Worked examples
3.5	.1. Worked example 1
3.5	.2. Worked example 2
3.6.	Summary
СНАРТ	TER 4: ONE-DIMENSIONAL CONSOLIDATION ANALYSIS OF
UNSAT	<b>TURATED SOILS SUBJECTED TO TIME-DEPENDENT LOADING</b> 109
4.1.	Introduction
4.2.	Governing equations for unsaturated soils
4.3.	Analytical formulations for 1D consolidation111
4.3	.1. Boundary and initial conditions
4.3	.2. Analytical procedure
4.3	.3. Settlement of the unsaturated soil layer
4.4.	Worked examples
	, on our on an approximation of the second

4.4.2.	Asymptotic Loading	124
4.4.3.	Sinusoidal Loading	127
4.4.4.	Damped Sine Wave Loading	131
4.5. Su	ummary	136

# 

5.1. Introduction	
5.2. Governing flow equations in unsaturated soils	
5.3. Analytical solution	141
5.3.1. Boundary and initial conditions	142
5.3.2. Excess pore pressure dissipation and settlement	142
5.3.3. Thermal equations	146
5.4. Examples	149
5.4.1. Example 1	150
5.4.2. Example 2	160
5.5. Summary	169
CHAPTER 6: A CLOSED FORM ANALYTICAL SOLUTION H DIMENSIONAL PLANE STRAIN CONSOLIDATION OF UNSA	
SOIL STRATUM	171
6.1. Introduction	171
6.2. Transient flow equations for 2D consolidation theory	171

	An	alytical solution for 2D unsaturated consolidation equations	
6.3	3.1.	Boundary and initial conditions	174
6.3	3.2.	Eigenfunction expansion and Laplace transformation methods	177
6.4.	Av	erage degree of consolidation of 2D unsaturated soil system	
6.5.	Wo	rked examples	
6.5	5.1.	Worked example 1	
6.5	5.2.	Worked example 2	
6.6.	Sur	nmary	
CHAP	TER	7: ANALYTICAL SOLUTION FOR THE TWO-DIMEN	NSIONAL
PLAN	E ST	RAIN CONSOLIDATION OF AN UNSATURATED SOIL ST	<b>FRATUM</b>
SUBJE	CTE	D TO TIME-DEPENDENT LOADING	
7.1.	Intr	oduction	202
7.2.			
	Go	verning equations of 2D plane-strain consolidation	
7.3.		verning equations of 2D plane-strain consolidation	
7.3. 7.4.	Ana		
	Ana No	alytical solution for excess pore pressure dissipation	204
7.4. 7.5.	Ana No	alytical solution for excess pore pressure dissipation	204 212 213
7.4. 7.5. 7.5	Ana Noi Wo	alytical solution for excess pore pressure dissipation	204 212 213 214
7.4. 7.5. 7.5	Ana Nor Wo	alytical solution for excess pore pressure dissipation rmalised settlement of 2D unsaturated soil consolidation orked examples Consolidation under ramped loading	204 212 213 214 218
7.4. 7.5. 7.4 7.4	An: Noi Wo 5.1.	alytical solution for excess pore pressure dissipation rmalised settlement of 2D unsaturated soil consolidation orked examples Consolidation under ramped loading Consolidation under asymptotic loading	204 212 213 214 218 221
7.4. 7.5. 7.4 7.4 7.4 7.4	Ana Nor Wo 5.1. 5.2.	alytical solution for excess pore pressure dissipation rmalised settlement of 2D unsaturated soil consolidation orked examples Consolidation under ramped loading Consolidation under asymptotic loading Consolidation under sinusoidal loading	204 212 213 214 218 221 225

СНАРТЕ	CR 8: ANALYTICAL SOLUTION TO AXISYMM	METRIC
CONSOI	LIDATION IN UNSATURATED SOILS WITH LINEARLY	DEPTH-
DEPEND	DENT INITIAL CONDITIONS	
8.1. I	Introduction	
8.2. I	Polar governing equations of flow	234
8.3. <i>A</i>	Analytical solution	
8.3.1	. Boundary and initial conditions	
8.3.2	Excess pore pressure dissipation	
8.3.3	Average degree of consolidation	
8.4. I	Examples	
8.4.1	. Example 1 – Axisymmetric consolidation with radial flow only	
8.4.2	Example 2 – Axisymmetric consolidation with both radial and	d vertical
flows	s	
8.5. 5	Summary	
СНАРТЕ	<b>ER 9: AXISYMMETRIC CONSOLIDATION IN UNSATURATE</b>	ED SOIL
DEPOSI	<b>F SUBJECTED TO TIME-DEPENDENT LOADINGS</b>	
9.1. I	Introduction	
9.2. I	Polar governing equations of flow	
9.3. <i>A</i>	Analytical solution	
9.3.1	. Boundary and initial conditions	
9.3.2	Excess pore-air and pore-water pressures	
9.3.3	Normalised settlement	277

9.4. Worked Examples
9.4.1. Ramped loading
9.4.2. Asymptotic loading
9.4.3. Sinusoidal loading
9.4.4. Damped sine wave loading
9.4.5. Variations in matric suction and net stress
9.5. Summary
CHAPTER 10: CONCLUSIONS AND RECOMMENDATIONS
10.1. Summary
10.2. Conclusions
10.3. Recommendations for future studies
REFERENCES
APPENDIX A – Dissipation of excess pore-air and pore-water pressures
<b>APPENDIX B</b> – Predicted excess pore pressures due to temperature variation
APPENDIX C – Dissipation of excess pore-air and pore-water pressures and consolidation settlement
APPENDIX D – Evaluation of initial excess pore pressures due to a change in total
stress
APPENDIX E – Solution predicting excess pore-air and pore-water pressure         dissipation         332
APPENDIX F – Polar transformation for x- and y-coordinates

APPENDIX G - Solutions for excess pore pressure dissipation and average degree of
consolidation
APPENDIX H – Initial excess pore pressures in response to constant loading
APPENDIX I – Excess pore-air and pore-water pressure dissipation

## **LIST OF FIGURES**

Figure 1.1. Schematic of flux surface boundary occurring at the surface of unsaturated soil system
Figure 1.2. A typical settlement curve obtained from oedometer test
Figure 2.1. An unsaturated soil element with air, water and contractile
Figure 2.2. Schematic phase diagram of unsaturated soil: (a) four-phase soil system and (b) simplified three-phase soil system (modified after Fredlund & Rahardjo 1993)
Figure 2.3. Surface tension effect in the contractile skin: (a) intermolecular forces acting on a molecule in the contractile skin and on a molecule in water; (b) a concave segment and surface tension in the contractile skin (after Fredlund et al. 2012)14
Figure 2.4. The 3D membrane with radii of curvature (modified after Fredlund et al. 2012)
Figure 2.5. Total, matric and osmotic suctions obtained using compacted Regina clay (modified after Krahn & Fredlund 1972)
Figure 2.6. Soil fabric modification due to varying suctions (after Koliji et al. 2006)20
Figure 2.7. Compression indices influenced by suction increase (after Cuisinier & Laloui 2004)
Figure 2.8. Result generated by oedometer test indicating collapse of metastable- structured brickearth (modified after Northmore et al. 1996)
Figure 2.9. Effects of external total stress and matric suction on inter-particle forces at contact of adjacent particles (after Wheeler & Karube 1996)
Figure 2.10. Normal and shear stresses acting on a cuboidal soil element (after Fredlund et al. 2012)

Figure 2.11. Components for force equilibrium of (a) soil element, (b) air phase, (c) water phase and (d) contractile skin in the y-direction (modified after Fredlund &
Rahardjo 1993)
Figure 2.12. A nonlinear stress-strain relationships and sign convention for volumetric deformation properties
Figure 2.13. Constitutive surfaces for: (a) soil structure and (b) water phase (modified after Fredlund et al. 2012)
Figure 2.14. Hysteresis associated with (a) soil structure and (b) contractile skin (after Fredlund et al. 2012)
Figure 2.15. Stress paths for determining volume change coefficients and vertical deformation (modified after Fredlund et al. 2012)
Figure 2.16. Slopes of compressibilities $\lambda_{v\sigma}$ and $\lambda_{vs}$ in the (e – lns) space (after Sheng et al. 2008)
Figure 2.17. Soil stratum under (a) the one-way drainage boundary condition and (b) the two-way drainage boundary condition
Figure 2.18. One-dimensional flow through the soil element (after Budhu 2008)57
Figure 2.19. Typical excess pore pressure isochrones under one-way drainage system (after Verruijt & Van Baars 2007)60
Figure 2.20. Average degree of consolidation (U) versus time factor $(T_v)$ for uniform and triangular initial conditions (modified after Taylor 1948, Venkatramaiah 2006, and Budhu 2008)
Figure 2.21. Typical drain well installed in saturated soil stratum: (a) vertical sand drains and (b) PVDs with smear effects
Figure 2.22. Plan of drain well systems: (a) square patterns and (b) triangular patterns 64

Figure 2.23. Relationship between average degree of consolidation (U <sub>r</sub> ) and time factor
(T <sub>r</sub> ) obtained from Barron (1948) solution (modified after Barron 1948, after
Craig 2004)
Craig 2004)07
Figure 2.24. Flows of pore-air and pore-water through the unsaturated soil element
(modified after Fredlund & Hasan 1979)
Figure 3.1. A simplified model for one-dimensional elevation of unsaturated soils: (a)
one-way drainage system and (b) two-way drainage system
Figure 3.2. Dissipation of excess pore-water and pore-air pressures for (a) one-way
drainage system and (b) two-way drainage system
Figure 3.3. Different initial conditions due to the changes of $\lambda w$ and $\lambda a$
Figure 3.4. Dissipation of pore pressures varying with permeability ratios in one-way
drainage system: (a) dissipation of pore-air pressure and (b) dissipation of pore-
water pressure
Figure 3.5. Dissipation of pore pressures varying with permeability ratios in two-way
drainage system: (a) dissipation of pore-air pressure and (b) dissipation of pore-
water pressure
Figure 3.6. Settlement of unsaturated soils varying with permeability ratios: (a) for one-
way drainage and (b) for two-way drainage systems
Figure 3.7. Dissipation of pore pressures varying with depth in one-way drainage
system: (a) dissipation of pore-air pressure and (b) dissipation of pore-water
pressure
Figure 3.8. Dissipation of pore pressures varying with depth in two-way drainage
system: (a) dissipation of pore-air pressure and (b) dissipation of pore-water
pressure
Figure 3.9. Dissipation of pore pressures varying with $\lambda a$ in one-way drainage system:
(a) dissipation of pore-air pressure and (b) dissipation of pore-water pressure 100

- Figure 3.10. Dissipation of pore pressures varying with λw in one-way drainage system:(a) dissipation of pore-air pressure and (b) dissipation of pore-water pressure ..101
- Figure 3.11. Dissipation of pore pressures varying with λa in two-way drainage system:(a) dissipation of pore-air pressure and (b) dissipation of pore-water pressure ..102
- Figure 3.12. Dissipation of pore pressures varying with λw in two-way drainage system:(a) dissipation of pore-air pressure and (b) dissipation of pore-water pressure ..103

- Figure 4.3. Variations in excess pore pressures and settlement with different ka/kw due to the ramped loading for (a–c) one-way and (d–f) two-way drainage conditions

Figure 4.6. Excess pore pressures and settlement $(ka/kw = 1)$ with different values of
the parameter b due to the asymptotic loading for (a-c) one-way and (d-f) two-
way drainage conditions

Figure 5.2. Temperature distributions along depth (modified after Hillel 2003) ....... 147

Figure 5.4. Changes in (a) pore-air and (b) pore-water pressures induced by the effect of time-dependent linear temperature
Figure 5.5. Changes in (a) excess pore-air and (b) excess pore-water pressures induced by combined effects of time-dependent linear temperature and constant loading 
Figure 5.6. Deformation of soil due to (a) the time-dependent linear temperature only and (b) the time-dependent linear temperature and constant loading
Figure 5.7. Changes in (a) pore-air and (b) pore-water pressures induced by the effect of time-dependent exponential temperature
Figure 5.8. Changes in (a) excess pore-air and (b) excess pore-water pressures induced by combined effects of time-dependent exponential temperature and constant loading
Figure 5.9. Deformation of soil due to (a) the time-dependent exponential temperature only and (b) the time-dependent exponential temperature and constant loading 156
Figure 5.10. Changes in (a) pore-air and (b) pore-water pressures induced by the effect of time-dependent diurnal temperature variation
Figure 5.11. Changes in (a) excess pore-air and (b) excess pore-water pressures induced by combined effects of time-dependent diurnal temperature variation and constant loading
Figure 5.12. Deformation of soil due to (a) the time-dependent diurnal temperature variation only and (b) the time-dependent diurnal temperature variation and constant loading
Figure 5.13. Effect of linear thermal parameter ' <i>a</i> ' on changes in (a) pore-air and (b) pore-water pressures
Figure 5.14. Combined effects of linear thermal parameter ' <i>a</i> ' and constant loading on changes in (a) excess pore-air and (b) excess pore-water pressures

Figure 5.15. Deformation of soil due to (a) the linear thermal parameter ' $a$ ' without
considering constant loading and (b) the linear thermal parameter ' $a$ ' while
considering constant loading

- Figure 5.17. Combined effects of exponential thermal parameter 'b' and constant loading on changes in (a) excess pore-air and (b) excess pore-water pressures. 165

- Figure 6.2. Different distributions of initial excess pore pressures along depth: (a) uniform distribution, (b) trapezoidal distribution and (c) triangular distribution 176

Figure 6.7. Average degree of consolidation varying with $k_a/k_w$ under (a) top drai	nage
and (b) top-base drainage boundary conditions	. 190

- Figure 6.18. Excess pore pressure isochrones against (a) depth ratio and (b) length ratio due to effects of  $\zeta_a$  and  $\zeta_w$  under top-base drainage boundary condition......200

Figure 7.1. The profile of the homogeneous soil stratum representing (a) top drainage boundary system and (b) top-base drainage
Figure 7.2. Load varying linearly with time
Figure 7.3. Variations in (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with different $k_a/k_w$ due to ramped loading
Figure 7.4. Influence of linear loading rate 'a' on (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with $k_a/k_w = 0.1$
Figure 7.5. Variations in excess pore-air and pore-water pressures due to ramped loading in 1D consolidation
Figure 7.6. Load varying exponentially with time
Figure 7.7. Variations in (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with different $k_a/k_w$ due to asymptotic loading
Figure 7.8. Influence of exponential loading rate 'b' on (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with $k_a/k_w = 0.1$
Figure 7.9. Load varying periodically with time
Figure 7.10. Variations in (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with different k <sub>a</sub> /k <sub>w</sub> due to sinusoidal loading
Figure 7.11. Influence of angular frequency ' $\theta$ ' on (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with $k_a/k_w = 0.1$
Figure 7.12. Damped sine wave load varying with time
Figure 7.13. Variations in (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with different $k_a/k_w$ due to damped sine wave loading
Figure 7.14. Influence of exponential loading rate 'c' on (a) excess pore-air pressure; (b) excess pore-water pressure; and (c) settlement with $k_a/k_w = 0.1$

- Figure 8.16. Matric suction change due to variations of (a)  $\zeta_a$  and (b)  $\zeta_w$  under the PTIB boundary condition (for radial and vertical flows, linear initial condition) .......259

- Figure 8.20. Distribution of excess pore pressures along the vertical domain at  $T = 10^{-3}$  at different radii under (a) PTIB and (b) PTPB boundary conditions while adopting  $\zeta_a = \zeta_w = 0.5$  (for radial and vertical flows, linear initial condition).....263

- Figure 9.4. Normalised settlement varying with k<sub>a</sub>/k<sub>w</sub> under the ramped loading.......280
- Figure 9.6. Effects of the linear loading parameter 'a' on the normalised settlement..281

Figure 9.8. Normalised settlement varying with  $k_a/k_w$  under the asymptotic loading...283

Figure 9.11. Dissipation rates of (a) excess pore-air and (b) excess pore-water pressures varying with $k_a/k_w$ under the sinusoidal loading
Figure 9.12. Normalised settlement varying with $k_a/k_w$ under the sinusoidal loading .286
Figure 9.13. Effects of the angular frequency '\psi' on the dissipation rates of (a) excess pore-air and (b) excess pore-water pressures
Figure 9.14. Effects of the angular frequency ' $\phi$ ' on the normalised settlement
Figure 9.15. Dissipation rates of (a) excess pore-air and (b) excess pore-water pressures varying with $k_a/k_w$ under the damped sine wave loading
Figure 9.16. Normalised settlement varying with k <sub>a</sub> /k <sub>w</sub> under the damped sine wave loading
Figure 9.17. Effects of the exponential loading parameter 'c' on the dissipation rates of (a) excess pore-air and (b) excess pore-water pressures while keeping the angular frequency 'φ' constant
Figure 9.18. Effects of the exponential loading parameter 'c' on the normalised settlement while keeping the angular frequency ' $\phi$ ' constant
<ul> <li>Figure 9.19. Effects of the angular frequency 'φ' on the dissipation rates of (a) excess pore-air and (b) excess pore-water pressures while keeping the exponential loading parameter 'c' constant</li></ul>
Figure 9.20. Effects of the angular frequency 'φ' on the normalised settlement while keeping the exponential loading parameter 'c' constant
Figure 9.21. Effects of the permeability ratio k <sub>a</sub> /k <sub>w</sub> on the (a) normalised matric suction and (b) normalised net stress under the ramped loading
Figure 9.22. Effects of the linear loading parameter 'a' on the (a) normalised matric suction and (b) normalised net stress
Figure 9.23. Effects of the permeability ratio k <sub>a</sub> /k <sub>w</sub> on the (a) normalised matric suction and (b) normalised net stress under the asymptotic loading

Figure 9.24. Effects of the exponential loading parameter	'b' on the (a) normalised
matric suction and (b) normalised net stress	

## LIST OF TABLES

Table 2.1. Relation between surface tension and temperature (after Kaye & Laby 1921)
Table 2.2. Criteria for determining collapsibility based on clay content (modified after Handy 1973)
Table 2.3. Criteria indicating severity of collapse based on percentage of collapse (modified after Pells et al. 1975)    25
Table 2.4. Potential swell-shrink of clayey soils based on various categories of PI (modified after BRE 1993)
Table 2.5. Potential swell and classifications based on USAEWES (modified after O'Neil & Poormoayed 1980)    28
Table 2.6. Single-valued effective stress equations for unsaturated soils (modified after      Fredlund 1987)
Table 2.7. Stress state variables depending on each referential pressure (Fredlund et al. 2012)
Table 2.8. Summary of constitutive equations for different loading conditions (modified after Fredlund et al. 2012)    45
Table 2.9. Dimensions of various types of vertical drain (modified after Holtz et al.      1991, and Smoltczyk 2003)
Table 2.10. Summary of theoretical solutions for determining the degree of consolidation Ur

# LIST OF NOTATIONS

# English letters

C <sub>a</sub>	interactive constant associated with the air phase;
C <sub>w</sub>	interactive constant associated with the water phase;
c <sup>a</sup> <sub>vr</sub>	coefficient of consolidation with respect to the air phase in the radial
	domain;
$c_{v_z}^a$	coefficient of consolidation with respect to the air phase in the vertical
	domain;
$c_{v_x}^a$	coefficient of volume change with respect to the air phase in x-direction;
$c_{\sigma}^{a}$	coefficient of consolidation due to total stress with respect to the air
	phase;
$C_{V_{r}}^{W}$	coefficient of consolidation with respect to the water phase in the radial
	domain;
$C_{V_Z}^W$	coefficient of consolidation with respect to the water phase in the vertical
	domain;
$C_{V_X}^W$	coefficient of volume change with respect to the water phase in x-
	direction;
$c_{\sigma}^{w}$	coefficient of consolidation due to total stress with respect to the water
	phase;
g	gravitational constant;
Н	thickness of the soil stratum;
i	integer for the Fourier sine series (for 2D plane strain consolidation)
	Fourier Bessel series (for axisymmetric consolidation);
j	integer for the Fourier sine series (for both plane strain and axisymmetric
	conditions);
К	eigenvalue for vertical boundary condition (for 1D consolidation);
Κ	ratio of the changes in horizontal (or radial) and vertical stresses at a
	point;
k	integer for the Fourier sine series (for 1D consolidation);
k <sub>ar</sub>	coefficient of permeability for the air phase in the radial domain;

k <sub>ax</sub>	coefficient of permeability for air in x-direction;
k <sub>az</sub>	coefficient of permeability for the air phase in the vertical domain;
k <sub>wr</sub>	coefficient of permeability for the water phase in the radial domain;
k <sub>wx</sub>	coefficient of permeability for water in x-direction;
k <sub>wz</sub>	coefficient of permeability for the water phase in the vertical domain;
L	width of soil layer;
М	molecular mass of the air phase;
m <sub>v</sub>	coefficient of volume change in saturated soils;
$m_1^a$	coefficient of volume change of the air phase with respect to the change
	of net stress;
$m_2^a$	coefficient of volume change of the air phase with respect to the change
	of suction;
$m_1^s$	coefficient of volume change of the soil with respect to the change of net
	stress;
$m_2^s$	coefficient of volume change of the soil with respect to the change of
	suction;
$m_1^w$	coefficient of volume change of the water phase with respect to the
147	change of net stress;
$m_2^w$	coefficient of volume change of the water phase with respect to the
	change of suction;
n	porosity;
q <sub>z</sub>	external loading;
R	universal air constant;
$R_a(r)$	eigenfunction with respect to the excess pore-air pressure for domain r;
R <sub>w</sub> (r)	eigenfunction with respect to the excess pore-water pressure for domain
7	r; investigated radius;
r	radius of zone of influence;
r <sub>e</sub>	pore radius;
r <sub>p</sub>	radius of the drain well;
r <sub>w</sub> S	matric suction;
S S*	normalized settlement;
5	

S(t)	consolidation settlement;
S <sub>max</sub>	maximum settlement;
S <sub>r</sub>	degree of saturation;
$S_{\infty}$	final ground surface settlement;
s <sub>f</sub>	final matric suction;
s <sub>0</sub>	initial matric suction;
Т	time factor;
$T_a(t)$	generalized Fourier coefficients varying with time with respect to the air
	phase;
T <sub>w</sub> (t)	generalized Fourier coefficients varying with time with respect to the
	water phase;
t	elapsed time;
U	degree of consolidation;
Ū	average degree of consolidation;
Ur	degree of consolidation under axisymmetric conditions;
и	displacement in x-domain;
u <sub>a</sub>	excess pore-air pressure;
u <sub>a,t</sub>	first order of partial differential equation (PDE) of air with respect to
	time;
u <sub>a,r</sub>	first order of partial differential equation (PDE) of air with respect to
	radius;
u <sub>a,rr</sub>	second order of partial differential equation (PDE) of air with respect to
	radius;
u <sub>a,xx</sub>	second order of partial differential equation (PDE) of air with respect to
	width;
u <sub>a,zz</sub>	second order of partial differential equation (PDE) of air with respect to
	depth;
u <sub>atm</sub>	atmospheric pressure;
u <sup>0</sup> a	maximum initial excess pore-air pressure;
u <sub>w</sub>	pore-water pressure;
u <sub>w,t</sub>	first order of partial differential equation (PDE) of water with respect to
	time;

u <sub>w,r</sub>	first order of partial differential equation (PDE) of water with respect to
	radius;
u <sub>w,rr</sub>	second order of partial differential equation (PDE) of water with respect
	to radius;
u <sub>w,xx</sub>	second order of partial differential equation (PDE) of water with respect
	to width;
u <sub>w,zz</sub>	second order of partial differential equation (PDE) of water with respect
	to depth;
$u_w^0$	maximum initial excess pore-water pressure;
V <sub>0</sub>	initial volume of the soil element;
Va	volume of air within soil element;
V <sub>w</sub>	volume of water within soil element;
ν	displacement in y-domain;
$v(r_p, s)$	predicted volume fraction of pores at suction s;
W	displacement in z-domain;
$X_a(x)$	eigenfunction with respect to pore-air pressure for domain x;
$X_w(x)$	eigenfunction with respect to pore-water pressure for domain x;
Х	investigated width;
$Z_a(z)$	eigenfunction with respect to the excess pore-air pressure for domain z;
$Z_w(z)$	eigenfunction with respect to the excess pore-water pressure for domain
	z; and
Z	investigated depth;

### **Greek letters**

$\gamma_{w}$	water unit weight;
Δs	suction change;
$\Delta \overline{\sigma}$	change in net stress;
ε <sub>v</sub>	total volumetric strain;
Θ	absolute temperature in Kelvin;
θ	angular coordinate;
$\theta^{\circ}$	temperature in degree Celsius;
$\lambda_a^{ij}$	separation constant with respect to the air phase;

- $\lambda_{w}^{ij}$  separation constant with respect to the water phase;
- $\mu^{j}$  eigenvalue for vertical boundary condition (i.e., PTIB and PTPB);
- $\xi^{i}$  eigenvalue for radial boundary condition;
- $\sigma_r$  total stress in r-domain;
- $\sigma_x$  total stress in x-direction;
- $\sigma_z$  total stress in z-domain;
- $\sigma_{\theta}$  total stress in  $\theta$ -domain; and
- $\overline{\sigma}$  net stress.